Expedition 316 Site C0006¹

Expedition 316 Scientists²

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Background and objectives

Integrated Ocean Drilling Program (IODP) Site C0006 (proposed Site NT1-03B; Kimura et al., 2007) targets the main frontal thrust at the seaward edge of the accretionary prism (Figs. F1, F2). Based on seismic data and submersible studies, this thrust was interpreted to have placed moderately consolidated (and presumably older) clastic rocks over weak and unlithified late Quaternary trench section clastic sediments (Ashi et al., 2002). The scientific objectives of drilling at Site C0006 are to clarify the evolution of the frontal thrust from its birth to death, the function of the frontal thrust with respect to large earthquakes, and the relationship between fluid behavior, slip, and deformation within this fault zone.

Site C0006 was first drilled during IODP Expedition 314 (see the "Expedition 314 Site C0006" chapter), and logging-whiledrilling (LWD) logs were obtained to 885.5 m logging depth below seafloor (LSF). During IODP Expedition 316, coring was completed to 603 m core depth below seafloor (CSF). Poor hole conditions stopped drilling at this site before the frontal thrust was reached.

During Expedition 314, four primary logging units were defined in IODP Hole C0006B based on visual inspection of the gamma ray, resistivity, and caliper log responses:

- 1. Logging Unit I (0–198 m LSF) is interpreted as sandy and muddy sediments.
- 2. Logging Unit II (198–428 m LSF) is interpreted as a mudstone with thick sandstone.
- 3. Logging Unit III (428–711 m LSF) is interpreted as alternating beds of mudstone and sandstone (base marked by a large fault zone).
- 4. Logging Unit IV (711 m LSF to total depth [TD]) is below the inferred fault zone and interpreted as sandstone.

Core samples from Expedition 316 drilling at this site will be integrated with the existing three-dimensional (3-D) seismic and LWD results to characterize physical properties, strength, composition, and structure of the hanging wall, frontal thrust, and footwall at this site. In situ temperature data were also collected to assess the thermal gradient and heat flow in this area.



Operations

Positioning on Site C0006

The D/V *Chikyu* arrived at Site C0006 on 27 December 2007 and began testing the underwater television system (UWTV). Electronics problems forced cancellation of that test, and positioning over Hole C0006C began at 1200 h on 28 December. The hydraulic piston coring system (HPCS) bottom-hole assembly (BHA) was rigged up and run to the seafloor, and Hole C0006C was tagged at 1915 h on 28 December.

Hole C0006C

Because of the lack of a camera system or remotely operated vehicle (ROV) observation, collection of a mudline core had to be accomplished by trial and error. One HPCS core (316-C0006C-1H) was taken at 1915 h on 28 December 2007 (33°1.6458'N, 136°47.6282'E; seafloor = 3880.5 m mud depth below sea level [MSL]), resulting in full recovery, which required repositioning and reshooting in order to collect the mudline.

Hole C0006D

One HPCS core (316-C0006D-1H) was taken in Hole C0006D (33°1.6431'N, 136°47.6282'E; seafloor = 3877.5 m MSL) at 2245 h on 28 December 2007, resulting in full recovery with no mudline. The vessel was again repositioned.

Hole C0006E

Core 316-C0006E-1H was collected at 0000 h on 29 December 2007, resulting in 5.19 m of recovery, including the mudline in Hole C0006E (33°1.6444'N, 136°47.6282'E; seafloor = 3875.81 m MSL). HPCS coring continued from 5.19 m CSF. We collected 14 HPCS cores with total recovery of 83.54 m (average recovery = 105.31%). Advanced piston coring temperature tool (APCT3) measurements were taken every other core starting at the third core (316-C0006E-3H, 5H, 8H, 10H, 12H, and 14H). Refusal (no penetration) occurred at Core 316-C0006E-14H, and HPCS coring was halted.

Extended shoe coring system (ESCS) coring commenced at that time, resulting in the recovery of 35 cores (316-C0006E-15X through 49X) with total recovery of 330.11 m at a rate of 74.76%. Six Davis-Villinger Temperature Probe (DVTP) measurements were made following Cores 316-C0006E-23X, 26X, 28X, 29X, 35X, and 42X. Three of the DVTP runs were unsuccessful because of battery failure, thermistor failure, and failure to penetrate formation following Cores 316-C0006E-23X, 28X, and 42X, respectively. After observing a drastically reduced rate of penetration during the cutting of Core 316-C0006E-49X, we determined that refusal had been reached, and Hole C0006E was completed at 409.4 m CSF at 1930 h on 6 January 2008. We killed Hole C0006E with highdensity mud, pulled the BHA out of the hole, tripped the drill pipe, and racked back the HPCS/ESCS BHA. During this time, an electrical problem with the wireline winch motor required that Core 316-C0006E-49X be recovered after recovering the BHA on the rig floor. This occurred at 0330 h on 7 January. Table T1 shows the cores collected, meters recovered, and recovery percentage for Holes C0006C, C0006D, and C0006E.

Hole C0006F

The *Chikyu* then relocated to Hole C0006F and the rotary core barrel (RCB) BHA was run to the seafloor. Hole C0006F ($33^{\circ}1.6242'N$, $136^{\circ}47.6282'E$; water depth = 3875.5 m MSL) was tagged at 1730 h on 7 January 2008. We conducted jet-in to 50 mbsf and washed to 395 mbsf. RCB coring operations began, and 23 RCB cores were recovered (Cores 316-C0006F-1R through 23R) from 395 to 603 m CSF with total recovery of 56.48 m at a rate of 27.15%.

Following collection of Core 316-C0006F-23R, it was determined based on pump rates, pressure, torque, and rotations per minute (rpm) that the hole condition had deteriorated to such a degree as to make further coring too risky. As pumping rate increased, the torque increased to the point of stalling the top drive (0 rpm); as pump rates dropped, torque would simultaneously drop and rpm would increase. The only way to get the bit back to the bottom of the hole was to run in the hole with <10 strokes per minute, which was considered unacceptably risky for either drilling or coring. The decision was made at ~0900 h on 13 January to abandon Site C0006 and relocate to proposed Site NT1-03A as an alternative means to achieve the science goals for the NT1-03 family of sites. We killed Hole C0006F with high-density mud, pulled the BHA out of the hole, tripped the drill pipe, and racked back the RCB BHA at 2100 h on 13 January. Table T2 shows the cores collected, meters recovered, and recovery percentage for Hole C0006F.

Lithology

Three lithologic units were recognized during examination of cores from Site C0006 (Fig. F3; Table T3). Four subunits are recognized in Unit II. Units and subunits are differentiated based on contrasts in grain size, mineralogy, composition, and presence (and thickness) of sand and ash layers. In choosing unit boundaries, we also considered biostratigraphic



information, paleomagnetic data, X-ray computed tomography (CT) images, observations of structural style, and interpretations of LWD and seismic results obtained during Expedition 314 (see the "Expedition 314 Site C0006" chapter). Numerous thrust faults offset the succession at Site C0006 with duplication of stratigraphic intervals. Thus, true stratigraphic thicknesses are difficult to determine and the estimates given here are maxima.

Unit I (trench to slope transition facies)

Interval: Sections 316-C0006E-1H-1, 0 cm, through 4H-3, 20 cm Depth: Hole C0006E = 0.00–27.23 m CSF Age: Pleistocene

The dominant lithology of Unit I is greenish gray silty clay that contains clay, quartz, feldspar, lithic fragments, vitric fragments, and calcareous nannofossils (Fig. F3; Table T3). Calcite content is an important defining characteristic of this unit, ranging from 0% to 7.5% and averaging 2%. In LWD data from Expedition 314, the corresponding interval was not logged with the resistivity tool and was included in a logging unit that largely corresponds to lithologic Unit II. Unit I consists of a fining-upward succession of silty clay, sand, silty sand, and rare volcanic ash layers. The mud is structureless and locally has green color banding. Sand and silty sand are extensively disrupted by a coring disturbance that locally creates mixtures of sand and mud. Lower in the unit, thin to thick beds with sharp bases and graded tops fine upward into the overlying mud. Generally, sand layers are thinner in the upper part of the unit. The sand component is mainly fine to very fine grained and consists of quartz, feldspar, lithic grains, and vitric fragments. A 1.25 m thick layer of light olivegray volcanic ash with abundant pumice fragments occurs near the base of the unit.

The contact between Unit I and underlying Subunit IIA is distinguished by the first appearance of thicker beds (>50 cm; Fig. F3B) of black sand below and the increase in mud content above the unit boundary. Deposition occurred on the lowermost slope above the trench floor by hemipelagic settling, onlap of axial turbidity currents that decreased through time, and accumulation of a thick ash.

Unit II (trench deposits)

Intervals: Sections 316-C0006E-4H-3, 20 cm, through 49X-CC, 21 cm, and 316-C0006F-1R-1, 0 cm, through 7R-CC, 21 cm Depths: Hole C0006E = 27.23-406.95 m CSF and Hole C0006F = 395.00-449.67 m CSF Age: Pleistocene Unit II is divided into four subunits based mainly on variations in silt and sand content (Fig. **F3**; Table **T3**). Lithologic variations in the cores, however, do not precisely correspond to these arbitrary or gradational divisions, and it was considered more appropriate to group them into a single unit with a general coarsening upward trend relating to a progressive increase in silt and sand content upsection. A similar coarsening upward trend is noted in the accreted trench deposits of the Nankai margin described by Moore and Karig (1976). The large variations in X-ray diffraction (XRD) data throughout this section (Tables **T4**, **T5**) can be partially attributed to the varied lithologies sampled (sand to silty clay; Figs. **F3B**, **F4**).

Unit II is also structurally complex, with numerous thrust faults causing significant repetition of the sequence (see "Structural geology" and "Biostratigraphy"). Although the exact positions of these faults are uncertain, they have been tentatively placed on the summary stratigraphic section (Fig. F3).

Subunit IIA (sand-dominated trench wedge)

Interval: Sections 316-C0006E-4H-3, 20 cm, through 12H-2, 10 cm Depth: Hole C0006E = 27.23–72.06 m CSF Age: Pleistocene

The dominant lithology of Subunit IIA is dark gray to black fine-grained sand consisting of metamorphic and volcanic lithic fragments with secondary quartz and feldspar. Individual beds are generally 1–7 m thick and massive, although any original sedimentary structures may have been destroyed by coring. Sand typically grades upward into silt and locally silty clay with indistinct boundaries between the different lithologies. Sand beds have sharp bases (Fig. **F5**). Silty clay interbeds are typically <1 m thick with minor sandy silt and clayey silt intervals also present.

Clay content ranges from 28.5% to 55% and averages 42%. Quartz content ranges from 20% to 29% and averages 24.1%, and plagioclase ranges from 21% to 46% and averages 33%. Calcite in this unit is below detection by XRD in most samples (only four samples contain calcite), ranging up to 3% (Fig. F4).

The high sand content of this subunit is suggestive of an axial channel deposit.

Subunit IIB (mixed sand-mud trench wedge)

Interval: Sections 316-C0006E-12H-2, 10 cm, through 24X-1, 0 cm Depth: Hole C0006E = 72.06–163.33 m CSF Age: Pleistocene

Subunit IIB consists of interbedded fine-grained sand, silty sand, and silty clay in approximately



equal abundances. The sand content of this subunit is markedly diminished compared to overlying Subunit IIA (Fig. F3B). Dark gray fine-grained sands and dark olive-gray silts are dominated by metamorphic and volcanic lithic grains with secondary quartz (averaging 25% by XRD) and plagioclase (averaging 31% by XRD), although the proportion of lithic fragments decreases in very fine sand and silt. Sand beds are typically normally graded with indistinct upper boundaries that grade into silty clay. The silty clay is greenish gray and is only slightly bioturbated or mottled in places. Carbonate content is below detection by XRD. Minor ash and carbonate-cemented tuff exist in the upper portions of this subunit (see description of carbonate-cemented ash below). Interpretation of this subunit was hampered by poor core recovery, possibly indicating substantial loss of the sand units shown by LWD logs (see the "Expedition 314 Site C0006" chapter).

Subunit IIC (mud-dominated trench wedge)

Interval: Sections 316-C0006E-24X-1, 0 cm, through 48X-1, 0 cm Depth: Hole C0006E = 163.33–391.33 m CSF Age: Pleistocene

The dominant lithology of Subunit IIC is greenish gray silty clay and minor lithologies include normally graded silt, sand, and rare ash. Within the coarser siliciclastic beds, silt is generally more abundant than sand, particularly when compared to Subunit IIA (Fig. F3B). The silty clay is slightly bioturbated and mottled in places, with local Chondrites burrows. Sand and silt beds are typically graded with indistinct upper boundaries and commonly exhibit parallel laminae and locally well-formed crosslaminae. They are typically 5–25 cm thick, although sand beds up to 5 m thick have also been identified (with their tops at 230, 247, 326, and 369 m CSF). The lowermost of these contains abundant organic matter and wood fragments (up to 50%) with individual fragments up to 3 cm across (Fig. F6). This bed coincides with the base of a significant fault and shows various structures indicating sand remobilization and injection.

Compositionally, this subunit is similar to Subunit IIB with the exception of a slightly greater calcite content (ranging from 0% to 12% and averaging ~1%) as determined by XRD.

Subunit IID (deep marine basin to muddominated trench transition)

Intervals: Sections 316-C0006E-48X-1, 0 cm, through 49X-CC, 21 cm, and 316-C0006F-1R-1, 0 cm, through 7R-CC, 33.5 cm Depths: Hole C0006E = 391.33–406.95 m CSF and Hole C0006F = 395.00–449.67 m CSF Age: Pleistocene

The dominant lithology of Subunit IID is greenish gray silty clay, and minor lithologies include silt and ash. Silt layers are thin-bedded; they are relatively rare in this section and absent below 405 m CSF. Sand beds are completely absent from this subunit. Ash layers are relatively abundant in comparison with overlying units (Fig. F7). The silty clay typically exhibits green (glauconitic?) color bands, which increase in frequency toward the base of the subunit. Mottling and slight to moderate bioturbation are common, but positive identification of Chondrites burrows is limited to the upper part of the subunit. A pronounced increase in the relative abundance of calcite in the XRD data (up to 13%; Fig. F4) appears to correspond to a zone of abundant foraminifer tests in the core (up to 8% in smear slides) in the lowermost part of the subunit.

Except for minor variations in calcite content, Subunits IIB, IIC, and IID manifest no prominent depthdependent or age-dependent trends in composition as determined from XRD (Fig. F4). X-ray fluorescence (XRF) analysis was applied to a subset of samples spanning these three subunits in an effort to find compositional trends related to the clay fraction (see "X-ray fluorescence" in the "Expedition 316 methods" chapter). Variations in the silt/clay ratio potentially provide a source of elemental variation that is large enough to mask trends related specifically to clay minerals, so the sample set for XRF (33 samples) was selected to include only a narrow range in the total clay content (48.0%-54.0% clay minerals). Despite this effort to constrain sources of elemental variation, no depth trends were detected in 10 of the 11 elements analyzed. Only P (Fig. F8) shows a subtle decreasing trend with depth that may reflect decreasing environmental oxygenation in areas more remote from persistent bottom currents, an interpretation that is consistent with the abundant pyrite observed in deeper mudstones.

Unit II is interpreted as having been deposited in a trench setting, with increasing proximity to the axial portion of the trench upsection.

Unit III (deep-marine basin)

Interval: Sections 316-C0006F-7R-CC, 33.5 cm, through 23R-CC, 21 cm Depth: Hole C0006F = 449.67–603.00 m CSF Age: early Pleistocene–late Miocene

Unit III is 140.06 m thick (Fig. F3; Table T3), although this thickness is exaggerated by repetition of parts of the unit along thrust faults (see "Structural



geology"). The unit (Fig. F9) consists of greenish gray to grayish silty clay with some interbedded volcanic tuff layers, including dolomite-cemented and calcite-cemented ash (see below). Bioturbation is widespread, particularly in the upper part of the unit with Zoophycos, Chondrites, other types of burrows, and color mottling. Green color bands are also abundant in the upper part of the unit. The silty clay consists mainly of clay with quartz, feldspar, and minor to rare calcareous nannofossils. Clay content of the silty clay (averaging 51% for the unit) increases downhole, and its color changes from greenish gray (Fig. F9A) to gray at 561.5 m CSF (Fig. F9B). Unit III has an overall increased clay mineral content and decreased quartz and feldspar content (averaging 22% and 25%, respectively) compared to overlying Subunit IID (Fig. F4). Volcanic ash layers are white to light gray, at least partly laminated, with sharp lower and diffuse upper contacts, and are locally burrowed. They consist mainly of glass with minor pumice, quartz, feldspar, and calcareous nannofossils.

Unit III was deposited by hemipelagic settling along with accumulation of volcanic ash during major volcanic eruptions. The stratigraphic position of Unit III is below the trench-wedge facies of Unit II. Its early Pleistocene–Miocene age and overall lithologic content are consistent with deposition in the Shikoku Basin. Similar deposits have been documented at Ocean Drilling Program Sites 808, 1173, and 1174 in the Muroto transect over 100 km to the westsouthwest along the Nankai Trough (Shipboard Scientific Party, 2001a, 2001b; Moore et al., 2001).

Diagenesis

Overall, diagenetic effects observed at this site correspond almost entirely to mechanical processes, an unsurprising result given that the maximum temperature in the deeper portions of Site C0006 is not expected to exceed 40°C (see "**Physical properties**"). Even allowing for uplift, the detrital feldspar and clay mineral assemblages at these temperatures are expected to provide reasonably faithful records of provenance information. Volcanic glass observed at this site is water-clear in transmitted light and shows no discernible evidence of alteration at the scale of smear slide observation.

Only minor evidence of chemical diagenesis could be detected at this site using macroscopic core observation and smear slides. Pyrite in the form of framboids, pyritized burrows, and small (<1 cm) nodules is distributed widely through the mudrocks in all of the units and is appreciated most fully in X-ray CT images.

Occurrences of ash cemented by calcite or dolomite were also encountered. Most samples of this material

were discovered as pieces of relatively lithified rubble in the tops of cores (Table T6). Two possible in-place occurrences of this lithology are in Sections 316-C0006F-12R-1, 7-32 cm, and 13R-2, ~45-52 cm. A second less certain in-place occurrence is in Section 316-C0006F-20R-1, 10–12 cm. XRD analysis indicates that the nonash component of these rocks consists of either dolomite or calcite with minor amounts of clay, quartz, and feldspar. Measurements of resistivity and velocity in one sample (rubble collected from Section 316-C0006E-46X-1) indicate values far in excess of that observed for normal silty clay (8 cm³ cube; $3.0 \times 1.9 \times 3.3$ kΩ; ~5.1 km/s Pwave velocity; see "Physical properties"). Resisitivity logs (see the "Expedition 314 Site C0006" chapter) show thin intervals of extremely high values and associated low gamma ray intensity that may correspond to this lithology. Further clues about the distribution of authigenic carbonate come from the drillers who reported informally having encountered extremely hard but thin layers. In thin section the dolomite appears as microcrystalline cement in wellsorted, little-compacted, and very pure volcanic ash (Fig. F7C). Millimeter-scale laminations correspond to different compactional states of the ash particles.

A third minor instance of chemical diagenesis was observed in Section 316-C0006F-19R-1, 91 cm (dark gray mud of Unit III). A minute sand concentration (most likely an agglutinate test) was examined in smear slide and discovered to contain an abundance of 2–10 μ m bladed crystals having low relief and extremely low birefringence (Fig. F10). These small crystals are very tentatively identified as the zeolite phillipsite.

X-ray CT number

X-ray CT images were used extensively by the science party for evaluation of sedimentological and structural features. Figure F11 shows the depth trends for CT number (averaged pixel intensity for a 1 mm² area) determined for coherent pieces and tectonic breccia clasts of silty clay. CT number reflects the average sample density at the scale of the CT observation, a value that is affected by sample composition (mineral composition and density) and porosity (bulk density), although in these porous samples, it is largely dominated by porosity. Across Unit I through Subunit IIC, CT number increases with depth. CT number decreases gradually from 1450 to 1300 between lower Subunit IID and upper Unit III. The lowest value of 1300 in this section is shown at 480 m CSF, and CT number recovers to 1450 at 530 m CSF. This relatively low CT number zone is consistent with the lower mud-dominant part of the site.



Structural geology

Various deformation structures were observed in cores and X-ray CT images from Holes C0006E and C0006F. Figure **F12** summarizes the structural observations. All structural data are given as supplementary material (see C0006_STRUCT_DATA.XLS in folder 316_STRUCTURE in "Supplementary material").

Bedding and fissility surface attitude and evolution with depth

Among the 174 measurements of bedding surface attitudes obtained by visual inspection of cores, 126 were corrected for true magnetic north using paleomagnetic data. Thirty one measurements are relevant to lithologic Unit I (trench to slope sediments, between 0 and 27 m CSF). The remaining 95 measurements pertain to the accretionary prism sediments crossed between 27 and 600 m CSF. Of a total of 65 fissility measurements, 63 can be used with good reliability. All fissility measurements were obtained in the accretionary prism sediments at depths >100 m CSF (Fig. F12). Figure F12 shows a clear decrease of the dip angles of bedding surfaces and fissilities with increasing depth, from up to 75° to 30° or less. A similar change of bedding dip angle versus depth was also obtained from analysis of LWD data (see "Structural geology" in the "Expedition 314 Site C0006" chapter).

Most bedding surfaces in slope sediments strike north-south to northwest-southeast and dip westward (Fig. F13A). Strikes of bedding or fissility surfaces in accretionary prism sediments (below 27 m CSF) are variable and no preferred direction is apparent (Fig. F13B, F13C).

Deformation in lithologic Unit I

Trench to slope transition sediments of lithologic Unit I are poorly consolidated. Between 15 and 35 m CSF, they are affected by normal faults striking north–south to northwest–southeast and dipping steeply (Fig. **F14**) with offsets <10 cm. Because of poor consolidation, fault surfaces could not be separated in order to allow examination of possible striations. Between 28 and 31 m CSF, which is slightly below the normal fault interval, the sediments are cut by two reverse faults showing very small offsets (<1 cm).

Deformation structures within the fractured/brecciated zone

Visual core description (VCD) and CT images allow us to distinguish a broad fractured/brecciated zone extending from 230 to 545 m CSF in which fracture density and intensity is highly variable (Fig. F15). This zone differs from the sections above or below with the following characteristics:

- 1. Coherent pieces of cores are short, usually not exceeding one section (~1.4 m).
- 2. Cores are commonly strongly fractured.
- 3. Striated or polished planes are common.
- 4. The zone contains intervals of breccias that are unambiguously of tectonic origin.

By contrast, the sections above or below this fractured and brecciated interval are more coherent, less fractured, and generally do not include tectonic breccias. The transition between the fractured/ brecciated zone and the underlying section appears rather sharp.

Minor faults

Within the fractured/brecciated zone defined above, minor faults of various types can be observed on cores, as well as on CT images.

CT images were used to investigate the fault geometry and offsets that existed prior to whole-round sampling and cutting. Figure **F16** shows a CT image of a fault displacing worm tubes with a normal offset of ~1 cm. Visually, this fault displays parallel lineations, and the faces of the fault are mated. That the worm tubes are displaced when the fault surfaces are mated strongly suggests that the fault is natural. Paradoxically, this normal fault strikes approximately perpendicular to the maximum principal horizontal stress (σ_{Hmax}) direction inferred from borehole breakouts (see "**Structural geology**" in the "Expedition 314 Site C0006" chapter).

Within the fractured/brecciated zone recognized above, dip angles of faults are scattered but clusters around 60° tend to dominate (Fig. F12). Fault plane strikes do not show any preferred direction (Fig. F17). Minor faults are characterized by striated and/ or polished surfaces or by offset markers. The sense of displacement is given by the offset of markers or, most commonly, by steps borne by the surface. Of the 220 observed faults, normal faults are the most frequent (42%), followed by reverse faults (12%) and left-lateral (10%) or right-lateral (10%) faults. The remaining faults (26%) have undetermined or ambiguous senses of displacement. Preliminary kinematic analysis of populations of normal faults, reverse faults, and strike-slip faults has not yielded consistent results, implying that fault-slip data sets are not homogeneous (Fig. F17). Additional sorting is clearly needed in order to define homogeneous subsets.

Fractures without displacement

The distinction between natural fractures and drilling-induced fractures is not easy at Site C0006. A



fracture that can be followed across several "parted" ("biscuited") core segments and that spans a distance greater than the borehole diameter is likely a natural fracture. Indeed, propagation of a fracture along the core is likely to stop at parting surfaces. The presence of plumose structures on fracture surfaces also supports natural propagation. A convincing example of such a tectonic fracture is found in interval 316-C0006F-18R-1, 70-125 cm. The surface of this fracture shows well-preserved plumose structures (Fig. F18) that clearly indicate a pure mode-I opening that initiated at some distance from the core and propagated approximately horizontally. Moreover, this fracture strikes parallel to the direction of σ_{Hmax} inferred on the basis of borehole breakouts in Expedition 314 (see "Structural geology" in the "Expedition 314 Site C0006" chapter); hence it is not drilling induced. However, when fractures are of small size (less than three times the core diameter) and lack plumose structures, there remains much ambiguity regarding the origin of the measured planes.

Deformation bands

Visually, deformation bands appear on cores as undulating bands that are darker than the host rock. Shear (tangential displacement) along deformation bands is established in several instances by offset markers. Deformation bands are visually observed in cores between 300 and 460 m CSF with a clear predominance between 300 and 405 m CSF (Fig. F12), which is within the fractured/brecciated zone mentioned above. Most deformation bands dip more steeply than 30°, and the sense of shear is reverse (Fig. F19). Figure F20 shows the equal-area projection of deformation bands for which paleomagnetic correction is reliable. These bands predominantly strike about northeast-southwest and dip either northwestward or southeastward, forming two sets with an apparent conjugate geometry. Each set was fitted by a mean plane, and the obtuse dihedral angle between the two mean planes is ~97°. The bisecting plane of this angle strikes ~48° and is almost vertical. Given the reverse sense of slip observed along these deformation bands, this geometry suggests a shortening axis oriented horizontal along 138°. A similar direction of shortening was previously deduced from deformation bands in the Muroto transect in the Nankai accretionary prism (Ujiie et al., 2004).

Deformation bands appear as bright bands in CT images. The CT number for deformation bands is often ~100 greater than that of the surrounding rock and likely reflects densification within the bands. A systematic search of CT images over the depth interval from 160 to 400 m CSF (Fig. F21) confirms the heterogeneous density distribution of bands determined by visual inspection.

Combined VCD and CT image analyses indicate that deformation bands are concentrated between 240 and 400 m CSF. The lower density of deformation bands below 400 m CSF may also be explained by a lithologic change because deformation bands tend to be developed in mudstones which lack bioturbation. Below 400 m CSF, the sedimentary pile is dominated by bioturbated mudstone. Bioturbation may prevent deformation bands from forming, possibly because of a random reorganization of initially well aligned clay particles.

Sediment-filled veins

Sediment-filled veins (vein structures) are uncommon at Site C0006. The clearest examples were observed at six locations between 395 and 510 m CSF. Sediment-filled veins are planar or sigmoidal. One occurrence shows sediment-filled veins displaced in a reverse sense by deformation bands (Fig. F19C).

Sand injection

Sand injection cut by biscuiting boundaries associated with ESCS coring can be observed at 370.18 m CSF. Injection is either vertical (sand dike, Fig. F22) or horizontal (sand sill). Boundaries with the host rock are sharp and planar or irregular. The injected sand is medium to coarse grained, and is well sorted. It is homogeneous except for elongated wood fragments that can reach 1 cm in length. No internal structure can be recognized in the filling.

Definition of zones of concentrated deformation within the fractured/ brecciated zone

The distribution of structural elements in the fractured/brecciated zone is shown in Figure F23. Core and thin section observation and CT image analysis allow us to define several intervals within the fractured/brecciated zone that appear significantly more deformed than the background (and that could be interpreted as faults). Because the whole zone is affected by tectonic fracturing as well as by drillinginduced disturbance, the definition of deformed intervals was based on all possible observations and will be further tested by onshore studies. Key observations that, taken together, allow us to define these intervals are

- 1. The presence of fault rocks such as breccia or gouge;
- 2. The presence of strongly fractured intervals (by strongly fractured, we mean that the intact core segments, if any, have lengths smaller than the



core diameter because of natural fracturing [biscuiting excluded]);

- 3. The presence of discontinuities of any type, such as abrupt changes in lithology, fracture, or deformation band intensity; and
- 4. A progressive change that leads to locally high density and/or preferred orientation of fabric elements, such as deformation bands and fractures, commonly associated with faults.

Based on these criteria, the following intervals appear as concentrated zones of deformation:

- 235–243 m CSF (Cores 316-C0006E-31X through 32X),
- 277–297 m CSF (Core 316-C0006E-36X through the top of 38X),
- 367.5-369.5 m CSF (Core 316-C0006E-45X),
- 433.75–440.00 m CSF (Cores 316-C0006F-5R through 6R), and
- 526–545 m CSF (Cores 316-C0006F-15R through 17R).

The 433.75–440.00 m CSF interval coincides with a biostratigraphic hiatus whose origin is still undetermined (see "**Biostratigraphy**").

235–243 m CSF (Cores 316-C0006E-31X and 32X)

On the basis of CT image measurements, linear density of deformation bands increases with depth from 210 m CSF to a maximum of 21 bands/m in Section 316-C0006E-32X-1 (Fig. F21). Linear density of deformation bands decreases abruptly in the middle of Section 316-C0006E-32X-2 and then remains low downhole through Section 316-C0006E-32X-5. Fracturing also progressively increases in intensity with depth through Core 316-C0006E-31X, displays maximum intensity in intervals 316-C0006E-32X-1 and 32X-2, and decreases through Section 316-C0006E-32X-5. Locally in Sections 316-C0006E-31X-5 through 32X-2, finely fractured rocks are evident where fracture spacing is <1 cm and the fractures display strong preferred orientations. On the basis of VCDs, these intervals are classified as highly fractured rocks.

A prominent fracture surface in Section 316-C0006E-31X-5 (235.30 m CSF) juxtaposes two fractured units with contrasting CT numbers (Fig. F24). With a correction based on paleomagnetic data, the surface is oriented 043°, 29° southeast, which is approximately parallel to one of the preferred orientations of deformation bands with reverse sense of shear and thus is compatible with regional northwest–southeast contraction.

277-297 m CSF (Core 316-C0006E-36X)

Core 316-C0006E-35X is characterized by unbroken mudstone in which subhorizontal bedding and fissility are well preserved. At 277.39 m CSF (Section 316-C0006E-36X-1, 6 cm), a network of anastomosing fractures cuts the subhorizontal layering (Fig. F25A). Below this depth, fractured and brecciated mudstones are observed throughout Core 316-C0006E-36X (Fig. F25B). The fracture sets are spaced as little as a few millimeters apart and have an anastomosing geometry, suggesting incipient brecciation (protobreccia). Brecciated fragments are centimeter to millimeter size with distinctly polished and slickenlined surfaces. Mudstone tends to be brecciated along the sets of inclined and subhorizontal surfaces, showing a foliated aspect. The abrupt occurrence of millimeterspaced anastomosing fracturing and brecciation across the top of Core 316-C0006E-36X constitutes a significant discontinuity that could correlate to a fault surface.

367.5-369.5 m CSF (Core 316-C0006E-45X)

Core 316-C0006E-44X and Sections 316-C0006E-45X-1 through 45X-5, 35 cm, are dominated by fractured mudstones. Interval 316-C0006E-45X-5, 35 cm, through 45X-6, 71 cm, is characterized by breccia, including centimeter- to millimeter-sized fragments that are ubiquitously polished and striated (Fig. F26A). At 369.18 m CSF (Section 316-C0006E-45X-6, 71 cm), a subhorizontal surface parallel to bedding/ fissility separates the brecciated interval above from the coherent interval below (Fig. F26B). Below this depth, original layering of sands and mudstones are well preserved and sands locally intrude into mudstone (see above, sand injection), which in turn are cut by biscuiting boundaries. The change in deformation style from fractured mudstone to breccia with depth and the prominent boundary between breccia and unbroken sands and mudstone layers at 369.18 m CSF suggest the presence of a fault.

433.75–440.00 m CSF (Cores 316-C0006F-5R and 6R)

Following Cores 316-C0006F-3R and 4R, which consist of ~4 m of highly fractured rock of unknown origin (tectonic, drilling-induced, or splitting-induced), Core 316-C0006F-5R includes coherent pieces of mudstones (interval 316-C0006F-5R-1, 0–73 cm) underlain by highly fractured mudstones nearly 2 m thick. Fragments have sizes <1 cm and commonly show polished/striated surfaces. The presence in interval 316-C0006F-5R-CC, 4–23 cm, of a piece of tectonic breccia (Fig. F27) is consistent with the presence of a major fault nearby. Core 316-C0006F-6R is



similar to the above-lying Core 316-C0006F-5R. It consists of 2 m of highly fractured mudstones with ~20 cm of tectonic breccia in the core catcher, confirming deductions from Core 316-C0006F-5R.

526–545 m CSF (Cores 316-C0006F-15R through 17R)

Section 316-C0006F-15R-3 shows a downhole increase in brecciation intensity. At 526.51 m CSF (Section 316-C0006F-15R-3, 48 cm), breccia is replaced by microbreccia (most brecciated fragments are <1 mm in size), which in turn changes to fault gouge at 526.65 m CSF (Fig. F28A). The thickness of the gouge zone is 8 cm. Careful observation of fault gouge both in core and thin section reveals that fault gouge is locally foliated, preserving composite planar fabric associated with shear (Fig. F28B). Below the gouge zone, breccia occurs again in Cores 316-C0006F-16R (Fig. F28C) and 316-C0006F-17R. Core 316-C0006F-18R is characterized by jointed mudstone with little or no evidence of brecciation.

Deformation below the fractured/ brecciated zone

Sediments found in the 545–603 m CSF interval, which consist of bioturbated hemipelagic mudstones (lithologic Unit III), are less fractured or brecciated than above 545 m CSF. Dip angles of fault planes are scattered between 20° and 88°, but steep angles predominate (Fig. F12). No preferred orientation of fault plane directions can be recognized. Among these faults, normal faults predominate (Fig. F29).

Discussion

The five intervals described above appear more deformed than the surrounding cores. In particular, they all include tectonically brecciated intervals recognized either visually or by relying on CT images. These five intervals are interpreted as faults within the fractured/brecciated zone. Such interpretations remain hypothetical, partly because of the generally poor recovery near the considered intervals. Keeping in mind these uncertainties, it is then possible to propose correlations between these fault intervals and the reverse faults recognized on seismic lines passing nearby Holes C0006E and C0006F (Fig. F30; see Moore et al.).

Conclusion

Despite poor recovery and drilling- or splittinginduced disturbance, CT scan image analysis and visual examination of cores from Holes C0006E and C0006F allow us to define a broad fractured/ brecciated zone that includes at least five intervals of concentrated deformation. The presence of these five intervals shows that deformation is not evenly distributed along the whole fractured/brecciated zone but is localized along narrow zones corresponding to faults, as suggested by seismic reflection profiles. Because of poor recovery, it is impossible to propose a typical thickness of fault core and damaged zone for any of the five recognized faults.

Biostratigraphy

Four holes were drilled at Site C0006 into the toe of the Nankai accretionary prism during Expedition 316. Only one core each was retrieved in Holes C0006C and C0006D. Hole C0006E was cored from the seafloor to 406.97 m CSF through slope sediments and into the sediment inferred to have been the marginal trench wedge deposits. Hole C0006F was cored from 390 to 603 m CSF in the lower part of the thrusted trench deposits into the upper part of Shikoku Basin sediments.

The biostratigraphy determined for Site C0006 is based on examination of calcareous nannofossils, radiolarians, and foraminifers from Holes C0006E and C0006F. In addition, a few samples from C0006F were analyzed for diatoms.

Calcareous nannofossils

Sediments recovered from Holes C0006E and C0006F are dominated by interbedded sand layers and volcanic ash layers in turbidite sequences (see "Lithology"), yielding few to rare and moderately to poorly preserved nannofossils in most samples from core catchers and within cores. This lack of nannofossils results in difficulties establishing a biostratigraphy. At least three difficult issues are merged: scarcity of nannofossils, poor preservation, and reworking.

A number of nannofossil samples were carefully selected from thin clay or particular ash layers within cores that contain relatively abundant and moderately preserved nannofossils (Tables **T7**, **T8**).

Problems due to poor preservation still exist. A case commonly seen in many samples is that only largesized nannofossils were preserved in sediments, whereas most small-sized species were lost. That is, the nannofossil assemblages found in sediments were changed by various processes, probably by dilution during turbidite flow, breakage by stress of deformation, and dissolution. These changes result in difficulties in finding and identifying event markers or in distinguishing them from species that are morphologically similar. Uncertain determination of species is indicated with a "?" in Tables T7 and T8.



These uncertain data will be improved through shore-based study.

Reworking is very common throughout the sediment sequence recovered in Holes C0006E and C0006F, leading to confusion in the determination of a number of last occurrence (LO) events. To solve this problem, the co-occurrences of other age-diagnostic specimens or the nannofossil assemblages were examined in detail to make a reliable determination. For example, a few Reticulofenestra asanoi and Calcidiscus macintyrei were observed in the uppermost two cores of Hole C0006E (Table T7). Observations of nannofossil assemblages in this interval suggest that the assemblages are dominated by Gephyrocapsa carribeanica in the medium-sized Gephyrocapsa groups (Gephyrocapsa spp. medium I and II). The first occurrence (FO) of this species was estimated at 0.76 Ma (Su, 1996). Therefore, the presence of R. asanoi and C. macintyrei in samples from these two cores was considered to be due to reworking.

A total of 17 nannofossil biostratigraphic events were recognized (Table T9). The presence of Emiliania huxleyi in Samples 316-C0006E-1H-CC and 2H-1, 34 cm, was not determined with high confidence because of the small size of this species and poor preservation. However, correlation with geomagnetic data in the same hole suggests that these samples are younger than 0.29 Ma. Therefore, the transition (X) from Gephyrocapsa spp. (>3.5 µm) to E. huxleyi was placed at 5.16 m CSF and the FO of E. huxleyi was placed at 5.19 m CSF, marking the bottom of Zone NN21 at this horizon. Common Pseudoemiliania lacunosa occurs in Sample 316-C0006E-3H-4, 79 cm, which was taken as its LO to mark the boundary between nannofossil Zones NN20 and NN19 (0.436 Ma), whereas its rare presence in samples above 15.22 m CSF is attributed to reworking.

The subdivision of Zone NN19 was difficult in Holes C0006E and C0006F, as nannofossil assemblages in most samples were significantly affected by the presence of large amounts of reworked fossils younger than Zone NN19, dilution by turbidite flow, and dissolution. Two separate intervals (from 73.35 to 85.54 m CSF and from 192.45 m CSF to the bottom of the hole) in Hole CO006E contain R. asanoi (LO = 0.9 Ma and FO = 1.078 Ma); however, the interval between 85.54 and 192.45 m CSF contains frequent Gephyrocapsa spp. large (>5.5 µm) and common C. macintyrei with co-occurrence of Helicosphaera sellii, suggesting an earlier Zone NN19 age for this interval (Table T7; Fig. F31). Common medium-sized *Gephyrocapsa lumina* (a typical early Pleistocene species) are also present, indicating an early Pleistocene assemblage. The nannofossil data obtained during shipboard analyses support the assumption that the sedimentary sequence within the occurrence range of *R. asanoi* contains at least one age reversal and possibly one or more minor or poorly defined age reversals. With this assumption, we propose a preliminary subdivision of Zone NN19 into three parts for Site C0006:

- 1. Normal Zone NN19 from 17.22 to 72.90 m CSF in Hole C0006E.
- 2. A possible repeated Zone NN19 in the middle part of Hole C0006E.
- 3. Normal Zone NN19 from 192.45 to 406.92 m CSF in Hole C0006E and from 396 to 496 m CSF in Hole C0006F (Table **T7**; Fig. **F31**).

Subsequently, a number of nannofossil events were determined for further subdivision of these parts of Zone NN19 (Table T9). Within the repeated part of Zone NN19, a short younger interval marked by the presence of R. asanoi in Sample 316-C0006E-24X-1, 96 cm (164.29 m CSF), is noted (Tables **T7**, **T9**). This sample was collected from Section 316-C0006E-24X (not a core catcher sample) and contains rare to frequent R. asanoi, which was confirmed by careful examination of several slides from the same sample. This sample contains a mix of younger and older species. Common to frequent Gephyrocapsa spp. $(\geq 4 \ \mu m)$ (reentrance [RE] = 1.04 Ma) and common C. macintyrei (1.6 Ma) together with a few Gephyrocapsa spp. large (>5.5 µm; 1.617 Ma) were observed, implying a possible contact boundary of older and younger sediments, possibly due to faulting. This sample (164.29 m CSF) is located near a change in lithology. Therefore, we consider the occurrence of *R*. asanoi to be an indication of a short age reversal (>0.9 to <1.04 Ma) in the repeated Zone NN19 sequence in Hole C0006E. At the bottom of Hole C0006E, the RE of *Gephyrocapsa* spp. ($\geq 4 \mu m$) at 391 m CSF is comparable to the RE of Gephyrocapsa spp. ($\geq 4 \mu m$) at 396 m CSF in Hole C0006F, providing consistent evidence from both holes. Four events, including the RE of *Gephyrocapsa* spp. (≥ 4 um), were available for subdivision of Zone NN19 sediments in Hole C0006F (Table T9).

Nannofossils below 434.71 m CSF were very poorly preserved, and a number of samples were barren of nannofossils (Table **T8**). Most nannofossil records were obtained from carefully selected thin clay intervals, ash layers, or ash pods within cores. These records allow identification of event markers and subdivision of the lower part of Hole C0006F into a sequence from middle Pliocene Zone NN16 to upper Miocene Zone NN12 (Table **T9**). The bottom of the repeated Zone NN19 interval, marked by the bottom of the first consistent occurrence (FCO) of *Gephyrocapsa* spp., was truncated by a number of late Pliocene events: the LOs of *Discoaster brouweri* (marker of Zone NN18), *Discoaster pentaradiatus* (marker of Zone



NN17), and Discoaster surculus (marker of Zone NN16) at 459.01 m CSF (Tables T8, T9), indicating the absence of the lower part of lower Pleistocene Zone NN19, upper Pliocene Zone NN18, and Zone NN17. A truncation in the same time interval was also observed at Site C0004 (see "Biostratigraphy" in the "Expedition 316 Site C0004" chapter); however, we are unable to explain the possible correlation at the present time. The sediment sequence from 459.01 to 485.88 m CSF was assigned to middle Pliocene calcareous nannofossil Zone NN16 based on the co-occurrence of D. surculus (marker of top of Zone NN16) and D. tamalis, as well as on the absence of Reticulofenestra pseudoumbilicus (>7 µm) (marker of top of Zones NN15–NN14) (Table T8). The recognition of the LO of Sphenolithus spp. at 476.98 m CSF provides subdivision of this zone. The interval from 487.67 to 505.42 m CSF was assigned to lower Pliocene Zones NN15-NN13 with its top marked by the LO of R. pseudoumbilicus (>7 µm) and its bottom marked by the FO of Ceratolithus rugosus (marker of boundary of Zone NN13/NN12). Zones NN15-NN13 could not be further subdivided in Hole C0006F because of the trace or sporadic presence of Discoaster asymmetricus (marker of base of Zones NN15–NN14) in Hole C0006F. The absence of Discoaster quinqueramus (marker of top of Zone NN11; LO = 5.59 Ma) from the whole sequence of Hole C0006F suggests that the interval from 507.53 m CSF to the bottom of the hole is within Zone NN12 and younger than 5.59 Ma (Table T8). The lowest occurrence of Ceratolithus acutus at 580 m CSF (FO = 5.32 Ma) was the only possible event marker identified for the long interval of Zone NN12.

Other microfossil groups

All core catcher samples were processed for radiolarian analysis, but most of them were barren. Sample 316-C0006E-1H-CC revealed a poorly preserved assemblage with apparent breakage. A few undiagnostic or nonidentifiable diatom frustules and fragments were found within the section to Core 316-C0006E-13H.

Planktonic foraminifers occur sporadically to Core 316-C0006E-11H (71.38 m CSF). However, abundant *Pulleniata finalis* were found in a horizon in Section 316-C0006F-6R-1, 100 cm (439 m CSF), indicating an age younger than 2.06 Ma.

A few discrete horizons within cores were also sampled for diatoms and radiolarians, but those that were not barren revealed only very rare broken specimens.

Summary and correlation to faults

Based on the nannofossil record at Site C0006, 17 nannofossil biostratigraphic events were recognized

and assigned an age of upper Miocene Zone NN12 to Pleistocene. The uppermost part of Zone NN21 might include a thin sediment layer of Holocene age. This is undeterminable based on nannofossil biostratigraphy. Plots of age versus depth in Holes C0006E and C0006F are combined with magnetostratigraphic results in Figure F31.

An age repetition interval was identified within Zone NN19; the occurrence range of R. asanoi in Zone NN19 may contain one or more repetitions within the sequence from 85.54 to 185.39 m CSF in Hole C0006E. There is also some inconclusive evidence for either a hiatus or an erosive event within this interval; however, shipboard data were insufficient to clarify nannofossil stratigraphy at this level of detail. This repetition is probably caused by faulting, in agreement with the lithologic Subunit IIB/IIC boundary. It is also possible that the "older" age assignment was affected by the presence of a large number of reworked older fossils and a lack of sufficient nannofossil data because of poor preservation. This will be improved through postcruise study. A short time gap of ~0.17 m.y. was found between 434.71 and 439.50 m CSF (Table T8; Fig. F31).

The bottom of repeated Zone NN19 sediments is truncated by middle Pliocene Zone NN16 sediments at 449.70 m CSF in Hole C0006F, indicating a time gap of ~1 m.y. Abundant planktonic foraminifers *P. finalis* (<2.06 Ma) found in Sample 316-C0006F-6R-1, 100 cm (439 m CSF), provide evidence for this age estimate. The time gap in Hole C0006F is consistent with the lithologic Unit II/III boundary. Unit III sediments were subdivided into middle–lower Pliocene Zone NN16, Zones NN15–NN13, and upper Miocene–lower Pliocene Zone NN12.

Results from seismic and structural studies at Site C0006 suggest several faults below 230 m CSF (see "Structural geology"). More detailed examination of nannofossil records from samples within these fault zones reveals poor preservation, indicating mechanical reworking and/or chemical degradation. For example, more nannofossil debris was observed in Samples 316-C0006E-45X-CC, 316-C0006F-6R-CC, and 17R-CC, whereas nannofossils have overgrown features in Samples 316-C0006F-31X-CC and 36X-CC (see the five zones of deformation in "Structural geology"). The short time gap between 434.71 and 439.50 m CSF (Table T8; Fig. F31) can be correlated to the possible fourth fault zone (see "Structural geology"). In addition, a difference between the upper and lower parts of the repeated interval of R. asanoi (192.48–434.71 m CSF; >0.9 to <1.078 Ma) was noted: nannofossils are moderately preserved above 358 m CSF, whereas they are poorly preserved and sediments contained more common reworked nannofossils below that depth (Tables T7, T8).



Furthermore, two very long sediment intervals covering such a short time span seem unlikely to be solely due to high sedimentation rates: the interval of *R. asanoi* (0.9–1.078 Ma) between 192.45 and 434.71 m CSF and the interval of Zone NN12 between 505.42 and 591.45 m CSF. Considering faults observed in these two intervals, it is reasonable to infer that their thickness might be partially caused by duplication due to thrust faulting.

Paleomagnetism

We made pass-through magnetometer measurements on all split-core archive sections at 5 cm intervals. In order to isolate characteristic remanent magnetization (ChRM), we subjected the cores to alternatingfield (AF) demagnetization. The archive-half cores were typically demagnetized to 40 mT. Before measurement data were uploaded to the J-CORES database, we excluded the top and bottom ~15 cm to avoid end-core edge effects (response of the magnetometer's pickup coils is ~20 cm) as well as those for voids caused by whole-round sampling. In order to test the archive-half core data and identify magnetic carriers, we demagnetized a total of 102 discrete samples using both AF and thermal techniques.

Natural remanent magnetization and magnetic susceptibility

Paleomagnetic data obtained at Site C0006 during Expedition 316 exhibit significant variations in demagnetization behavior among various recovered lithologies. Drilling-induced remagnetization exists in the recovered cores (Figs. F32, F33, F34), but it had less effect compared with those in Hole C0004C sediments. Interestingly, drilling-induced remagnetization in a few cores is of opposite polarity (see Figs. F32, F33B); perhaps a different type of core barrel was used to core these sediments. In almost all cases, we were able to remove drilling-induced remagnetization with 20–30 mT AF demagnetization and to isolate ChRM direction using higher fields.

The most significant variations in natural remanent magnetization (NRM) intensity and susceptibility for whole cores from Site C0006 are well correlated with lithology. Paleomagnetic measurements indicate that mudstones in Unit III have the lowest NRM intensity (averaging ~0.1 mA/m) compared to those in turbidite Unit II (~12 mA/m) and nannofossilbearing mud and sand in Unit I (~2 mA/m). Variations in magnetic susceptibility generally correlate with variations in NRM intensity (Fig. F32). Magnetic susceptibility values are generally ~19 × 10⁻³ SI for sediments in Unit I, >200 × 10⁻³ SI for Unit II, and

 12×10^{-3} SI for Unit III. A few discrete peaks of higher NRM and susceptibility values appear in some depth intervals in Units I and II (e.g., around 18, 27, 161, 231, and 326 m CSF; see Fig. F32) and visibly correlate with the presence of volcanic ash in these regions (see "Lithology").

Paleomagnetic stability tests and core orientation

Remanent magnetization of discrete samples was investigated using stepwise AF or thermal demagnetization (Fig. F33). In most cases, the steep downward component of magnetization imparted by the coring process is easily removed by AF demagnetization. Thermal demagnetization also successfully removed this drilling-induced component (Fig. F34). Most samples show unblocking temperatures between 200° and 400°C, indicating that titanomagnetites are likely the main magnetic carriers in these samples. A histogram of inclinations isolated from discrete samples is shown in Figure F35. Inclinations from archive-half core pieces at <100 m CSF are concentrated at approximately ±45° (Fig. F32), similar to the expected dipole inclination at the site (52°). A pronounced shallowing of inclinations is evident in the interval from ~120 to 380 m CSF, where inclination values are more typically shallower than 30°. This interval corresponds to the observed zones of faulting and fracturing (see "Structural geology"), suggesting that inclination values may have been affected by faulting and tilting. Results from discrete sample demagnetization also provide an opportunity to evaluate the accuracy of archive-half core remanence data that are used (in combination with discrete sample results) to reorient core pieces to a common geographic framework. This paleomagnetic core reorientation method has been successfully used for both continental and oceanic outcrops (e.g., Fuller, 1969; Kodama, 1984; Shibuya et al., 1991). Assuming the direction of stable remanent magnetization (either viscous remanent magnetization or primary magnetization) with respect to a common reference line that is scribed the length of the core represents the expected magnetic direction at the site, the orientation of paleomagnetic ChRM, which specifies the rotation of the core relative to the geographic coordinates, is then used to restore the core azimuth. For intervals of particular interest for structural geology at Site C0006, we used either the stable ChRM isolated from progressive demagnetization of discrete samples and small homogeneous segments (that contain structural features) or an average declination from 3-4 consecutive measuring intervals with the same inclination sign from archive-half core data. The combined data sets suggest that defor-



mation bands in cored units generally strike southwest and dip northwest or southeast (See "Structural geology").

Magnetostratigraphy

We used ChRM inclinations from both pass-through and discrete measurements to define magnetic polarity sequences for Site C0006. As at Site C0004, magnetic polarity sequences at Site C0006 could not be completed because of incomplete recovery and wholeround sampling of archive-half sections. Faulting also affects this site and complicates magnetostratigraphy. Nevertheless, a few magnetic reversals discerned on the basis of changes in sign of inclinations can be identified, which constitute partial magnetostratigraphic records at Site C0006. Biostratigraphic samples between 5 and 10 m CSF in Hole C0006D have been assigned ages of ~0.43 Ma. Thus, the observed predominantly negative inclination in this interval suggests that these sediments were deposited within the Emperor event (0.42 Ma), a short reversed polarity event within the upper part of the Brunhes normal chron (Gradstein et al., 2004). This event is likely recorded in Holes C0006C and C0006E, each ~2.5 m from Hole C0006D, and at Site C0004 (~20 km northwest of Site C0006). If confirmed by further shore-based study, this record could serve as a chronostratigraphic marker to correlate sedimentary layers in the Nankai Trough region.

On the basis of shipboard micropaleontological data, the uppermost 80 m of sediment in Hole C0006E has an age in the range of 0.8-1.1 Ma. The Brunhes/ Matuyama Chron boundary (0.78 Ma) is placed at 32.75 m CSF as magnetic inclination at this depth changes polarity from normal to reversed (Fig. F36). This match is definite because the Matuyama is the only reversed chron of this particular age. Between 145 and 192 m CSF, cores have been assigned to ages ranging from 1.6 to 1.67 Ma (see "Biostratigra**phy**"). Therefore, the shift in polarity from reversed to normal at 160 m CSF would correspond to the onset of the Gilsa Subchron (1.68 Ma), and the upper part of Hole C0006E contains only a partial record of the Matuyama Chron and no record of the Jaramillo Subchron (0.99–1.07 Ma).

Biostratigraphic data suggest that sediments between 200 and 410 m CSF may be 0.8–1.1 Ma in age. This information suggests that the relatively well defined record of a reversed interval between 250 and 345 m CSF and the shift in polarity from reversed to normal at ~345 m CSF represent the upper part of the Matuyama Chron and the onset of the Jaramillo normal polarity subchron and infer a relatively rapid sediment accumulation rate (~180 m/m.y.) for the early Pleistocene in Holes C0006E and C0006F. Alter-

natively, the thickness of the strata could also be due to thrust faulting in the region.

Inorganic geochemistry

The main objectives of the geochemical program at Site C0006 are to

- Characterize in situ biogeochemical reactions;
- Constrain in situ inorganic diagenetic reactions with depth;
- Identify potential deep sourced fluids within fault zones and other permeable horizons, as well as fluid-sediment reactions at the source; and
- Constrain the subsurface hydrology, including fluid flow pathways and possible transport mechanisms.

A total of 71 whole-round samples were collected for interstitial water analyses at Site C0006 (2 samples from Hole C0006C, 2 from Hole C0006D, 46 from Hole C0006E, and 21 from Hole C0006F). Wholeround lengths ranged from 10 to 42 cm with larger subsamples collected from cores recovered deeper within the hole where the sediments were more consolidated. There was no seafloor camera or ROV deployed at this site (see "Operations"), thus the mudline was targeted blindly. The first two holes failed to target the mudline, and therefore the exact depths of the four samples collected in Holes C0006C and C0006D are unknown. Based on sulfate values of these samples (Table T10), Core 316-C0006C-1H likely overpenetrated the sediment/water interface by >10 m and Core 316-C0006D-1H likely missed the mudline by ~8 m. The mudline was successfully recovered in Hole C0006E.

Samples were collected at a spatial resolution of two per core in the uppermost 30 m in Hole C0006E to define the sulfate-methane transition (SMT) and to identify and quantify the anaerobic oxidation of methane (AOM) magnitude at this site, as well as for future geochemical and microbiological studies. Below Core 316-C0006E-3H, one sample was taken per core when recovery was sufficient. The geochemical objectives below the SMT in Holes C0006E and C0006F were to identify the main in situ diagenetic reactions in the sediment section and to identify any exotic/deeply sourced fluids along the fault zones. This was done through analysis of dissolved elements that reflect inorganic fluid-rock reactions or microbially mediated reactions. Elemental concentrations and δ^{18} O isotope ratios are reported in Tables T10, T11, T12, T13, and T14 and plotted as a function of depth in Figures F37, F38, F39, F40, F41, F42, and F43. Because of the brecciated nature of some of the sedimentary material in Holes C0006E and



C0006F (see "Structural geology"), some cores were extremely difficult to clean prior to processing. This is observed in elevated SO₄ concentrations in Table T12, which show that a significant number of interstitial water samples were contaminated with surface seawater during drilling operations. All of the contaminated samples were collected below the SMT where in situ SO₄ is expected to be zero. These samples were corrected for drill water contamination based on measured SO₄ concentrations using the procedure and equations outlined in the "Inorganic geochemistry" section of the "Expedition 316 methods" chapter. Uncorrected concentrations of all of the elements analyzed are presented in Tables T12, T13, and T14, and corrected values are presented in Tables T10 and T11. Only corrected values are presented in the figures.

Salinity, chloride, and sodium

Pore fluid salinity varies from 34.4 at 1.3 m CSF to 29.50 at 571.2 m CSF (Fig. F37). Salinity at 571.3 m CSF (near the base of the hole) is ~16% less than modern seawater value. The pore fluid salinity profile can be divided into two zones. (1) The first zone extends from the seafloor to the base of Subunit IIA and is characterized by a steady decrease from nearseawater value to 32.67 at the base of Unit I followed by an increase to 33.66 at ~100 m CSF (Fig. F37A). (2) Below this depth pore fluid salinity decreases with minor variations to 31.83 at 400 m CSF (base of Subunit IIC). From ~400 m CSF to TD, salinity continues to decrease but is more variable. The salinity decrease in the upper ~20 m of the sediment section reflects active sulfate reduction and subsequent precipitation of authigenic carbonates consuming dissolved SO₄, Ca, and Mg within this interval (Fig. F38A, F38C, F38D). The drop in salinity at the top of Subunit IIB at 76.4 m CSF coincides with sharp minima in both Cl and Na. The decrease in salinity from ~400 m CSF to ~603 m CSF (TD) coincides with decreasing Cl, Na, K, Rb, and Mg.

Pore fluid chloride varies, ranging from 518 to 571 mM, and the profile can be divided into three distinct zones:

- 1. The first zone extends from the sediment/water interface to 100.1 m CSF. Cl in this zone initially decreases from 562 to 558 mM at 1.3 to 12.2 m CSF and then increases to 571 mM (~2.1% greater than modern seawater value) at 100.1 m CSF. Superimposed on this increase is a sharp decrease in Cl at 76.4 m CSF, coincident with a sharp decrease in Na (Fig. F37B, F37C).
- 2. The second zone of the Cl profile extends from 100.1 to 534.2 m CSF and is characterized by steadily decreasing Cl with local minor varia-

tions (Fig. **F37B**). In this zone, a Cl minimum of 534 mM at 292.0 m CSF coincides with a Na minimum. A Cl peak of 562 mM at 534.2 m CSF is coincident with a fault zone (see "**Structural geology**").

3. The third zone extends from 534 m CSF to the base of the hole at 590.2 m CSF and is characterized by steadily decreasing Cl to ~7% less than modern seawater value.

The slow increase in Cl from 12.2 to 100.1 m CSF may be the result of hydrous silicate formation during volcanic ash alteration or evidence of active gas hydrate formation in the upper sediment column. This slight Cl increase could also be a manifestation of trapped interglacial seawater, which would suggest that sufficient time has not yet passed for the signal to diffuse. During core recovery, gas hydrates dissociate and release freshwater into the pore spaces, thus diluting pore fluid Cl. Two negative excursions in the Cl profile at 77 and 292 m CSF, coincident with excursions in salinity, clearly indicate gas hydrate dissociation during core recovery, with Cl values in these horizons being ~6% and 5% of seawater value, respectively.

The Na profile mimics the Cl profile and increases to ~300 m CSF, including a local minimum of 463 mM (Fig. **F37C**) at 77 m CSF. Another local Na minimum of 463 mM (Fig. **F37C**) at 292 m CSF is coincident with a Cl minimum. Below ~300 m CSF, Na decreases to TD with minor local minima and maxima. Two Na minima at 77 and 292 m CSF probably reflect localized gas hydrate dissociation during core recovery, which is also corroborated by the constant Na/Cl ratio within these intervals (Fig. **F37D**). The general decrease in Na from ~300 m CSF to TD also mimics the Cl profile (Fig. **F37D**).

Pore fluid constituents controlled by microbially mediated reactions

Sulfate and alkalinity

Sulfate decreases linearly from 25.2 mM at 1.3 m CSF to 2.14 mM at 7.9 m CSF (Fig. F38A) and is completely depleted by 12.2 m CSF. A concomitant increase in headspace methane concentration at ~8 m CSF (see "Organic geochemistry") constrains the SMT to ~8–12 m CSF (Fig. F38F). The SMT depth is shallower at this site than at Site C0004 upslope, where the SMT is located at 16–20 m CSF. The shallower SMT at Site C0006 could be the manifestation of a higher methane flux or more intense sulfate reduction rates. Between the SMT and ~534 m CSF, sulfate remains depleted with occasional peaks reflecting drilling-induced contamination (Table T12). Results for samples from the sulfate depletion zone were cor-



rected for drilling contamination based on measured SO_4 concentrations and are presented in Tables T10 and T11. All of these samples were highly brecciated. Below ~534 m CSF, dissolved SO₄ increases downhole (Fig. F38A). These units were highly consolidated with the exception of Core 316-C0006F-16R (534.2 m CSF), which was brecciated and from a fault zone. Thus, the outside of the interstitial water whole rounds were easy to clean, which would suggest the increase in sulfate values at the base of the hole reflects detectable in situ pore fluid sulfate. However, methane values remain elevated within this interval (see "Organic geochemistry") and alkalinity remains constant, suggesting the increase reflects sampling artifacts associated with drill water contamination. To be conservative, SO₄ values of the deepest six samples were not used to correct pore fluid chemical data for drill water contamination.

Pore fluid alkalinity increases rapidly in Unit I and reaches a maximum of 25.8 mM at 7.9 m CSF, concomitant with an increase in headspace methane (see **"Organic geochemistry**") and the SMT at this site. Alkalinity at the SMT is less than expected for sulfate reduction/organic matter degradation and AOM, suggesting active precipitation of authigenic carbonates near the depth of the SMT. This explanation is supported by decreases in Ca, Mg, and Mn in this depth interval (Figs. F38C, F38D, F39D). Below the SMT, alkalinity decreases to 3.3 mM at 590.2 m CSF.

Ammonium, phosphate, bromide, and manganese

Ammonium monotonically increases through Unit I and Subunit IIA (Fig. **F39A**). Below this depth, ammonium continues to increase at a slower rate to the middle of Subunit IIB. The ammonium maximum of 6098 μ M occurs at 122 m CSF, below which concentration gradually decreases in Subunit IIC. The concentration gradient steepens in Subunit IID and Unit III, decreasing to 656 μ M by 590.2 m CSF. The steady ammonium increase in the upper ~72 m CSF indicates production by microbially mediated decomposition of organic matter fueled by sulfate reduction above the SMT. Ammonium remains elevated below the SMT because of a combination of ongoing organic matter degradation and high burial rates.

Phosphate increases rapidly in the upper sediment section, reaching a maximum of 89 μM at 17.4 m

CSF. Below this depth, phosphate decreases until ~100 m CSF, below which it is close to detection limit to 593.8 m CSF. The increase in phosphate in the upper 17 m reflects active organic matter decomposition in the active sulfate reduction zone. Unlike dissolved NH_4 , PO_4 decreases relatively sharply be-

low the maximum at 17.4 m CSF, indicating that phosphate is controlled by mineral precipitation reactions. Thus, phosphate is likely controlled by apatite solubility, as authigenic apatite is the major sink for dissolved phosphate.

The dissolved bromide profile generally mimics the NH₄ profile. Br increases from 0.86 mM at 1.3 m CSF to 1.06 mM at 62.5 m CSF and then remains relatively constant to the middle of Subunit IIC, below which it decreases gradually to 590.2 m CSF (Br = 0.86 mM). Bromide in marine interstitial water is sensitive to organic matter diagenesis, with concentration higher than seawater value reflecting marine organic matter decomposition. Terrestrial organic matter degradation does not contribute much Br to the pore fluids. The Br profile at this site reflects a mixture between marine and terrestrial organic matter degradation, but the relatively low Br indicates that the labile organic matter is predominantly terrestrial in origin. Br at Site C0006 is lower than at Site C0004, reflecting higher rates of terrigenous sedimentation at this site.

Manganese concentrations are above seawater value in the upper 4 m of the sediment column, reflecting MnO₂ reduction during microbially mediated organic matter degradation. Manganese reaches depletion in the active sulfate reduction zone and at the SMT, likely due to precipitation of authigenic rhodochrosite at the alkalinity maximum. Manganese then increases slightly below this depth to an average of ~4.5 µM and remains relatively constant with depth to Subunit IID. The slightly elevated dissolved Mn from 17.4 to 406.0 m CSF likely reflects ongoing microbially mediated organic matter diagenesis using Mn oxyhydroxides as terminal electron acceptors. Manganese increases and is more variable in Unit III, possibly reflecting a different sediment source with a higher MnO₂ and Mn hydroxide content.

Major cations (Ca, Mg, and K)

Calcium decreases from 8.76 mM at 1.3 m CSF to 3.97 mM at 17.4 m CSF (Fig. **F38C**). The Ca minimum is ~7 m below the alkalinity maximum and the SMT. Magnesium rapidly decreases in the same depth range interval. Dissolved Mg decreases from 47.5 mM at 1.3 m CSF to 33.8 mM at 17.4 m CSF (Fig. **F38D**). This decrease is ~3 times greater than that of Ca values, suggesting precipitation of Mg and Ca in authigenic carbonates, as well as the exchange of Mg to clay minerals formed by ash alteration. Below this depth, the Ca and Mg profiles are mirror images. From 17.4 to 448.5 m CSF, Ca steadily increases to 10.75 mM, below which the slope of the profile changes. Ca reaches 17.96 mM at the base of the hole (Fig. **F38C**). Below the SMT, Mg continues to



steadily decrease from 17.4 m CSF to 13.85 mM at the bottom of the hole (Fig. F38D).

A significant amount of ash and up to ~20% feldspar were identified in the sediment section drilled at Site C0006 (see "Lithology"). Concentrations of both of these components are highest in Subunit IIC. Alteration of the ash and feldspars could contribute to the increase in Ca (feldspar weathering) and decrease in Mg (ash alteration) from the SMT to the base of Subunit IID. In Unit III, Ca increases rapidly to 17.96 mM (~1.7 times seawater value) at the base of the hole, whereas Mg remains relatively constant. The increase in Ca in this depth interval could be the result of diffusive communication with a compositionally different fluid below the base of Hole C0006F or it could reflect more mature diagenetic reactions with depth.

Potassium decreases overall with depth. In the uppermost 17.4 m, this decrease is more rapid than below, declining from 11.8 mM at 1.3 m CSF to 10.4 mM at 17.0 m CSF (Fig. F40E). K is likely higher than seawater value as a result of pressure changes that occur during core recovery or ion exchange with NH₄ on clay minerals. Below this depth, K continues to decrease to 6.6 mM in the middle of Subunit IID at 405.0 m CSF. From 405.0 m CSF to the base of Hole C0006F, K decreases more rapidly, reaching 3.2 mM at 571.3 m CSF (~70% less than modern seawater value). The general decline in pore fluid potassium below the SMT is likely the result of in situ formation of zeolites during alteration of volcanic ash and feldspars. Authigenic zeolites, possibly phillipsite, were recognized in smear slides from selected intervals in Unit II (see "Lithology"). The rapid K decline in Unit III may reflect more mature diagenesis of volcanic ash and feldspars due to the greater age of the sediments (late Miocene; see "Biostratigraphy") or communication with a compositionally different fluid below the base of Hole C0006F.

Minor elements (B, Li, H₄SiO₄, Sr, and Ba)

Boron decreases throughout the sediment section from 556 μ M at 1.3 m CSF to 94 μ M at 571.3 m CSF (~80% less than modern seawater value). B decreases most rapidly from the seafloor to the base of Subunit IIB at 163 m CSF. B gradually decreases in Subunits IIC and IID and is relatively constant, albeit with local scatter, in Unit III. Boron at Site C0006 is likely predominantly controlled by low-temperature alteration of volcanic ash with subsequent authigenic clay formation, as well as by B uptake by adsorption on clay minerals.

Lithium concentrations are above seawater value in the upper ~ 2 m of the sediment section, and then rapidly decrease to below seawater value from 2 to

20 m CSF. Li remains relatively low, ranging between 7.3 and 20.2 μ M to ~200 m CSF; local maxima are as high as 33 μ M (Fig. F40A). At ~200 m CSF, Li gradually increases to the Subunit IIC/IID boundary. From this unit boundary, Li increases from 42 μ M at 406 m CSF to 136 μ M at 571 m CSF.

Dissolved silica increases rapidly from 437 μ M at 1.3 m CSF to 695 μ M at 12.2 m CSF, below which silica varies, ranging from ~400 to 1000 μ M. Throughout the section at Site C0006, diatoms and radiolarians are either absent or very rare and fragmented (see "Lithology" and "Biostratigraphy"). Thus, the initial increase in H₄SiO₄ is likely due to the dissolution of siliceous biogenic material, whereas variations in silica below Unit I likely reflect varying dominant silicate diagenetic reactions. An increase in H₄SiO₄ in Unit III, as well as more variability in concentrations, likely reflects the change in depositional environment, lithology, and age of this unit.

Strontium rapidly decreases initially in the upper 12 m and remains below modern seawater value until 43.0 m CSF. At 76.4 m CSF, Sr sharply decreases, below which Sr increases to Subunit IID. Below Subunit IID, Sr is more variable and decreases with depth to the base of Hole C0006F (Fig. F40D). The slight Sr decrease in the upper 12 m reflects minor Sr precipitation in authigenic carbonates in the sulfatereduction zone. There was very little CaCO₃ in the sediment section at Site C0006, which is mainly dominated by clays, quartz, and feldspars (see "Lithology"). This composition is reflected in the nearseawater concentration of Sr below the SMT to ~300 m CSF. The steady increase in Sr from 300 m CSF to the middle of Subunit IID may reflect in situ volcanic ash diagenesis, as the concentration of ash and abundance of ash layers increase within this interval (see "Lithology").

Dissolved barium increases from 0.6 µM at 1.3 m CSF to 12.7 µM at 12.0 m CSF, which is ~2 m below the base of the SMT. Ba remains remarkably constant, ranging from 9 to 19 µM from 12.0 m CSF to the middle of Subunit IID. From ~387 m CSF, Ba increases and varies through Unit III to the base of Hole C0006F. The main Ba-containing phase in marine sediments is the mineral barite (BaSO₄), with aluminosilicates and Fe and Mn oxyhydroxides being the most important secondary phases. The mineral barite is stable under oxic conditions but becomes undersaturated and dissolves when pore fluid sulfate is depleted, releasing dissolved Ba to the pore fluids. The slight increase in pore fluid Ba in the upper 8 m of the sediment section is likely due to the dissolution of Fe and Mn oxyhydroxides during organic matter diagenesis. The increase in Ba across the SMT and with depth is most likely the result of barite



dissolution in the sulfate depletion zone. The nearconstant dissolved Ba in Unit II is likely the manifestation of a near-uniform sedimentary barite content resulting from relatively rapid sedimentation of terrigenous material in a trench environment. The rapid increase in dissolved Ba in Subunit IID and Unit III is also likely related to the depositional environment. These sediments were deposited in an abyssal plaintype setting with less contribution of terrigenous material and a higher relative contribution of marine organic matter and biogenic barite.

Trace elements (Rb, Cs, V, Cu, Zn, Mo, Pb, and U)

The pore fluid rubidium profile mimics the K profile (Fig. F40E, F40F). Rb decreases from above seawater value to 1.06 µM at 43.0 m CSF and then remains relatively constant in Subunits IIB and IIC at ~1.0 µM. Rb decreases in Subunit IID and Unit III, reaching ~0.45 μ M at the base of the hole (~30% less than modern seawater value). Rb is likely higher than seawater value in the upper 20 m of the sediment column because of cation exchange with NH₄ on clays in the zone of most intense organic matter degradation and ammonium production. The general decline in Rb with depth likely reflects uptake by authigenic zeolites formed during volcanic ash alteration. The steady decrease in Rb in Unit III may reflect more mature ash diagenesis, given the older age of sediments within this unit, or communication with a low-Rb fluid at depths below the base of Hole C0006F. Dissolved Cs remains relatively constant from the seafloor to 405 m CSF, varying from 4.4 to 8.7 µM. Cs decreases within Subunit IID from 5.3 µM at 405 m CSF to 3.2 µM at 406 m CSF and then remains relatively constant to TD.

Vanadium is above seawater value and variable from 1.3 to 243.4 m CSF (Fig. **F41D**). Below this depth, V remains fairly constant with depth to the base of the hole, ranging from 4.7 to 33.8 nM. V is most variable in Unit I and Subunits IIB and IIC, with concentrations ranging from 6.9 to 89.5 nM. This variability in the V profile may indicate enhanced metal mobility in certain horizons and will be the focus of postcruise research. Fe is highly variable, ranging from 0 to 51 µM. In general, Fe is much higher in Unit I and Subunits IIA and IIB, which likely reflects ongoing microbially mediated organic matter oxidation using Fe oxyhydroxides as terminal electron acceptors. Subunits IIC and IID and Unit III as a whole exhibit low dissolved Fe, except for peaks at ~200, 260, and 340 m CSF.

Both dissolved zinc and molybdenum are highly variable, exhibiting scatter in each of the lithologic units. Mo ranges from 26 to 850 μ M, and dissolved Zn ranges from 30 to 1294 nM. In general, Mo and

Zn are relatively lower in Unit I and Subunit IIA and higher in Subunits IIB-IID and Unit III. Copper concentration is relatively low and variable in Unit I and Subunits IIA–IID, ranging from 57 to 8466 nM. There is a sharp increase in Cu across the Subunit IID/Unit III boundary, reflecting a change in lithology. Cu is variable in Unit III, ranging from 696 to 31,893 nM. Uranium decreases abruptly from 25.7 nM at 1.3 m CSF to 0.7 nM at 4.4 m CSF (Fig. F42). Uranium is more soluble under oxidizing conditions than reducing conditions; thus the rapid decline in U is the manifestation of the rapid depletion of dissolved oxygen in the upper part of the sediment section. U remains low with an average concentration of 1.5 nM in Unit I and Subunits IIA-IID. U is slightly higher and more variable in Unit III with a maximum concentration of 9.2 nM. Lead is relatively low in Unit I and Subunits IIA-IID, with peaks at 17.4, 137.5, 329.0, and 404.9 m CSF. Average Pb concentration

329.0, and 404.9 m CSF. Average Pb concentration increases in Unit III. The enrichment in U and Pb in Unit III reflects a change in lithology. Yttrium concentration generally decreases with depth, ranging from 6.4 pM at 12.2 m CSF to 0.15 pM at TD.

$\delta^{18}O$

Pore fluid δ^{18} O varies from 0.19‰ to -4.19‰ (Fig. **F43**). From 1.3 to 81.9 m CSF (bottom of Subunit IIA), the δ^{18} O profile is characterized by a steady decrease in values to -3.00‰. Below this depth, δ^{18} O remains relatively constant to ~400 m CSF, the base of Subunit IID. δ^{18} O is variable in Unit II, with a prominent peak of -1.60‰ at 439 m CSF.

Summary and discussion

The primary features of the pore fluid geochemical profiles collected at Site C0006 are

- 1. Relatively shallow SMT and high burial rates and input of terrigenous material in Unit I and Subunits IIA, IIB, and IIC;
- 2. Disseminated gas hydrates with localized occurrences of elevated pore space gas hydrate concentrations;
- 3. No detectable recent fluid flow from depth along the imbricate thrust faults above the deformation front; and
- 4. Distinct change in pore fluid chemistry and isotopic composition in Unit III.

Microbially mediated reactions and high influx of terrigenous sedimentary material

The pore fluid profiles in the upper ~60 m of the sediment column are dominated by microbially mediated reactions, and the SMT is reached at 8–12 m CSF. Above this interface, sulfate-reducing microbial



communities utilize interstitial sulfate to oxidize sedimentary organic matter, reducing sulfate to sulfide and producing bicarbonate by Reaction 1:

$$2CH_2O + SO_4^{2-} \rightarrow H_2S + 2HCO_3.$$
(1)

Below the interface, methanogens generate methane. At the interface in some environments (especially diffusive settings), microorganisms symbiotically reduce sulfate and oxidize methane by a biogeochemical process called anaerobic oxidation of methane (AOM). The net biogeochemical process is described by Reaction 2 (Reeburgh, 1976):

$$CH_4 + SO_4^{2-} \rightarrow HCO_3^{-} + HS^{-} + H_2O.$$
(2)

Pore fluid alkalinity reaches a maximum of 25.78 mM at the depth of the SMT. Based on Reactions 1 and 2, if sulfate reduction by oxidation of organic matter is the dominant process controlling sulfate to the depth of the SMT, then two moles of alkalinity are produced for each mole of SO₄ reduced (~60 moles of alkalinity). If AOM is the dominant process controlling pore fluid sulfate, then one mole of alkalinity is produced for each mole of SO₄ reduced (~30 moles of alkalinity). Alkalinity at the SMT is less than expected from both processes because of the active formation of authigenic carbonate at this interval, which is manifested by the sharp decrease in Ca and Mg from the seafloor to slightly below the SMT. Although the linearity of the SO₄ reduction profile and relatively low alkalinity suggest that AOM is the dominant process controlling sulfate, the large decreases in Ca and Mg to the SMT indicate that ordinary organic matter oxidation is also a control. Shorebased δ^{13} C-DIC analyses will aid in constraining the relative extent of AOM at this site.

Ammonium increases below the SMT, reaching a broad maximum of ~6000 µM between ~72 and 200 m CSF. This broad zone of elevated NH₄ is likely due to the combination of ongoing organic matter degradation and high burial rates (combination of high sedimentation rates and thrust faulting) at this site. Unit I has a slope association and Subunits IIA, IIB, and IIC were deposited in a trench environment where sedimentation rates are high and dominated by terrigenous material (see "Lithology"). The amount of terrigenous material and deposition rate increase upsection. Thus, the broad maximum in NH₄ is likely the manifestation of high sedimentation rates effectively burying ammonium more quickly than diffusion and advection across the sediment/water interface could remove it. Sedimentation rates are lower and the amount of terrigenous material decreases with depth in Subunits IIC and IID where ammonium gradually decreases. Unit III is interpreted to be a deepwater marine environment with low terrigenous material input and sedimentation rates, and within this unit ammonium decreases. The greater proportion of terrigenous material in comparison to marine material is corroborated by overall low Br, which suggests degradation of terrestrial organic matter is much more prominent than degradation of marine organic matter in the upper sediment section. Br then decreases with depth into Unit III, indicating lower rates of organic matter degradation. The higher amount of terrestrial material in the upper sediment section is also observed in pore fluid Ba, which is relatively low in Unit I and Subunits IIA, IIB, and IIC, likely reflecting dilution of biogenic barite by terrigenous material. Ba increases in Unit III, which was likely deposited in a deepwater marine environment seaward of the deformation front. This type of depositional environment would have a lower contribution from terrigenous sources and thus would have higher biogenic barite concentration.

Gas hydrate occurrence

The relatively shallow SMT at Site C0006 suggests an elevated upward methane flux and the heat flow is anomalously low for this region (see "Physical properties"), both of which provide ideal conditions for gas hydrate formation in the sediment column. The thermal gradient at Site C0006 is 27°C/km, compared with >50°C/km at Sites C0004 and C0008 (see "Physical properties"), and the bottom water temperature is 2°C. Assuming equilibrium with Structure I gas hydrate, the CSMHYD program of Sloan (1998) was used to compute the gas hydrate stability field at this site. From the thermal gradient, the gas hydrate stability field for Structure I gas hydrate extends from the seafloor to ~800-850 m. Pore fluid Cl from ~100 to ~500 m CSF gradually declines from 571 to 540 mM, which likely reflects dissociation of disseminated gas hydrates within the sediment pore space during core recovery. The gradual decrease in pore fluid Cl indicates that gas hydrate, though overall very low, increases with depth. Using a background pore fluid value of 568 mM, the pore space gas hydrate ranges from negligible to <2% within the sediment column. Superimposed on the gradual decline in Cl are two Cl minima of 526 mM at 76 m CSF and 533 mM at 292 m CSF, which indicate horizons of elevated gas hydrate occurrence; however, hydrate concentrations at these two depths are still relatively low, comprising less than $\sim 5\%$ of the sediment pore space.

Pore fluid geochemical profiles through fault zones

The pore fluid geochemical profiles are relatively smooth through the deformation zone at Site C0006,



which is characterized by a zone of imbricate thrust faults extending from ~275 to 540 m CSF (see **"Structural geology**"). Within this deformation zone, Ca, Sr, and Li steadily increase and Cl, Na, Mg, B, K, and Rb decrease. There are no local maxima or minima coincident with the faults at Site C0006; thus, there is a lack of evidence for recent updip flow of fluids from greater depths along these fault zones, suggesting that either recent rupture has been localized, fault permeability is not enhanced during slip events, or these faults have been inactive in the recent past.

From ~500 m CSF to the base of the hole at ~600 m CSF, there are distinct changes in many of the pore fluid chemical profiles. Within this interval, Li and Ca markedly increase and Cl, K, and Rb decrease. Sediments at the base of Hole C0006F, comprising Unit III, are late Miocene in age (see "Biostratigraphy"), and the geochemical variations could reflect more mature diagenetic reactions because of the greater potential age of pore fluids. Another possibility is that these fluids reflect diffusional communication with a fluid originating deeper than the base of Hole C0006F, potentially residing in faults and fractures associated with the frontal thrust.

Organic geochemistry

At Site C0006, four holes were drilled. In Holes C0006C and C0006D, the mudline was not confirmed. Because of the unknown depths (see "Inorganic geochemistry"), data from these holes are included in tables (Tables T15, T16, T17) but are not shown in figures.

Hydrocarbon gas composition

At Site C0006, the SMT zone is at ~8-12 m CSF, which is a few meters shallower than at Site C0004 (Table T16; Fig. F44). The methane depth profile below 14 m CSF decreases throughout the sediment column (except for two peaks at ~100 and 310 m CSF). These increased methane values are obtained only a few meters below the occurrence of measured chloride anomalies that suggest the occurrence of gas hydrates (see "Inorganic geochemistry"). Thus, the enrichment in methane content at these two intervals could be related to the destabilization of gas hydrates and the subsequent release of methane into the sediment. Ethane was detected in low amounts in the sediment below 76 m CSF. Higher molecular weight hydrocarbons were not detected at Site C0006. The methane/ethane (C_1/C_2) ratio remains high throughout the sediment column, indicating biogenic origin of the hydrocarbon gases.

Sediment carbon, nitrogen, and sulfur composition

The amount of calcium carbonate $(CaCO_3)$ in sediments at Site C0006 is lower than that at Site C0004 (Table **T17**; Fig. **F45**). The highest values were obtained in Unit I, with a maximum concentration of 6.2 wt%, followed by a decrease in Subunit IIA. This is consistent with calcite data obtained from XRD measurements (see "Lithology"). A slight increase in CaCO₃ occurs at the Unit II/III boundary. The highest carbonate value was measured at the bottom of Hole C0006F.

Except for a few enrichments, total organic carbon (TOC) remains low throughout the core (average = 0.46 wt%). Total nitrogen (TN) increases throughout Unit III. Because ammonium concentration decreases (see **"Inorganic geochemistry"**) and total clay content is higher in Unit III (see **"Lithology"**), the TN enrichment is probably related to clay-bound nitrogen substances. The ratio of TOC to TN (C/N) averages ~7.0, indicating that organic matter at Site C0006 is mainly of marine origin. A few higher values indicate that some terrigenous organic compounds are present in lower concentrations in Units I and II.

Total sulfur (TS) concentration in sediments is generally low (average = 0.25 wt%). In Unit I, TS is higher, showing a maximum of 1.7 wt% at ~17 m CSF. The enrichment is below the SMT and can most likely be associated with the precipitation of fine-grained iron sulfides. This will be evaluated by shore-based analyses of samples. In Unit II, TS concentration remains low (average = 0.2 wt%) and slightly increases again in Unit III to 0.77 wt%. The higher TS concentration below ~500 m CSF can be related to the occurrence of small pyrite nodules (see Fig. F6).

Additionally, three samples from 370.18, 370.67, and 371.05 m CSF were analyzed (data are not included in figures). The samples were selected from wood-bearing sediments in turbidite sequences (see Fig. F6). TS concentrations in these samples are 1.8, 2.66, and 2.32 wt%, respectively. TOC and TN concentrations are up to 10 times higher than in the surrounding sediments, with TOC contents of 3.8, 6.87, and 3.91 wt%, respectively, and TN contents of 0.1, 0.15, and 0.11 wt%, respectively. The mean C/N ratio of the three samples is ~40.

Microbiology and biogeochemistry Sample processing

To study microbiological and biogeochemical characteristics in sediments at Site C0006, samples were



obtained from 143 different depth locations (Table **T18**). Almost all sample processing was carried out after X-ray CT scanning and was completed within 1 h after core recovery on deck.

Cell abundance

Using paraformaldehyde-fixed slurry samples, preliminary microbial cell abundances were enumerated by visual inspection using the SYBR Green I staining method (Lunau et al., 2005, see "Microbiology and biogeochemistry" in the "Expedition 316 methods" chapter). At Site C0006, ~109 cells/cm3 were detected in the upper lithologic unit above 100 m CSF. An apparent increase of microbial biomass was observed in sand layers, possibly suggesting the occurrence of energy supply via fluid circulation. Below the upper lithologic unit, microbial population decreased with depth in the accretionary prism, which is in good agreement with typical cell abundance tendencies that have been observed in global marine subsurface sediments (Parkes et al., 2000). In the accretionary prism, no or very small proliferation of cell abundance was observed in sand layers and at the Unit II/ III boundary (Fig. F46). Most cells were tiny coccoids, but rod-shaped cells were also observed as minor components (Fig. F47). Generally, the microbial population in the accretionary prism at Site C0006 was found to be low (10⁷ cells/cm³), which is in clear contrast to the constant and abundant microbial population (10⁹ cells/cm³) at Site C0004. Average cell abundance in sediments at Site C0006 was estimated to be $6.19 \times 10^8 \pm 2.27 \times 10^8$ cells/cm³ (N = 27).

Given the cell abundance profile at Site C0006, it is hypothesized that the microbial population size may indicate the energy status of the subsurface. The microbial population generally decreases with increasing depth because of the limited availability of nutrient and energy sources that support microbial growth activity. If the decreasing population ratio indicates the balance point between community size and life maintenance energy (Hoehler, 2004), the accretionary prism at Site C0006 may be a harsh and energy-starved habitat for subseafloor life. It is a clear contrast to the accretionary prism at Site C0004, where relatively high biomass is present throughout the cored materials (Fig. F46). In addition, it is worth noting that the energy flux does not always indicate flux or hydrological movement of interstitial water; dehydration of smectite or physical compaction may induce water flux along faults and/ or fractures, but the fluids do not always contain the energy (nutrient) substrates required for microbial life. On the other hand, porous sand layers in the upper unit harbor abundant microbial populations, suggesting that the environment is rich in available

energy sources and habitable space. The potential energy sources in the sand layers are probably buried consumable organic matter (e.g., organic acids) and/ or substrates derived from fluid circulation.

Physical properties

At Site C0006, physical property measurements were made to provide basic information characterizing lithologic units, states of consolidation, deformation, and strain and to correlate coring results with downhole logging data. After capturing X-ray CT images and the core reached thermal equilibrium with ambient temperature at ~20°C, gamma ray attenuation (GRA) density, magnetic susceptibility, natural gamma radiation, P-wave velocity, and noncontact electrical resistivity were measured using a multisensor core logger (MSCL) system on whole-round core sections (MSCL-W). Thermal conductivity was measured using either a full-space needle probe method or a half-space line source method on split working halves. The half-space method was used on lithified sediments deeper in the hole that were impenetrable with the needle probe. Cores were split in two longitudinally, one half for archiving and one half for sampling and analysis. A photo image capture logger (MSCL-I) and a color spectrophotometer (MSCL-C) were used to collect images of the split surfaces of the archive halves. Moisture and density (MAD) were measured on discrete subsamples collected from the working halves as well as from "clusters" adjacent to whole-round samples removed before splitting. Vane shear and penetration experiments were performed on the working halves to 270 m CSF. Additional discrete subsamples from working halves were used to perform electrical conductivity measurements, P-wave velocity measurements, and anisotropy calculations.

Density and porosity

Bulk density values at Site C0006 were determined from both GRA measurements on the MSCL and MAD measurements on discrete samples from the working halves of split cores (see "**Physical properties**" in the "Expedition 316 methods" chapter). A total of 613 discrete samples were analyzed for MAD (14 from Hole C0006C, 14 from Hole C0006D, 507 from Hole C0006E, and 78 from Hole C0006F).

MAD wet bulk density increases dramatically from 0 to ~38 m CSF and then decreases slightly from ~38 to ~50 m CSF, followed by a gradual increase to ~400 m CSF (Fig. F48A). Maximum MSCL bulk density values (one component of the MSCL logging suite) also show similar trends. MSCL bulk density is generally lower than MAD bulk density, likely because of voids in the unsplit cores, and reveals a



larger degree of scatter compared to density from discrete samples. The scatter in MAD bulk density is likely due to lithologic variations among the interbedded sand, silt, and mud at this site. Grain density averages ~2.7 g/cm³ (Fig. **F48B**) and increases slightly (~0.05 g/cm³) from 0 to 570 m CSF. Grain density values >3 g/cm³ are likely artifacts.

Porosity was estimated from whole-round core MSCL scans and calculated from MAD measurements on discrete samples. MAD porosity (see "Physical properties" in the "Expedition 316 methods" chapter) generally decreases with depth (Fig. F48C) and varies inversely with bulk density. Because of the greater scatter in MSCL density and porosity values, we focus on bulk density and porosity values calculated from MAD measurements.

Density and porosity of lithologic units

At Site C0006, bulk density of the Pleistocene trenchslope transition package of mud and interbedded sand comprising Unit I (see "Lithology") increases in the upper 5 m from ~1.80 to ~1.90 g/cm³ and then gradually increases from ~1.90 to 1.92 g/cm³ with depth to 27 m CSF (Fig. F48A). As density increases, porosity decreases (Fig. F48C).

Unit II is composed of trench-wedge and trenchbasin transitional sand, silt, and mud of Pleistocene age (see "Lithology"). From Subunit IIA through the upper one third of Subunit IID (i.e., from ~27 to ~410 m CSF), bulk density gradually increases from ~1.92 to ~2.07 g/cm³ (Fig. F48A). This trend is mirrored by a gradual decrease in porosity with depth from ~46% at the top of Unit II to ~38% at ~410 m CSF (Fig. F48C). Gaps in the data in Unit II mark regions of low core recovery and likely indicate the presence of fault zones (see "Structural geology"). In the bottom two-thirds of Subunit IID (from ~410 to ~450 m CSF), bulk density decreases rapidly from ~2.07 to 1.94 g/cm³ (Fig. F48A), whereas porosity increases from ~39% to ~49% (Fig. F48C).

From ~450 to ~475 m CSF, bulk density decreases and porosity increases. At ~475 m CSF, however, the bulk density and porosity trends reverse, increasing and decreasing, respectively, with increasing depth (Fig. **F48A**, **F48C**). From ~475 to 570 m CSF, bulk density increases from ~1.90 to ~2.10 g/cm³ (Fig. **F48A**). Similarly, porosity decreases dramatically from ~49% to ~40% from ~475 to ~570 m CSF.

Relationships of density and porosity changes with unit and structural boundaries

MAD-derived bulk density and porosity increase and decrease, respectively, from 0 to ~410 m CSF and re-

veal no clear discontinuities at depths corresponding to possible faults at 235, 277, and 367 m CSF or at the Unit I/Subunit IIA, Subunit IIA/IIB, or Subunit IIC/IID lithologic boundaries within that depth range. A discontinuity in the porosity versus depth trend at ~410 m CSF occurs within Subunit IID and coincides with a thrust fault at ~410 m CSF inferred from seismic reflection data and above the top boundary of the shear zone in the interval from 434 to 440 m CSF identified in the split core.

The zone of highest porosity (~50%) between ~450 and ~490 m CSF is bounded by faults. This zone of elevated porosity possibly results from increased occurrences of fluid-filled microcracks and other faultrelated damage. Alternatively, elevated porosity in this zone could indicate that these sediments are underconsolidated, reflecting elevated fluid pressures, which may have localized shear deformation in this region. We note that although mud and silt samples from these zones of elevated porosity appear to be well-indurated chunks of material, they are actually quite friable in hand sample. This observation suggests that these are zones of fault-related damage. In either case, this interval appears to be a zone of significant faulting.

We also note that the interval of elevated porosity appears to correlate with an interval of increased clay content. Lithologic analyses of the split core reveal that Unit III exhibits an overall increase in clay content and decreases in quartz and feldspar contents compared to the overlying Subunit IID (see "Lithology"). Clays may lead to spuriously high porosity because the drying process during MAD measurement removes interlayer water from smectite (Brown and Ransom, 1996). Clays may also decrease permeability of sediments and rocks in this interval, allowing pore fluid overpressures to develop more easily.

From ~490 to 570 m CSF, porosity decreases with depth, though porosity values in this interval are still higher than might be predicted based on the overall trend observed from ~5 to 410 m CSF. These higher than expected porosity values are probably explained in part by lithologic and compositional differences between units, which result in different porosity-depth trends. The mismatch may also indicate that rocks in this interval are significantly damaged by the overlying fault or faults from ~434 to ~490 m CSF and the faults from ~533 to ~560 m CSF, identified on the basis of seismic data and structural geology observations. Alternatively, the high porosity could be due to the presence of interlayer water in clays and/or overpressured fluids.



P-wave velocity and electrical conductivity in discrete samples

P-wave velocity and electrical conductivity were measured on cubic samples along x-, y-, and z-directions of the core reference (see "Physical properties" in the "Expedition 316 methods" chapter). Samples were relatively indurated, and no noticeable disaggregation was observed when immersed in seawater. This induration is in marked contrast to the behavior observed in samples from Site C0004 through the shallow megasplay. The electrical conductivity data set is more extensive than that collected for P-wave velocity. The instrument used to measure P-wave velocity requires an applied normal stress of ~120 kPa, which caused deformation to samples from depths shallower than 230 m CSF, voiding the measurement. Conversely, in some deeper cores, P-wave velocity measurements were easier to obtain because of the difficulty of sawing adequate faces for electrical conductivity measurements. Results of electrical conductivity, P-wave velocity, and associated anisotropy measurements are plotted in Figure F49.

Electrical conductivity (Fig. F49A) decreases overall with depth. Although the data are highly scattered throughout the uppermost 300 m, below 300 m CSF electrical conductivity manifests two recognizable trends in the intervals from ~300 to ~400 m CSF and from 470 to 600 m CSF. Both trends show a decrease in electrical conductivity but are offset by ~10% through an increase in electrical conductivity within Subunit IID. These trends and offsets are also observed in LWD resistivity-at-the-bit (RAB) data, which improves our confidence that this pattern is real (see the "Expedition 314 Site CO006" chapter). Additionally, these trends mimic trends observed in MAD porosity (Fig. F48C). MAD porosity values are offset by ~10%, similar to the offset observed in electrical conductivity data. Between 410 and 470 m CSF, poor core condition prevented adequate sampling.

Electrical conductivity anisotropy shows considerable scatter at depths shallower than 300 m CSF (Fig. **F49B**). At ~200 m CSF, three sets of measurements indicate high anisotropy and are associated with significantly lower magnitudes of electrical conductivity. Between 300 and 400 m CSF, transverse anisotropy decreases with depth and, coupled with the decrease in electrical conductivity (Fig. **F49A**), might indicate progressive compaction with depth.

P-wave velocity (Fig. **F49C**) increases from ~1800 m/s a little below 200 m CSF to ~2100 m/s near the bottom of Hole C0006E. At ~300 m CSF and again at ~400 m CSF are two zones that correspond to increased scatter in both *P*-wave velocity and electrical conductivity measurements. *P*-wave velocity also decreases by as much as 300 m/s through discrete in-

tervals at 520, 550, and 570 m CSF. Although these velocity differences could potentially be associated with faults, microstructural data are needed to conclusively establish the cause of these low-velocity zones. The anisotropy of *P*-wave velocity (Fig. F49D) generally decreases with depth with two discrete zones of higher transverse anisotropy at ~400 and ~480 m CSF.

Thermal conductivity

Thermal conductivity measurements were conducted on whole-round HPCS and ESCS cores (<316 m CSF) and on split core samples from RCB cores from >316 m CSF. Thermal conductivity ranges from 0.51 to 1.61 W/($m \cdot K$) (Table T19; Fig. F50A). Thermal conductivity from the seafloor to ~80 m CSF shows a striking positive excursion through Unit I and Subunit IIA that likely reflects higher sand content through this interval. A negative trend in thermal conductivity is observed through Subunit IIA, likely reflecting a decrease in sand content. Between ~80 and 400 m CSF, thermal conductivity generally increases, likely reflecting decreasing porosity. As porosity decreases, thermal conductivity increases as water is forced out of void spaces because the thermal conductivity of sediment is greater than water. Thermal conductivity values in this region show large scatter relative to the mean, likely reflecting the effects of interbedded sands and clays. Thermal conductivity in Unit III increases with depth but is offset to lower values relative to the trend through Subunits IIB and IIC.

In situ temperature

In situ temperature was measured using both the APCT3 and DVTP. Three of six deployments of the APCT3 and three of seven deployments of the DVTP were successful (Table T20). All measurements were made in calm to moderate seas. Temperature-time series for each temperature measurement are shown in Figure F51. The temperature tool was stopped at the mudline for as long as 10 min prior to each penetration. The average apparent bottom water temperature is 1.65°C (Table T20). Significant frictional heating occurred on all penetrations, and the temperature versus time records exhibit the characteristic probe penetration heating pulse and subsequent decay (Fig. F51). Equilibrium temperature estimates are based on a 1/time approximation from the temperature-time series while the tool is in the bottom sediments. The effective origin time of the thermal pulse associated with tool penetration was estimated by varying the assumed origin time until the thermal pulse decay followed the theoretical curve. A delay of 15–106 s from the initial penetration heating time



was found to be required to give a linear 1/time plot. Because of tool movement in the bottom, the time over which equilibrium temperatures are estimated is variable. Equilibrium temperature estimates are based on relatively short fits at 98.3 and 220.3 m CSF with fitting times of 2.8 and 3.3 min, respectively. However, in spite of the short period over which these equilibrium temperatures are estimated, and with the exception of the measurement at 277.3 m CSF, resulting temperatures form a relatively constant gradient with depth giving confidence to individual temperature determinations (Fig. F50B). Additionally, it is important to note that temperature derived from both the APCT3 and DVTP give consistent results.

Equilibrium temperatures as a function of depth are quite linear, with the exception of the measurement at 277.3 m CSF. The best fitting thermal gradient through the first six measurements is 27°C/km (Fig. **F50B**). The equilibrium temperature at 277.3 m CSF falls well below the thermal gradient derived above with a temperature only slightly warmer than bottom water. The low thermal gradient coupled with this anomalously cold temperature at depth suggests that colder than normal conditions exist around Hole C0006E.

Heat flow

If heat transfer is by conduction and heat flow is constant, the thermal gradient will be inversely proportional to thermal conductivity according to Fourier's law. This relationship can be linearized by plotting temperature as a function of summed thermal resistance (Bullard, 1939) (see the "Expedition **316 methods**" chapter) (Fig. F50C). In the following analysis, the temperature measurement at 277.3 m CSF is not included. The least-squares fit to the temperature and thermal resistance data indicates a heat flow of 33 mW/m² and a bottom water temperature of 2.1°C. The estimated bottom water temperature is only 0.4°C different than the measured apparent bottom water temperature (Table T19). Predicted temperature deviates from those measured by <0.2°C. With the exception of the measurement at 277.3 m CSF, a constant conductive heat flow appears to describe the overall thermal structure quite well. This heat flow value is anomalously low with respect to other heat flow values along the Nankai Trough and in the vicinity of the Kii transect (Yamano et al., 2003).

Two features of the temperature-depth profile at Site C0006 are important. The first is the very low but constant thermal gradient, which gives rise to an anomalously low heat flow value. The second feature is the low temperature measurement at 277.3 m CSF.

The heat flow value appears to be a local feature because it is anomalously low relative to heat flow values at Sites C0004 and C0007, as well as regional data determined from gravity-driven probes. Possible explanations for this locally low heat flow value include the dissociation of hydrate and local downward flow of seawater. Because of the low thermal gradient, depths drilled at Site C0006 are all within the hydrate stability zone, precluding the widespread dissociation of hydrate. The lack of widespread hydrate is also confirmed by both interstitial water geochemistry and methane measurements on cores. Inorganic geochemistry results do not indicate downward fluid flow. However, downward fluid flow seaward of Hole C0006E but close to the hole may induce the locally low thermal gradient. The low temperature measurement at 277.3 m CSF is 6.6°C cooler than predicted by the best-fit conductive gradient (Fig. F50B). This temperature measurement coincides with a sharp negative anomaly in both sodium and chlorinity concentrations (see "Inorganic geochemistry") consistent with the local presence of methane hydrates. However, a 6.6°C temperature drop associated with the dissociation of hydrate seems implausible. Another explanation for the low temperature measurement is the infiltration of cold bottom water through the sediments prior to the temperature measurement because of drilling disturbance. The lithology at this depth is sandy silt and core recovery was poor (recovery = 38%). Thus it is possible that the low temperature reflects intrusion of seawater prior to the temperature measurement. Discerning the cause of the low heat flow will require additional work.

Shear strength

Shear strength measurements were determined using a semiautomated miniature vane shear device and a pocket penetrometer. Measurements were made at discrete locations on the working halves of split cores at a frequency of approximately three measurements per core in sections 2, 5, and 7. Tests were conducted on relatively intact and homogeneous regions of these sections, generally somewhere between 50 and 100 cm below the top of the section. To minimize error induced by disturbance of the core by the measurement technique, vane shear tests were conducted first, followed by penetrometer tests 1–2 cm from the site of the vane shear penetration, followed by MAD sampling. No vane shear measurements were conducted on whole cores. Both instruments were inserted orthogonally to the surface of the working halves. The rotation rate of the semiautomated vane shear apparatus on board the *Chikyu* is 71°/min.



Results of shear strength measurements from the vane shear and penetrometer methods are presented in Figure F52. Both measurement techniques were applied at regular intervals to 270 m CSF in Hole C0006E. An additional measurement was taken in an apparently unconsolidated sandy layer in Core 316-C0006E-31X at 321 m CSF, but this was not a characteristic lithology for either the core or Subunit IIC as a whole.

We observe a rapid increase in shear strength in the uppermost 40 m CSF in all of Unit I and into the top of Subunit IIA. At 40 m CSF, shear strength drops rapidly and is associated with the prevalence of sandy beds. Both vane shear and penetrometer measurements may differ for fine-grained and coarsegrained sediments because of variations in partial drainage behavior during the test. Deformation of low-permeability clay-rich sediments is likely to be nearly undrained, whereas the deformation of highly permeable coarse-grained sediments is likely to be nearly drained. As a result, direct comparison between values for substantially different lithologies is not straightforward.

The Subunit IIA/IIB boundary is coincident with an increase in shear strength at 72 m CSF. A similar increase at 110 m CSF does not appear to correlate with a significant lithologic change. Shear strength continues to increase to 200 m CSF. Between 200 and 275 m CSF, there is an apparent decrease in shear strength. This decrease will need to be corroborated by shore-based research, as there is some bias in both methods due to changing deformation style as rocks become more cohesive. Vane shear and penetrometer techniques are designed for pervasive deformation and failure of sediments and are not calibrated for measuring materials that fail because of the formation of discrete fractures.

Color spectrometry

Results from the measurement of color reflectance are presented in Figure F53. The L* values range from ~20 to 50. The a* values range from -2 to 2 and the b* values range from 0 to 4. At less than ~100 m CSF, there is a slight decrease in each index. There is no significant anomaly of these values with depth.

Magnetic susceptibility

Volumetric magnetic susceptibilities were measured using the whole-round core MSCL in all recovered cores from Site C0006 (Fig. F54). Uncorrected magnetic susceptibility values are presented in this volume. Magnetic susceptibility varies between ~0 and 500×10^{-3} SI with a mean of ~ 200×10^{-3} SI. Magnetic susceptibility values in Unit I are relatively low with the exception of a positive spike at ~37 m CSF. Within Subunit IIA, values generally decrease with depth but oscillations may reflect interbedded sands and clays. Within Subunits IIB and IIC, magnetic susceptibility values are relatively constant with a relatively wide range between ~200 and 400×10^{-3} SI. Values within Subunit IID decrease with depth and are very low through Unit III. These low values may be erroneous because of incomplete core recovery near the bottom of the hole.

Natural gamma ray

Natural gamma ray (NGR) results are reported in counts per second (cps). The background scatter, produced by Compton scattering, photoelectric absorption, and pair production was measured at the beginning and subtracted from measured gamma ray values. In general, NGR counts are low and consequently may be affected by the short counting interval and porosity variations. The average and standard deviation of NGR results are 34 and 8 cps, respectively (Fig. **F55**). NGR values decrease through Unit I and Subunit IIA, increase with depth in Subunit IIB, and remain relatively constant through Subunits IIC and IID and Unit III where there are no significant anomalies.

Integration with seismic and logging-while-drilling data

Distances between Holes C0006B, C0006E, and C0006F are ~25 m and distances between Holes C0006C, C0006E, and C0006D are ~2.5 m (Fig. F2). Core-seismic integration between Holes C0006B, C0006E, and C0006D is primarily based on prestack depth-migrated seismic profiles of Inline 2435 from the Center for Deep Earth Exploration (CDEX) 3-D seismic survey (Fig. F2) and Cross-line 1755 from the Institute for Frontier Research on Earth Evolution (IFREE) 3-D seismic survey. Additionally, the structural and lithologic framework in Hole C0006F relies on Line 89 of the IFREE 3-D seismic survey for correlation. Thick sand layers provide key reflections for correlation. For example, the truncation points indicate an unconformity at the Unit I/Subunit IIA boundary. However, because each of these holes intersects many faults, dips of strata change with depth, complicating correlations. Additionally, between 110 and 210 m seismic depth below seafloor (SSF) as well as between 330 and 530 m SSF, the seismic phases between holes are discontinuous.

In spite of the low vertical seismic resolution and discontinuous reflectors, core and log data between



Holes C0006B, C0006E, and C0006F are integrated based on the comparison between NGR, MSCL Pwave velocity logs, and gamma ray and sonic logs from LWD data sets (Fig. F56A). Correlations between Holes C0006C, C0006E, and C0006D rely on MSCL NGR and P-wave velocity logs (Fig. F56B). The logs are well correlated because these holes are very close to each other. Generally, the estimated uncertainty in correlated depths is <10 cm. Correlations between Holes C0006E and C0006F have greater uncertainty. Core recovery in Hole C0006F was low, and therefore MSCL-W logs are incomplete for this hole. Furthermore, the LWD sonic log from Hole C0006B is absent at coring intervals of Hole C0006F, and comparison of MSCL-W NGR data and the LWD gamma ray log does not provide a unique solution. As a result of these complications, the correlation between Holes C0006B and C0006F relies to a greater extent on bedding and structural dips interpreted from seismic reflection data; borehole images from the RAB tool have also been used to correlate data between holes. This proved effective for some thick sand layers that are well matched between Holes C0006E and C00006F.

Depth-shifted profiles are shown in Figure F56 and depth shifts applied to Hole C0006B are given in Table T21. The depth shifts are based on 70 correlations between the five holes. The depth transfer functions were defined by linear regression of the correlated positions. Generally, the depth offsets were <8 m.

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Figure F2. 3-D seismic profile through Sites C0006 and C0007 (see Moore et al.). VE = vertical exaggeration.



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Figure F3. Core recovery and sand and silt distribution, Site C0006. A. Core recovery and lithologic units. CSF = core depth below seafloor. LWD = logging-while-drilling. (Continued on next page.)





Figure F3 (continued). B. Distribution of sand and silt.











Figure F5. Core photographs, Units I and II. **A.** Greenish gray clay with normal fault, Unit I (interval 316-C0006E-3H-2, 40–68 cm). **B.** Thick soupy sand beds separated by ash, Subunit IIA (interval 316-C0006E-7H-1, 10–64 cm). **C.** Graded sands with indistinct upper boundaries, Subunit IIB (interval 316-C0006E-15X-1, 44–84 cm).





Figure F6. Core photographs, Subunits IIC and IID. **A.** Wood-bearing turbidite sand (interval 316-C0006E-45X-7, 60–98 cm). **B.** Wood fragment (Section 316-C0006E-45X-7, 37 cm). **C.** Greenish gray claystone from Subunit IID (interval 316-C0006F-5R-1, 48–74 cm).





Figure F7. Occurrence of ash, Site C0006. **A.** Distribution and thickness of volcanic ash layers. **B.** Glass shards in ash layer (Section 316-C0006E-42X-8, 90 cm). **C.** Lamination in dolomitized ash (Section 316-C0006E-47X-1, 4 cm). **D.** Carbonate-cemented ash with bioturbated top (interval 316-C0006F-12R-1, 12–25 cm). CSF = core depth below seafloor.





Figure F8. XRF phosphorous, Subunits IIB, IIC, and IID. CSF = core depth below seafloor.





Figure F9. Core photographs of typical appearance of mudstone lithologies, Unit III. **A.** Bioturbated greenish gray claystone with abundant *Zoophycos* burrows (interval 316-C0006F-11R-1, 15–28 cm). **B.** Gray claystone with small fault and possible vein structures(?) (interval 316-C0006F-19R-1, 80–104 cm).




Figure F10. Photomicrograph of possible phillipsite (arrows) observed in a smear slide (Section 316-C0006F-19R-1, 119 cm).



150 µm



Figure F11. Computed tomography (CT) number vs. depth, Holes C0006C and C0006D. Average value for each core obtained from ~70 measurements with a 4–10 cm interval. CSF = core depth below seafloor. Orange and red dots = averages for intervals.





Figure F12. Structural observations with distribution and dip angle of bedding, fissility and fault surfaces, and deformation bands vs. depth, Site C0006. Black horizontal lines = intervals of concentrated deformation (probable faults) identified on the basis of multiple lines of evidence (see the "**Expedition 316 methods**" chapter). CSF = core depth below seafloor. LWD = logging-while-drilling.



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N = 42

N = 95



N = 31

Figure F14. Photographs of normal faults in lithologic Unit I (trench to slope transition sediments). **A.** Interval 316-C0006E-3H-9, 44–70 cm. **B.** Interval 316-C0006E-3H-9, 110–137 cm. Half arrows = sense of shear.





Figure F15. Core photographs and corresponding CT images of heterogeneously fractured or brecciated intervals in the upper part of the fractured/brecciated zone. **A.** Intervals 316-C0006E-39X-1 and 39X-2. **B.** Close-up of breccia (interval 316-C0006E-39X-1, 24–43 cm). On the CT image (right side), intervals appearing as non-fractured correspond to drilling mud and fragments injected between more coherent pieces during drilling (biscuiting).



10 cm



2 cm



Figure F16. CT cross-sectional images of a normal fault (interval 316-C0006F-15R-1, 63–83 cm). A. View perpendicular to core axis. **B.** View along the core axis. **C.** Thick slice CT image viewed parallel to strike of the fault; colored lines identify three correlative high CT number markers offset along the fault surface. Sense of shear is normal, and displacement is ~1 cm. With a correction based on paleomagnetic data, normal fault is oriented 068°, 78° northwest. Fault is located just above zone of tectonic breccia located at 533–543 m CSF in Hole C0006F. Half arrows = sense of shear.



3 cm



Figure F17. Lower-hemisphere equal-area projections of all faults from the fractured/brecciated zone, showing the heterogeneity of the data set.





Figure F18. A. CT image of a tectonic joint viewed along the core axis and perpendicular to strike. **B.** Photograph of the joint surface (interval 316-C0006F-18R-1, 89–102 cm). Macroscopic planarity of joint and plumose structures on the surface attest to mode-I opening. With a correction based on paleomagnetic data, the joint is oriented vertical and strikes 155°. The joint is located just below the zone of tectonic breccia located at 533–543 m CSF in Hole C0006F.





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Figure F19. Typical aspects of deformation bands. **A.** Deformation bands showing two oppositely dipping sets (interval 316-C0006E-42X-1, 108–116 cm). **B.** Deformation bands showing kinklike aspect or bifurcation into twin strands (interval 316-C0006E-40X-1, 37–46 cm). **C.** Sediment-filled veins displaced with a reverse sense by deformation bands (interval 316-C0006-41X-6, 105–109 cm). Half arrows = sense of shear, broken lines = black seams deflected by the deformation band showing a reverse sense of shear.



2 cm



Figure F20. Lower-hemisphere equal-area projection of deformation bands after paleomagnetic correction. **A.** Poles to surfaces of deformation bands. **B.** Average of two sets of deformation bands with the plane bisecting the obtuse dihedral angle.





Figure F21. Variation in density of deformation bands with depth in Hole C0006E (150–400 mbsf interval) determined from CT scan images. Linear density determined by counting total number of bands in each core section and dividing by section length for a total of 44 sections. Peaks in density at 240, 292, 312, 335, and 373 m core depth below seafloor (CSF) or abrupt changes in density at 241.3 and 330.8 m CSF are considered possible indicators of fault locations.





Figure F22. Photograph of vertical sand dike (interval 316-C0006E-45X-7, 11–27 cm) (370.18 m CSF). Red dashed lines = boundaries, arrows = biscuiting boundaries filled with mud. The sand dike is cut by biscuiting boundaries, suggesting sand injection is natural in origin.



2 cm



Figure F23. Distribution of deformed intervals along with nonrecovered sections across fractured/brecciated section. CSF = core depth below seafloor. Red arrows = locations of highly deformed intervals (concentrated zones of deformation), which could correspond to faults on the basis of multiple observations of fault-related features (see text).





Figure F24. Images of prominent fracture surface at 235.30 m CSF (interval 316-C0006E-31X-5, 110–128 cm), as it appears in CT scan images. **A.** View along strike of the surface showing true dip of 29° in the direction N133°E, approximately parallel to the plate convergence direction. Also shown are three horizontal slices from (**B**) above, (**C**) through, and (**D**) just below the prominent surface, showing a change in the fracture fabric across the discontinuity.





Figure F25. Photographs of strongly fractured rocks and tectonic breccias (Core 316-C0006E-39X) with corresponding CT images. **A.** Close-up of tectonic protobreccia (interval 316-C0006E-39X-1, 6–12 cm). **B.** Strongly fractured interval (Sections 316-C0006E-39X-1 and 39X-2). Note the presence of relatively intact pieces.









Figure F26. Tectonic breccia at 369 m CSF (Core 316-C0006E-45X). **A.** Close-up photograph and CT image of brecciated mudstone (interval 316-C0006E-45X-5, 46–61 cm). **B.** Boundary (red arrow) between breccia and unbroken intervals.



2 cm



10 cm



Figure F27. Photograph of tectonic breccia (interval 316-C0006F-5R-CC, 11–23 cm).





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Figure F28. Fault rocks in the lower part of the fractured/brecciated zone (Cores 316-C0006E-15R and 16R). **A.** Microbreccia and fault gouge (double arrow) and corresponding CT image (interval 316-C0006F-15R-3, 55–69 cm). **B.** Photomicrograph of fault gouge shown in A, showing composite planar foliation likely of tectonic origin. **C.** Fault breccia and corresponding CT image (interval 316-C0006F-16R-2, 42–58 cm).



2 cm

2 cm



1 mm



Figure F29. Photographs of normal faults in bioturbated hemipelagic mudstone. **A.** Concentration of faults (interval 316-C0006F-7R-1, 54–66 cm). **B.** Normal fault crosscutting sediment-filled veins (interval 316-C0006F-8R-1, 6–11 cm). Half arrows = sense of shear.





2 cm

Figure F30. Location of faults identified on basis of multiple structural observations in Holes C0006E and C0006F with important lithologic and biostratigraphic boundaries indicated, projected on a nearby seismic reflection profile oriented approximately perpendicular to the plate boundary (see **Moore et al.**). Correlation of structurally defined faults with stratigraphic boundaries and inclined seismic reflectors is readily apparent. CSF = core depth below seafloor. VE = vertical exaggeration.





Figure F31. Age vs. depth based on nannofossil events and magnetostratigraphic data, Holes C0006E and C0007F. Gray interval = section containing reworked material, indistinct repetitions, and/or possible hiatus/ erosive events; below gray interval = top of repeated section. CSF = core depth below seafloor.





Figure F32. Magnetic susceptibility and remanent magnetization before (green) and after (purple, red, and blue) 40 mT alternating-field (AF) demagnetization, Holes C0006E and C0007F. **A.** Magnetic susceptibility. **B.** Intensity. **C.** Inclination. **D.** Declination of archive halves. NRM inclinations are biased toward high positive inclinations, suggesting that drilling-induced magnetization is present. AF demagnetization to 40 mT can effectively remove drilling-induced magnetization, as indicated by changes in inclination and intensity. CSF = core depth below seafloor.





Figure F33. Vector endpoint and stereonet magnetization directions showing the results of AF demagnetization for sediments. **A.** Sample 316-C0006E-45X-3, 36–38 cm. **B.** Sample 316-C0006F-8R-1, 6–8 cm. **C.** Sample 316-C0006E-46X-2, 67–69 cm. Black and white squares = projection of magnetization vector endpoint on the horizontal and vertical planes, respectively. NRM = natural remanent magnetization.





Figure F34. Vector endpoint and stereonet magnetization directions showing the results of thermal demagnetization for sediments. **A.** Sample 316-C0006E-39X-2, 38–40 cm. **B.** Sample 316-C0006E-46X-4, 9–11 cm. **C.** Sample 316-C0006F-12R-1, 15–17 cm. Black and white squares = projection of magnetization vector endpoint on the horizontal and vertical planes, respectively. NRM = natural remanent magnetization.





Figure F35. Histogram of inclinations isolated from discrete samples, Holes C0006E and C0006F.





Figure F36. Downhole variation in stable magnetic inclination, inferred polarity, and biostratigraphic zones for sediments, Site C0006. CSF = core depth below seafloor. Black areas = normal polarity, white areas = reversed polarity, hatched area = mixed polarity. AF = alternating field.









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Figure F40. Concentrations of (A) lithium, (B) silica, (C) boron, (D) strontium, (E) potassium, (F) rubidium, and (G) cesium from interstitial waters, Site C0006. CSF = core depth below seafloor. SW = seawater values.







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Figure F43. δ^{18} O isotopic depth profile, Site C0006. CSF = core depth below seafloor. SW = seawater value.



Figure F44. Dissolved methane and ethane concentrations calculated from headspace samples (see Table T16), as well as values of C_1/C_2 in sediments, Site C0006. CSF = core depth below seafloor.







Figure F45. Calcium carbonate (CaCO₃), total organic carbon (TOC), total nitrogen (TN), carbon to nitrogen (C/N) ratio, and total sulfur (TS) in sediments, Site C0006. CSF = core depth below seafloor.


Figure F46. Microbial cell abundance enumerated by microscopic direct count of SYBR Green I–stained cells, Site C0006. CSF = core depth below seafloor.





Figure F47. Fluorescent microscopic image of SYBR Green I–stained cells detected from the accretionary prism close to the lithologic Unit II/III boundary (Section 316-C0006F-3R-2; 414.5 m CSF).



10 µm

Figure F48. Density and porosity measurement results, Holes C0006C, C0006D, C0006E, and C0006F. A. Gamma ray attenuation (GRA) density measured using a multisensor core logger (MSCL) system on whole-round core sections (gray dots) and wet bulk density measured on discrete samples using MAD methods (red dots). **B.** Grain density measured on discrete samples using MAD methods. **C.** MSCL-derived porosity (gray dots) and MAD porosity (red dots). CSF = core depth below seafloor.





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Figure F49. Measurements on discrete samples. A. *P*-wave velocity. **B**. *P*-wave velocity anisotropy. **C**. Electrical conductivity. Black cross = individual measurement, black square = measurement along core axis, red square = average conductivity per sample, green line = LWD bit conductivity data for comparison. **D**. Electrical conductivity anisotropy. For transverse anisotropy, positive values equal lower magnitude along core axis. CSF = core depth below seafloor.





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Figure F50. Thermal data, Site C0006. A. Thermal conductivity. **B.** Equilibrium temperatures (circles) and projected temperatures (line). Best-fit linear gradient to the equilibrium temperature is 27° C/km. C. Temperature as a function of thermal resistance. Best-fit slope gives a heat flow value of 33 mW/m^2 and a bottom water temperature of 2.1° C. CSF = core depth below seafloor.





Figure F51. Temperature time series (blue line), Site C0006. APCT3 measurements at (A) 24.2 m CSF, (B) 38.5 m CSF, and (C) 64.7 m CSF. Unshaded area = data used for equilibrium temperature fit, red line = theoretical equilibrium curve, triangle = beginning of fit, inverted triangle = end of fit, dashed red line with circles = estimate of equilibrium temperature. Note frictional heating at penetration (dashed vertical line) and at pull out. (Continued on next page.)







Figure F51 (continued). DVTP measurements at (D) 98.3 m CSF, (E) 220.3 m CSF, and (F) 277.3 m CSF.



Figure F52. Shear strength measurements from Site C0006 show a general increase with depth with low values corresponding to Subunit IIA and a marked increase at the boundary with Subunit IIB. Penetrometer measurements are consistently higher than those measured with the vane shear apparatus. CSF = core depth below seafloor.











Figure F54. Magnetic susceptibility as a function of depth, Site C0006. CSF = core depth below seafloor.





Figure F55. Natural gamma ray (NGR) values with depth, Site C0006. CSF = core depth below seafloor. cps = counts per second.





Figure F56. Correlations between all holes, Site C0006. A. Correlations between LWD data from Hole C0006B and MSCL-W data from Holes C0006E and C0006F. Numbers below holes are water depth (meters below mean sea level). Correlation positions are given in Table T21. CSF = core depth below seafloor. NGR = natural gamma ray, GR_RAB = gamma ray resistivity at the bit, sonic = sonic velocity. (Continued on next page.)





Figure F56 (continued). B. Correlations of MSCL-W data from Holes C0006C, C0006D, and C0006E.





Recovery

(%)

Table T1. Coring summary, Holes C0006C, C0006D, and C0006E. (See table note.) (Continued on next page.)

Hole C0006C Latitude: 33 Longitude: Seafloor (dr Distance be Water depth Total depth Total depth Total length Total core re Core recover Total number	°01.6458'N 136°47.628 Illers measui tween rig flu (drillers deg ation (core of cored se ecovered (m ry (%): 108 er of cores:	2'E rement f oor and s easurement oth below depth be ction (m b): 10.26 .00	rom rig floo sea level (m ent from se v rig floor, r elow seafloo): 9.5	or, m): 3909.): 28.5 a level, m): 3 n): 3918.50 or, m): 9.50	0 3880.5				
Hole C0006D Latitude: 33 Longitude: Seafloor (dri Distance be Water depth Total depth Total penetr Total length Total core re Core recover Total number	°01.6431'N 136°47.628 Illers measur tween rig flo (drillers me ation (core of cored se ecovered (m ry (%): 107 er of cores:	2'E rement f poor and s easurement oth below depth be ction (m ction (m ction 27 .37	rom rig floc sea level (m ent from se v rig floor, r elow seafloc): 9.5	or, m): 3906.): 28.5 a level, m): 3 m): 3915.50 or, m): 9.50	0 3877.5				
Hole C0006E Latitude: 33 Longitude: Seafloor (dri Distance be Water depth Total depth Total penetr Total length Total length Total core re Core recove Total number	°01.6444'N 136°47.628 illers measur tween rig flø 1 (drillers dep ation (core of cored se ecovered (m ry (%): 80.6 er of cores: 4	2'E rement f oor and s easurement oth below depth be ction (m a): 330.3 58 49	rom rig floc sea level (m ent from se v rig floor, r elow seafloo): 409.4 2	or, m): 3904.): 28.5 a level, m): 3 n): 4313.74 or, m): 409.4	3 3875.8 14				
Core	Date	Loca Shot	l time On deck	Depth [Top	DRF (m) Bottom	Depth Top	CSF (m) Bottom	Advanced (m)	Recovered (m)
316-C0006C- 1H 28	Dec 2007	1812	1846	3909.00	3918.50	0.00	9.50	9.50	10.26

108.00 316-C0006D-1H 28 Dec 2007 1951 2200 3906.00 3915.50 0.00 9.50 9.50 10.20 107.37 316-C0006E-1H 28 Dec 2007 2310 2337 3904.31 3909.50 0.00 5.19 5.19 5.90 113.68 2H 29 Dec 2007 0026 0112 3909.50 3919.00 5.19 14.69 9.50 106.74 10.14 3H 29 Dec 2007 0205 0240 3919.00 3928.50 14.69 24.19 9.50 10.41 109.58 3928.50 4H 29 Dec 2007 0354 0448 3937.53 24.19 33.22 9.03 9.03 100.00 5H 29 Dec 2007 0708 0800 3937.53 5.30 100.00 3942.83 33.22 38.52 5.30 6H 29 Dec 2007 0902 1315 3942.83 3943.00 38.52 38.69 0.17 0.17 100.00 7H 3943.00 29 Dec 2007 1955 2037 3952.50 38.69 48.19 9.50 10.32 108.63 8H 29 Dec 2007 2154 2244 3952.50 3962.00 48.19 57.69 9.50 10.63 111.89 9H 30 Dec 2007 0003 0056 3962.00 3968.82 57.69 64.51 6.82 6.82 100.00 10H 30 Dec 2007 3968.82 3968.98 100.00 0307 0359 64.51 64.67 0.16 0.16 11H 30 Dec 2007 0523 0633 3968.98 3975.79 64.67 71.48 6.81 6.81 100.00 3975.79 6.34 12H 30 Dec 2007 0756 0840 3982.13 71.48 77.82 6.34 100.00 13H 30 Dec 2007 1001 1049 3982.13 3983.64 77.82 79.33 1.51 1.51 100.00 14H 30 Dec 2007 1225 1310 3983.64 3983.64 79.33 79.33 0.00 0.00 0.00 30 Dec 2007 15X 1435 1548 3983.64 3993.14 79.33 88.83 9.50 5.80 61.05 16X 30 Dec 2007 1730 3993.14 4002.64 88.83 98.33 9.50 2.03 21.37 1643 17X 30 Dec 2007 2135 4002.64 98.33 106.33 45.38 2225 4010.64 8.00 3.63 18X 30 Dec 2007 2327 0022 4010.64 4020.14 106.33 115.83 9.50 1.66 17.47 19X 31 Dec 2007 0057 0157 4020.14 4029.64 115.83 125.33 9.50 5.15 54.21 20X 31 Dec 2007 0240 0325 4029.64 4039.14 125.33 134.83 9.50 7.88 82.95 1 Jan 2008 1617 4039.14 4048.64 134.83 144.33 4.78 50.32 21X 1711 9.50 22X 1 Jan 2008 1825 1923 4048.64 4058.14 144.33 153.83 9.50 7.30 76.84 23X 1 Jan 2008 2005 2058 4058.14 4067.64 153.83 163.33 9.50 8.53 89.79 4077.14 24X 0427 2 Jan 2008 0515 4067.64 163.33 172.83 9.50 1.55 16.32



Table T1 (continued).

		Loca	al time	Depth I	DRF (m)	Depth	CSF (m)	Advanced	Recovered	Recovery
Core	Date	Shot	On deck	Тор	Bottom	Тор	Bottom	(m)	(m)	(%)
25X	2 Jan 2008	0705	0758	4077.14	4086.64	172.83	182.33	9.50	9.07	95.47
26X	2 Jan 2008	1108	1335	4086.64	4096.14	182.33	191.83	9.50	9.99	105.16
27X	2 Jan 2008	1748	1954	4096.14	4105.64	191.83	201.33	9.50	10.03	105.58
28X	2 Jan 2008	2054	2250	4105.64	4115.14	201.33	210.83	9.50	4.04	42.53
29X	3 Jan 2008	0405	0603	4115.14	4124.64	210.83	220.33	9.50	10.00	105.26
30X	3 Jan 2008	1107	1317	4124.64	4134.14	220.33	229.83	9.50	9.87	103.89
31X	3 Jan 2008	1412	1625	4134.14	4143.64	229.83	239.33	9.50	5.92	62.32
32X	3 Jan 2008	1748	1936	4143.64	4153.14	239.33	248.83	9.50	9.00	94.74
33X	3 Jan 2008	2050	2245	4153.14	4162.64	248.83	258.33	9.50	0.00	0.00
34X	4 Jan 2008	0033	0301	4162.64	4172.14	258.33	267.83	9.50	8.60	90.53
35X	4 Jan 2008	0458	0722	4172.14	4181.64	267.83	277.33	9.50	3.68	38.74
36X	4 Jan 2008	1150	1358	4181.64	4191.14	277.33	286.83	9.50	9.83	103.47
37X	4 Jan 2008	1516	1722	4191.14	4200.64	286.83	296.33	9.50	9.08	95.58
38X	4 Jan 2008	1840	2035	4200.64	4210.14	296.33	305.83	9.50	1.32	13.89
39X	4 Jan 2008	2158	2337	4210.14	4219.64	305.83	315.33	9.50	9.91	104.32
40X	5 Jan 2008	0108	0319	4219.64	4229.14	315.33	324.83	9.50	8.78	92.42
41X	5 Jan 2008	0424	0616	4229.14	4238.64	324.83	334.33	9.50	7.15	75.26
42X	5 Jan 2008	0826	1047	4238.64	4248.14	334.33	343.83	9.50	9.88	104.00
43X	5 Jan 2008	1532	1751	4248.14	4257.64	343.83	353.33	9.50	8.54	89.89
44X	5 Jan 2008	2012	2209	4257.64	4267.14	353.33	362.83	9.50	9.89	104.11
45X	5 Jan 2008	2332	0123	4267.14	4276.64	362.83	372.33	9.50	9.89	104.11
46X	6 Jan 2008	0332	0523	4276.64	4286.14	372.33	381.83	9.50	8.30	87.37
47X	6 Jan 2008	0734	0935	4286.14	4295.64	381.83	391.33	9.50	9.82	103.37
48X	6 Jan 2008	1104	1320	4295.64	4305.14	391.33	400.83	9.50	9.84	103.58
49X	6 Jan 2008	1622	0333	4305.14	4313.75	400.83	409.44	8.61	6.04	70.15

Note: DRF = drillers depth below rig floor, CSF = core depth below seafloor.



Table T2. Coring summary, Hole C0006F. (See table note.)

Hole	C0006F

Latitude: 33°01.6242'N Longitude: 136°47.6282'E Seafloor (drillers measurement from rig floor, m): 3904.0 Distance between rig floor and sea level (m): 28.5 Water depth (drillers measurement from sea level, m): 3875.5 Total depth (drillers depth below rig floor, m): 4507.00 Total penetration (core depth below seafloor, m): 208.00 Total length of cored section (m): 208.0 Total core recovered (m): 56.48 Core recovery (%): 27.15 Total number of cores: 23

	Date	Loc	al time	Depth I	DRF (m)	Depth (CSF (m)	Advanced	Recovered	Recoverv
Core	(Jan 2008)	Shot	On deck	Тор	Bottom	Тор	Bottom	(m)	(m)	(%)
316-C0	006F-									
1R	9	0202	0355	4299.0	4308.5	395.00	404.50	9.50	2.16	22.74
2R	9	0509	0712	4308.5	4318.0	404.50	414.00	9.50	2.66	28.00
3R	9	0838	1038	4318.0	4327.5	414.00	423.50	9.50	1.91	20.11
4R	9	1148	1352	4327.5	4337.0	423.50	433.00	9.50	2.26	23.79
5R	9	1443	1649	4337.0	4342.0	433.00	438.00	5.00	1.88	37.60
6R	9	1828	2019	4342.0	4351.5	438.00	447.50	9.50	1.96	20.63
7R	9	2218	0001	4351.5	4361.0	447.50	457.00	9.50	2.49	26.21
8R	10	0130	0334	4361.0	4370.5	457.00	466.50	9.50	2.21	23.26
9R	10	0432	0620	4370.5	4380.0	466.50	476.00	9.50	2.33	24.53
10R	10	0721	0938	4380.0	4389.5	476.00	485.50	9.50	1.89	19.89
11R	10	1022	1231	4389.5	4399.0	485.50	495.00	9.50	2.50	26.32
12R	10	1335	1518	4399.0	4408.5	495.00	504.50	9.50	2.75	28.95
13R	10	1639	1816	4408.5	4418.0	504.50	514.00	9.50	3.04	32.00
14R	10	1931	2103	4418.0	4427.5	514.00	523.50	9.50	4.38	46.11
15R	10	2234	0013	4427.5	4437.0	523.50	533.00	9.50	3.48	36.63
16R	11	0123	0326	4437.0	4446.5	533.00	542.50	9.50	2.30	24.21
17R	11	0441	0648	4446.5	4456.0	542.50	552.00	9.50	2.08	21.89
18R	11	0906	1054	4456.0	4465.5	552.00	561.50	9.50	1.99	20.95
19R	11	1329	1504	4465.5	4475.0	561.50	571.00	9.50	6.47	68.11
20R	11	1738	1924	4475.0	4484.5	571.00	580.50	9.50	2.61	27.47
21R	11	2219	0059	4484.5	4494.0	580.50	590.00	9.50	0.10	1.05
22R	11	0740	0927	4494.0	4497.5	590.00	593.50	3.50	2.08	59.43
23R	13	0257	0735	4497.5	4507.0	593.50	603.00	9.50	0.95	10.00

Note: DRF = drillers depth below rig floor, CSF = core depth below seafloor.



Table T3. Summary of lithologic units, Holes C0006E and C0006F. (See table note.)

	Hole, core, section	on, interval (cm)	Depth	CSF (m)	Thickness	Stratigraphic	Lithologic	Processes
Unit	Тор	Bottom	Тор	Bottom	(m)	age	description	of formation
	316-	316-						
I	C0006E-1H-1, 0	C0006E-4H-3, 20	0.00	27.23	27.2	Pleistocene	Nannofossil-bearing mud, interbedded sand layers, and a volcanic ash layer near the base	Hemipelagic settling, turbidites, and a volcanic ash layer
IIA	C0006E-4H-3, 20	C0006E-12H-2, 10	27.23	72.06	44.8	Pleistocene	Thick to thin sands with thin interbedded nannofossil-bearing mud layers and a volcanic ash layer	Turbidites, hemipelagic settling, and a volcanic ash layer
IIB	C0006E-12H-2, 10	C0006E-24X-1, 0	72.06	163.33	91.3	Pleistocene	Sands interbedded with nannofossil-bearing mud, rare volcanic ash layers	Turbidites, hemipelagic settling, and rare volcanic ash layers
IIC	C0006E-24X-1, 0	C0006E-48X-1, 0	163.33	391.33	228.0	Pleistocene	Mud with sand/silt layers and rare volcanic layers	Hemipelagic settling, thin- bedded turbidites, and rare volcanic ash falls
IID	C0006E-48X-1, 0	C0006F-7R-CC, 33.5	391.33	449.67	58.3	Pleistocene	Mud with volcanic ash layers and rare thin silt layers	Hemipelagic settling, volcanic ash layers, and rare thin-bedded turbidites
Ш	C0006F-7R-CC, 33.5	C0006F-23R-CC, 21	449.67	603.00	153.3	Pleistocene to Miocene	Mud with tuff layers	Hemipelagic settling and rare volcanic ash layers

Note: CSF = core depth below seafloor.

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													/	Abunda	nce ca	lculate	d from S	VD norn	nalizati	on fact	or	
				Peak	intensity	(counts	s/step)	Integra	ted peak	area (tota	counts)		Calcula	ated ab	undan	ce (wt%	%)	Nor	malize	d abun	dance ((wt%)
						ase				ase				ase		g				ase		
Unit	Hole, core, section, interval (cm)	Core type	Depth CSF (m)	Clay	Quartz	Plagiocla	Calcite	Clay	Quartz	Plagioclé	Calcite	Clay	Quartz	Plagioclá	Calcite	Correcte calcite	Absolute total	Clay	Quartz	Plagiocla	Calcite	Relative total
	316-																					
1	C0006E-1H-2, 0–1.5	WR	1.21	73	1.502	337	72	2,492	48.028	22.806	2.268	39.1	26.9	28.3	-1.2	0.0	94.2	41.5	28.5	30.0	0.0	100
	C0006D-1H-2, 0-1.5	WR	1.21	50	1.023	287	96	3.013	45,127	22,477	3,804	44.2	25.1	27.8	0.5	0.5	97.6	45.3	25.7	28.5	0.5	100
	C0006C-1H-2, 0–1.5	WR	1.27	58	1.046	296	182	2.227	36,213	19.521	6,135	34.8	20.1	24.4	4.5	4.5	83.8	41.5	24.0	29.1	5.4	100
	C0006D-1H-2, 20–21.5	WR	1.41	54	1.333	346	119	2.212	44,939	24,479	3,496	37.7	25.0	30.8	0.7	0.7	94.2	40.1	26.6	32.7	0.7	100
	C0006E-1H-4, 69.5-71	WR	3.53	75	1.374	286	20	2.597	43,753	21,168	1,385	39.1	24.4	26.2	-2.2	0.0	89.7	43.6	27.2	29.2	0.0	100
	C0006D-1H-5, 0-1.5	WR	4.04	68	1.242	284	118	2.754	38,031	17,717	5,457	38.6	21.2	21.7	3.3	3.3	84.7	45.5	25.0	25.6	3.9	100
	C0006E-1H-5, 0-1.5	WR	4.24	78	, 1.750	388	85	1.934	53,198	26,172	2.630	35.8	29.9	32.8	-0.6	0.0	98.4	36.4	30.3	33.3	0.0	100
	C0006E-1H-6, 49.5-51	WR	4.97	66	1,192	230	130	2.682	37,509	15,697	4,398	36.4	21.0	18.9	2.0	2.0	78.3	46.4	26.8	24.2	2.6	100
	C0006C-1H-6, 0-1.5	WR	5.97	85	1.475	260	72	2,512	45,498	20.002	2.423	37.4	25.5	24.5	-0.8	0.0	87.4	42.8	29.2	28.1	0.0	100
	C0006E-2H-3, 0-1.5	WR	7.79	66	1.430	296	77	2.551	43,158	18,377	2.757	36.7	24.2	22.4	-0.3	0.0	83.3	44.1	29.0	26.9	0.0	100
	C0006E-2H-4, 115.5-117	WR	9.18	58	1.137	305	190	2,491	39,127	19,912	7.366	37.6	21.8	24.7	5.9	5.9	89.9	41.8	24.2	27.5	6.5	100
	C0006E-2H-7, 0-1.5	WR	12.09	58	1.310	401	159	2,528	43,545	25,505	5.520	41.8	24.1	32.2	3.1	3.1	101.1	41.3	23.9	31.8	3.0	100
	C0006E-3H-3, 0–1.5	WR	17.29	55	1.692	376	63	2.008	53,637	25.095	1.879	35.7	30.1	31.3	-1.6	0.0	97.1	36.8	31.0	32.2	0.0	100
	C0006E-3H-6, 55–56.5	WR	20.98	72	949	275	136	3,157	28,088	16,714	4,404	42.3	15.3	20.7	2.0	2.0	80.2	52.7	19.1	25.8	2.4	100
	C0006E-3H-6, 95–96,5	WR	21.38	69	1.255	250	250	2.613	42.754	17.744	8.129	37.1	24.0	21.5	6.7	6.7	89.3	41.5	26.9	24.1	7.5	100
	C0006E-3H-7, 0–1,5	WR	21.66	61	1.457	347	164	2.449	44.827	21.539	5.744	38.0	25.1	26.7	3.5	3.5	93.3	40.8	26.9	28.6	3.8	100
	C0006E-3H-7, 0–1.5	WR	21.66	69	1.401	375	36	2.962	49.088	23.772	1.060	44.3	27.4	29.4	-3.2	0.0	101.1	43.9	27.1	29.1	0.0	100
	C0006E-4H-4, 29,5–31	WR	28.74	57	1.479	396	105	2.236	47.307	26.887	2.165	39.6	26.3	34.0	-1.3	0.0	99.8	39.6	26.4	34.0	0.0	100
	C0006E-4H-5_0-1_5	WR	29.92	53	1.521	485	64	2.027	46.871	33,140	2,412	42.1	25.8	42.6	-1.0	0.0	110.5	38.1	23.4	38.6	0.0	100
	C0006F-5H-1, 126 5-128	WR	34.49	68	1,110	250	55	3,201	35,218	19.069	1,173	43.9	19.4	23.5	-2.6	0.0	86.9	50.6	22.3	27.1	0.0	100
	C0006E-5H-3, 0–1,5	WR	35.84	54	1.621	703	62	1.657	51.647	42.159	1.215	44.7	28.3	54.9	-2.8	0.0	127.9	35.0	22.1	42.9	0.0	100
	C0006E-5H-4, 20–21.5	WR	36.26	51	1.340	617	61	1.673	43.820	34.518	1.926	39.7	24.0	44.8	-1.3	0.0	108.5	36.6	22.1	41.3	0.0	100
	C0006E-5H-5, 70-71.5	WR	38.20	48	2.142	851	37	1.190	62,199	46.300	1.192	42.6	34.4	60.2	-2.9	0.0	137.2	31.0	25.1	43.9	0.0	100
	C0006E-7H-2, 115,5–117	WR	41.25	47	1.442	439	60	624	44.469	32.271	2.016	27.7	24.7	42.0	-0.4	0.0	94.3	29.3	26.2	44.5	0.0	100
	C0006E-7H-4, 0–1.5	WR	42.92	43	1.988	866	45	813	60.897	52.569	1.392	43.5	33.4	69.0	-2.6	0.0	145.9	29.8	22.9	47.3	0.0	100
	C0006E-7H-4, 20,5–22	WR	43.12	61	2.136	581	56	733	60.418	37.724	1.537	31.9	33.8	48.6	-1.8	0.0	114.4	27.9	29.5	42.5	0.0	100
	C0006E-8H-1, 55–56.5	WR	48.74	65	1.300	355	102	2.675	41.841	21.350	3.214	40.2	23.3	26.5	0.2	0.2	90.1	44.6	25.8	29.4	0.2	100
IIA	C0006F-8H-2_86_5-88	WR	50.45	57	2,354	976	41	721	66 420	51,194	1,423	41.3	36.7	66.8	-2.6	0.0	144.9	28.5	25.4	46.1	0.0	100
	C0006E-8H-4_0-1_5	WR	51.79	52	1,228	266	136	2.827	38,415	20,707	4,227	41.4	21.3	25.7	1.5	1.5	89.9	46.1	23.6	28.6	1.7	100
	C0006F-9H-2 93-94 5	WR	60.04	51	1,133	320	107	2,722	35,124	21.055	3,640	40.8	19.3	26.4	0.9	0.9	87.4	46.6	22.1	30.2	1.0	100
	C0006E-9H-5_0-1_5	WR	62.41	53	1,984	484	42	926	61.022	31,881	1,511	29.6	34.4	40.5	-1.8	0.0	104.5	28.3	32.9	38.8	0.0	100
	C0006F-10H-8, 0–1, 5	WR	64.51	58	1,741	550	57	1.137	50.687	30,665	1,550	31.2	28.3	39.3	-1.5	0.0	98.9	31.6	28.6	39.8	0.0	100
	C0006F-11H-1, 79–81	WR	65.46	66	1,237	287	38	3,099	38,716	20,212	1,441	43.6	21.4	25.0	-2.3	0.0	90.0	48.5	23.8	27.8	0.0	100
	C0006E-11H-4, 0–1.5	WR	67.70	46	2,066	447	52	1.452	60,935	30.851	1.522	34.0	34.3	39.0	-2.1	0.0	107.3	31.7	31.9	36.3	0.0	100
	C0006E-12H-6_0-1_5	W/R	76 31	52	1 487	432	67	2 1 1 8	46 132	29 603	2 232	40.4	25.5	37.8	_1 1	0.0	107.5	39.0	24.6	36.4	0.0	100
	C0006E-15X-4 0–1 5	W/R	81 76	59	1,10,	288	80	2 795	47 542	21 115	2 3 9 7	40.9	26.6	25.9	_1.1	0.0	93.4	43.8	28.5	27.7	0.0	100
	C0006E-16X-1, 0-1.5	W/R	89.80	76	1,000	528	54	2,725	43 853	26 852	1 9 2 9	46.5	20.0	33.9	_2.0	0.0	104.6	44 5	23.1	32.4	0.0	100
	C0006E-16X-2, 0-1.5	W/R	90.11	59	1 592	446	63	2,250	48 692	28,032	2 1 7 2	40.5	27.1	35.5	_1 3	0.0	103.0	39.3	26.3	34.4	0.0	100
	C0006E-17X-1 115 5-117	W/R	99.49	61	1 470	601	55	1 962	49 849	35 4 39	1 823	42.9	27.5	45.7	_1.9	0.0	116.1	37.0	23.7	39.3	0.0	100
	C0006E-17X-3_0_1_5	W/R	100.30	61	1,470	446	47	1 880	49 918	26 851	1,025	35.9	27.9	33.0	_2.0	0.0	97.7	36.7	28.6	34.7	0.0	100
	C0006E-17X-5, 27 5-29	W/R	101.30	61	1 279	482	107	1 589	42 371	36 680	4 360	40.6	27.7	47.8	1 9	1 9	113.4	35.8	20.0	42.2	17	100
	C0006E-19X-3 113 5-115	W/R	118 40	63	1 211	468	67	1 738	41 678	28 805	1 905	36.3	23.0	37.0	_1.7	0.0	963	37.7	23.9	38.4	0.0	100
	C0006F-19X-4 95 5-97	\//R	119.40	50	1 1 7 4	322	56	2 286	40 391	20,005	1 281	38.7	22.0	31 3	_2.2	0.0	923	42.0	24.2	33.9	0.0	100
	C0006E-19X-5, 0-1.5	W/R	119.02	52	1 040	304	64	2,200	37 665	20 502	1 995	41 1	20.8	25.5	_1 4	0.0	87.5	47.0	23.8	29.2	0.0	100
	C0006E-19X-6 39_40 5	\A/D	120 47	61	1 054	260	138	2,020	3/ 350	18 620	1 7 77	40.5	10.0	23.5	2 3	23	84.8	47.7	22.0	27.2	2.7	100

Table T4. XRD data, Site C0006. (See table notes.) (Continued on next four pages.)



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Table T4 (continued). (Continued on next page.)

Interval Path														A	Abunda	nce ca	lculate	d from S	VD norn	nalizati	on facto	or	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					Peak i	ntensity	(counts	/step)	Integra	ted peak	area (total	counts)		Calcula	ated ab	undan	ce (wt	%)	Nor	malized	d abund	lance (wt%)
Hole, corr, section, interval (cm) Core Uppe Despti CSF (m) Despti CSF (m) <thdespticsf (m)<="" th=""> Despti CSF (m)</thdespticsf>							e				e				e		-				e		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$						N	clas			N	clas			N	clas		tec	Ite		N	clas		e
Unit interval (cm) type CSF (m) G G G G <td></td> <td>Hole, core, section,</td> <td>Core</td> <td>Depth</td> <td>></td> <td>artz</td> <td>.õj</td> <td>cite</td> <td>></td> <td>artz</td> <td>.ē</td> <td>cite</td> <td>></td> <td>artz</td> <td>.ē</td> <td>cite</td> <td>rec</td> <td></td> <td>></td> <td>artz</td> <td>.ē</td> <td>cite</td> <td>ativ</td>		Hole, core, section,	Core	Depth	>	artz	.õj	cite	>	artz	.ē	cite	>	artz	.ē	cite	rec		>	artz	.ē	cite	ativ
C0006E 20X1, 38.5-40 WR 125.72 44 1,316 590 73 1,084 45.915 41,393 2,284 38.8 25.1 54.3 -0.7 0.0 118.1 32.8 21.2 45.9 0.0 100 C0006E 20X-1, 125120 WR 127.9 51 1.32 327 64 1,357 1,757 1,951 2.22 41.2 1.8 1.1 1.2 0.0 82.0 32.6 8.0 100 C0006E 20X5, 31.6-53 WR 13.457 77.2 26 78 3.01 100 35.6 19.744 3.652 45.1 74.4 4.04 4.04 4.01 2.4 50 100 C0006E 21X.2 4.04 4.01 3.4 57.7 3.4 0.0 100 C0006E 21X.2 4.04 1.8 1.27 4.0 1.08 4.21 4.02 2.21 1.1 6.0 1.8 3.7 1.0 1.21 1.26 0.0 1.16 4.02 1.21 </td <td>Unit</td> <td>interval (cm)</td> <td>type</td> <td>CSF (m)</td> <td>Cla</td> <td>Ŋu</td> <td>Pla</td> <td>Cal</td> <td>Cla</td> <td>ηQ</td> <td>Pla</td> <td>Cal</td> <td>Cla</td> <td>Ŋ</td> <td>Pla</td> <td>Cal</td> <td>calo Co</td> <td>Abs tot</td> <td>Cla</td> <td>Ŋ</td> <td>Pla</td> <td>Cal</td> <td>Rel</td>	Unit	interval (cm)	type	CSF (m)	Cla	Ŋu	Pla	Cal	Cla	ηQ	Pla	Cal	Cla	Ŋ	Pla	Cal	calo Co	Abs tot	Cla	Ŋ	Pla	Cal	Rel
c00066_20X.1 ls5-120 WR l252.6 69 l,942 l2580 30.871 l,16 40.0 21.6 40.0 -1.6 0.0 10.04 99.8 20.0 100 C00066_20X3, 0-1.5 WR 13.18 67 1.22 67 8 1.357 1.787 1.787 1.7877 1.7877 1.7877 1.7877 1.7877 1.7877 1.788 3.27 1.788 3.27 1.7873 1.788 3.27 1.7873 3.839 -0.7 0.0 1.207 2.217 3.53 1.001		C0006E-20X-1, 38.5-40	WR	125.72	44	1,316	590	73	1,084	45,915	41,393	2,284	38.8	25.1	54.3	-0.7	0.0	118.1	32.8	21.2	45.9	0.0	100
c c c 3,65 9,026 1,591 2,222 41.2 21.8 9,1<-1,2 0.0 82.0 92.6 52.3 0.1 0.0 82.0 82.0 22.6 53.3 0.0 100 0 0 0 0 0 0.0		C0006E-20X-1, 118.5–120	WR	126.52	69	1,159	327	69	, 1,942	37,580	30,871	1,616	40.0	20.5	40.0	-1.6	0.0	100.4	39.8	20.4	39.8	0.0	100
c c		C0006E-20X-2, 121.5–123	WR	127.96	95	1,049	239	76	3,165	39,026	15,951	2,222	41.2	21.8	19.1	-1.2	0.0	82.0	50.2	26.5	23.3	0.0	100
c c c y		C0006E-20X-3, 0-1.5	WR	128.16	68	1.244	256	63	3.270	41.357	17.877	, 1,943	43.5	23.0	21.6	-1.8	0.0	88.1	49.4	26.1	24.5	0.0	100
CONORE-22X-5, DB-109-5 WR 132.09 50 1,21 399 99 2,162 40,52 26,73 40,9 90 2,162 40,52 26,73 40,9 90,2 13,4 40,44 32,33 26,66 33,32 21,41 90,0 00 00,0 95,4 40,9 21,64 40,9 21,64 40,9 22,3 40,0 10,2 37,4 10,0 10,0 00,0 95,4 40,9 21,64 43,25 20,0 10,0 10,0 95,2 42,2 11,3 0,1 00 00,0 95,2 42,2 11,3 10,0 10,0 10,0 95,2 43,2 21,1 31,1 21,1		C0006E-20X-5, 33.5-35	WR	131.34	57	772	256	78	3,401	35.836	19,744	3.652	46.5	19.7	24.4	0.4	0.4	91.0	51.1	21.6	26.8	0.5	100
C0006-20X, 70-15 WR 13 28 5 52 1 319 508 73 1.678 40.474 32 32 2.658 38 22.1 41.9 -0.2 0.0 24.7 21.6 40.9 0.0 100 C00066-21X.3 0-15 WR 187.38 70 1.981 370 71 2.084 33.78 2.599 2.39 1.5 3.24 3.90 0.977 53.1 2.38 2.10 0.868 4.61 2.42 2.11 3.67 0.0 100 C00066-22X.3, 30-15 WR 146.07 59 1.204 24 2.798 4.119 19.435 1.708 4.00 2.29 4.10 0.0 8.64 6.67 2.144 1.815 3.48 2.61 3.17 -1.4 0.0 8.64 6.67 2.144 1.815 3.48 2.61 3.17 1.40 0.0 1.00 8.64 2.22 2.87 0.0 100 0.00 2.62 3.87 2.22 3.87 2.22 <td></td> <td>C0006E-20X-5, 108-109.5</td> <td>WR</td> <td>132.09</td> <td>50</td> <td>1.231</td> <td>399</td> <td>99</td> <td>2.162</td> <td>40.527</td> <td>26.678</td> <td>2.898</td> <td>39.0</td> <td>22.3</td> <td>34.0</td> <td>0.0</td> <td>0.0</td> <td>95.4</td> <td>40.9</td> <td>23.4</td> <td>35.7</td> <td>0.0</td> <td>100</td>		C0006E-20X-5, 108-109.5	WR	132.09	50	1.231	399	99	2.162	40.527	26.678	2.898	39.0	22.3	34.0	0.0	0.0	95.4	40.9	23.4	35.7	0.0	100
C0006-21X-2 C0006-21X-3 C-1		C0006E-20X-7, 0–1.5	WR	132.85	52	1.319	508	73	1.678	40.447	32.339	2.636	38.3	22.1	41.9	-0.2	0.0	102.4	37.4	21.6	40.9	0.0	100
C0006E-21X-3, 0-15 WR 137.38 70 1091 370 71 2.084 34.378 2.394 3.27 18.8 32.7 0.0 000 89.2 22.2 21.1 36.7 0.0 100 IB C0006E-21X-3, 33-34.5 WR 146.07 59 1,204 29.4 82 2,798 41,199 19.455 1,908 40.0 22.9 2.16 40.0 86.8 61.1 24.4 27.5 40.7 21.2 18.5 -0.5 0.0 86.8 61.1 24.4 27.5 40.7 21.2 18.5 -0.5 0.0 86.8 61.1 24.0 10.0 102.0 86.6 40.7 2.13 46.007 24.71 48.77 2.21 15.1 0.0 11.0 01.00 01.0 02.0 88.7 0.1 10.0 10.2 0.8 24.27 10.0 11.0 10.2 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0		C0006E-21X-2 94–96	W	137.22	60	1.584	398	76	1.816	47.423	26.752	2.318	35.3	26.4	33.9	-0.7	0.0	95.7	36.9	27.7	35.4	0.0	100
C0006E-21X-4 3-5 W 137/23 89 '994 217 78 33/04 34/239 7.168 42.3 19.0 164 -12 00 79.7 53.1 23.8 23.1 0.0 100 IBB C00066-22X-3, 0-1.5 WR 146.83 53 1,485 360 2,5144 1,815 34.8 26.1 31.7 -1.4 0.0 92.6 36.2 24.2 2.0 100 C00066-22X-4, 0-3.1.5 WR 147.48 64 1,173 21.1 78 3,143 38,102 1,46,403 22.4 3.0 2.4 0.0 100.0 38.9 2.2 3.9 -2.4 0.0 101.0 38.9 2.6 3.4 0.0 100 100 100 38.9 2.6 3.4 0.0 100 100 100 1.4 2.5 3.0 0.0 100 1.4 2.5 3.0 0.0 100 1.4 2.5 3.0 1.0 1.00 <t< td=""><td></td><td>C0006E-21X-3. 0–1.5</td><td>WR</td><td>137.38</td><td>70</td><td>1.091</td><td>370</td><td>71</td><td>2.084</td><td>34.378</td><td>25.499</td><td>2.394</td><td>37.7</td><td>18.8</td><td>32.7</td><td>-0.4</td><td>0.0</td><td>89.2</td><td>42.2</td><td>21.1</td><td>36.7</td><td>0.0</td><td>100</td></t<>		C0006E-21X-3. 0–1.5	WR	137.38	70	1.091	370	71	2.084	34.378	25.499	2.394	37.7	18.8	32.7	-0.4	0.0	89.2	42.2	21.1	36.7	0.0	100
IB C0006E-22X-3 33.4.5 WR 146.07 59 1,204 22,798 41,189 1,9435 1,908 40.0 22.9 23.9 -1.6 0.0 86.8 4.6.1 26.4 22.7 0.0 100 C0006E-22X-4, 30-31.5 WR 146.83 53 1,485 360 55 1,884 46.673 2,124 1,815 4.0.0 2,22 43.9 -2.4 0.0 13.5 19.00 2.2 38.7 0.0 100 C0006E-22X-4, 105-116.5 WR 148.35 1,524 47.3 51 2,183 46,008 34,087 1,461 44.3 25.2 43.9 -2.4 0.0 113.5 39.0 2.2 3.8 0.0 100 100 100 10.0 13.5 49.0 1.0 11.9 13.5 49.0 1.0 11.9 13.6 40.0 100 100 100 14.8 71 1.0 1.257 40.0 100 100 14.4 13.5 11.94 40.0 100 100 100 100 100 10.0		C0006E-21X-4, 3–5	W	137.73	89	994	217	78	3.304	34.239	15.301	2.168	42.3	19.0	18.4	-1.2	0.0	79.7	53.1	23.8	23.1	0.0	100
C0006E-22X-3, 0-1.5 WR 146.83 53 1,884 46,673 25,144 1,815 34.8 26.1 31.7 24 0.0 92.6 37.6 28.1 34.2 0.0 100 C0006E-22X-3, 0-1.5 WR 147.48 64 1,173 211 78 3,143 38,102 12,15 30.0 80.4 50.0 80.4 50.0 80.4 50.0 80.4 50.0 80.4 50.0 80.0 100 C0006E-22X-4, 10-15 WR 150.20 58 1,665 409 76 2,191 48,797 2,773 2,358 39.7 27.2 35.1 1-11 0.0 102.0 89.2 65.4 40.0 100 C0006E-23X-1, 65-665 WR 154.48 58 1,043 226 90 3,453 39.96 2,461 46.02 2,150 41.4 25.5 33.0 10 100.0 100 120.0 83.0 20.0 100 100 120.0	IIB	C0006E-22X-2, 33–34.5	WR	146.07	59	1.204	294	82	2.798	41.189	19.435	1.908	40.0	22.9	23.9	-1.6	0.0	86.8	46.1	26.4	27.5	0.0	100
C0006E-22X-4, 30.31,5 WR 147.48 64 1,173 211 78 3,143 38,102 15,450 2,725 40.7 21.2 18.5 -0.5 0.0 80.0 50.6 24.4 23.0 0.0 100 C0006E-22X-4, 115-116.5 WR 148.33 61 1,534 473 51 2,183 46.0 34.087 1,777 2,588 39.72 23.51 -11 0.0 110.5 39.0 26.6 34.4 0.0 100 C0006E-23X-4, 66-67.5 WR 154.48 85 1,043 27.0 93.15 49.5 -1.9 0.0 119.1 31.9 26.5 34.6 0.0 100 C0006E-23X-4, 10-1-102.5 WR 154.48 78 1,041 27.5 59 3,09 40,99 16,292 1,506 42.7 22.9 1,4 40.0 180.0 150.0 32.0 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100		C0006E-22X-3_0-1_5	WR	146.83	53	1,485	360	55	1.884	46 673	25,144	1,815	34.8	26.1	31.7	-1.4	0.0	92.6	37.6	28.1	34.2	0.0	100
C0006E-22X-4, 115-116.5 WR 148.33 61 1,534 473 51 2,183 46,008 34,087 1,461 44.3 25.2 3.9 -2.4 0.0 113.5 39.0 22.2 38.7 0.0 100 C0006E-22X-6, 6-6.75 WR 150.66 51 7.2 35.1 1.1 1.9 1.0 102.0 38.9 22.2 38.7 0.0 100 C0006E-22X-6, 6-6.5 WR 154.48 78 1.043 22.6 90 3.433 37.95 16.166 31.54 44.3 21.1 19.4 -0.2 0.0 84.7 52.3 2.9 2.2 40.6 0.0 100 C0006E-23X-1, 01-102.5 WR 154.84 77 1,501 47.95 88 3.489 14.347 2.350 41.7 1.2 0.0 80.7 50.0 3.0 1.0 100 0.0 100 0.0 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 10		C0006F-22X-4 30-31.5	WR	147.48	64	1,173	211	78	3,143	38,102	15,450	2,725	40.7	21.2	18.5	-0.5	0.0	80.4	50.6	26.4	23.0	0.0	100
C0006E-22X-6, 20-21.5 WR 150.20 58 1,665 409 76 2,109 48,99 27,773 2,358 39.7 27.2 35.1 -1.1 0.0 102. 38.9 26.6 34.4 0.0 100 C0006E-22X-6, 66-67.5 WR 150.26 56 1,729 58 52 1,287 56,793 38,329 1,678 38.0 31.5 49.5 -1.9 0.0 119.1 31.9 26.5 4.6 0.0 100 C0006E-23X-1, 65-665 WR 154.48 58 1,043 226 90 3,453 37,956 16,166 3,154 44.3 21.1 94 -0.2 00 84.7 52.3 24.9 22.8 0.0 100 C0006E-23X-3, 67-68.5 WR 154.84 57 1,510 413 71 2,469 46,027 2,6194 2,185 41.4 25.5 33.0 -1.3 0.0 100.0 41.4 25.6 33.0 40.990 C0006E-23X-3, 67-68.5 WR 157.32 77 1,201 257 59 3,309 40,999 16,292 1,506 42.7 22.9 19.4 -2.3 0.0 85.0 53.3 26.9 22.9 0.0 100 C0006E-23X-3, 67-68.5 WR 157.32 77 1,201 257 59 3,309 40,999 16,292 1,506 42.7 22.9 19.4 -2.3 0.0 85.0 53.3 26.9 22.9 0.0 100 C0006E-23X-4, 0-1.5 WR 157.32 77 1,201 257 59 3,309 40,999 16,292 1,506 42.7 22.9 19.4 -2.3 0.0 85.0 53.3 26.9 22.9 0.0 100 C0006E-23X-4, 0-1.5 WR 157.32 77 1,461 246 69 2,680 43,997 22.71 2,357 44.4 19.3 17.0 -1.2 0.0 88.7 55.0 2.40 21.0 0.0 100 C0006E-23X-4, 0-1.5 WR 157.92 67 1,465 588 69 1,884 14,347 2,357 44.4 19.3 17.0 -1.2 0.0 88.3 50.8 23.7 25.6 0.0 100 C0006E-23X-6, 02-91.5 WR 180.12 71 1,335 501 81 2,775 18,507 2,732 44.8 209 22.6 -0.7 0.0 105.1 37.2 25.0 3.78 0.0 100 C0006E-25X-6, 52-56.5 WR 180.12 71 1,335 501 81 2,775 18,507 2,732 44.8 209 22.6 -0.7 0.0 105.4 43.2 23.0 33.8 0.0 100 C0006E-25X-6, 02-35.5 WR 180.12 71 1,335 501 81 2,775 18,507 2,732 44.8 209 22.6 -0.0 107.2 35.4 29.6 35.1 0.0 100 C0006E-25X-6, 02-3 10.8 11,275 58 1,261 463 28 1,989 44,29 32.105 1,673 41.0 24.4 41.3 -1.8 0.0 106.8 38.4 22.9 33.8 0.0 100 C0006E-25X-6, 02-118.5-120 W 183.01 73 1,009 211 79 3,651 37,61 15,655 2,531 45.9 2.05 1.7. 0 0.90, 48.3 20, 20.4 0.0 100 C0006E-25X-4, 0-1.5 WR 183.81 64 1,262 309 62 2,314 4,59 2,518 4.1.7 17.8 1.0 0 106.8 38.4 22.9 3.7 0.0 100 C0006E-25X-4, 0-1.5 WR 183.81 64 1,262 37.7 57 1,2276 32,253 14,55 2,558 4.7.1 10.9 10.8 1.3.5 92.8 3.7 2.0 3.0 100 C0006E-25X-4, 0-1.5 WR 193.82 49 1,292 406 75 1,374 379 37.7 12,377 44.1 21.2 24.0 -1.5 0.0		C0006E-22X-4 115-116 5	W/R	148 33	61	1 534	473	51	2 1 8 3	46 008	34 087	1 461	44 3	25.2	43.9	_2 4	0.0	113 5	39.0	22.2	38.7	0.0	100
C0006E-22X, 6 6-67.5 WR 150.66 56 1,729 581 52 1,287 56,793 38,29 1,678 38.0 31.5 49.5 1,9 0.0 119.1 31.9 26.5 31.0 100 C0006E-23X, 1, 65-66.5 WR 154.48 58 1,043 226 90 3,453 37,956 16,166 3,154 44.3 21.1 19.4 -0.2 0.0 84.7 52.3 24.6 3.00 100 C0006E-23X, 1, 10-102.5 WR 154.4 58 1,246 46,027 2,69 14.4 28.1 14.2 2.5 30.0 100		C0006E-22X-6 20-21 5	W/R	150.20	58	1,551	409	76	2,103	48 797	27 773	2 3 5 8	39.7	27.2	35.1	_1 1	0.0	102.0	38.9	26.6	34.4	0.0	100
C0006E-23X.1, 65-66.5 WR 154.84 77 1,510 413 71 2,69 46,027 26,194 2,185 41.4 25.5 3.0 -1.3 0.0 10.00 41.4 25.6 3.0 0.0 100 C0006E-23X.3, 67-68.5 WR 156.91 58 1,544 98 88 2,021 51,086 9,9205 2,461 46.2 28.0 50.7 -1.3 0.0 120.0 41.4 25.6 3.0 0.0 100 C0006E-23X.3, 67-68.5 WR 157.3 77 1,201 257 59 3,309 40,959 16,292 1,506 42.7 22.9 19.4 -2.3 0.0 85.0 50.3 26.9 22.9 0.0 100 C0006E-23X.5, 90-91.5 WR 157.7 67 1,036 221 69 3,583 34,894 14,347 2,357 44.4 19.3 17.0 -1.2 0.0 85.0 50.3 26.9 22.9 0.0 100 C0006E-23X.5, 90-91.5 WR 158.7 467 1,036 221 69 3,583 34,894 14,347 2,357 44.4 19.3 17.0 -1.2 0.0 85.0 50.3 26.9 22.9 0.0 100 C0006E-23X.5, 90-91.5 WR 158.7 1,461 284 69 2,680 43,997 22,721 2,369 41.1 42.5 28.3 -1.1 0.0 93.8 43.8 26.1 30.1 0.0 100 C0006E-23X.5, 90-91.5 WR 158.92 67 1,465 508 69 1,884 47,413 31,056 2,491 39.1 26.2 39.8 -0.7 0.0 105.1 37.2 25.0 37.8 0.0 100 C0006E-23X.5, 90-91.5 WR 180.12 71 1,336 501 81 2,765 44,397 28,369 2,093 46.0 24.4 36.0 -1.7 0.0 106.4 43.2 23.0 33.8 0.0 100 C0006E-25X.7, 0-1.5 WR 180.12 71 1,336 501 81 2,765 44,397 28,369 2,093 46.0 24.4 36.0 -1.7 0.0 106.4 43.2 23.0 33.8 0.0 100 C0006E-25X.7, 0-1.5 WR 180.12 71 1,336 501 81 2,765 44,397 28,369 2,093 46.0 24.4 36.0 -1.7 0.0 106.4 43.2 23.0 33.8 0.0 100 C0006E-25X.7, 0-1.5 WR 180.19 51 1,852 408 60 1,903 56,573 29,789 1,263 37.9 31.7 37.6 -2.6 0.0 107.2 35.4 29.6 35.1 0.0 100 C0006E-25X.14.5-149 WR 183.81 64 1,262 109 64 2,912 39,421 1,342 1,824 1,827 45.6 2.17 0.0 09.9 46.8 24.0 29.2 0.0 100 C0006E-25X.4 14.5-149 WR 183.81 64 1,262 109 64 7.9 12,327 32,76 32.5 14.5 9.20.5 18.6 -1.7 0.0 106.8 38.4 22.9 38.7 0.0 100 C0006E-25X.4 14.5-120 W 185.01 73 1009 1211 79 3,61 13,65 1,539 41.0 24.4 41.3 -1.8 0.0 106.8 38.4 22.9 38.7 0.0 100 C0006E-25X.4 14.5-120 W 185.01 73 1,099 121 79 3,61 13,65 1,539 24.0 29.2 14. 21.9 0.0 100 C0006E-27X.7, 118-120 W 185.01 73 1,099 24.7 63 1,264 32.9 1,374 35.0 2.6 43.2 -1.5 0.0 18.8 35.8 24.5 39.7 0.0 100 C0006E-27X.5, 16.5-18 WR 19.5.7 66 1,092 426 7 1,829 3,551 1,936 42.0 2.0 5.3 3.6 -1.6		C0006E-22X-6 66-67 5	W/R	150.20	56	1 729	581	52	1 287	56 793	38 329	1 678	38.0	31.5	49.5	_1.1	0.0	1191	31.9	26.5	41.6	0.0	100
C00006223X-1, 101-102.5 WR 134.4 77 1,510 143 77 2,649 4,6027 26,194 414 21.5 3.0 -1.3 0.0 100.0 142 2.6.3 0.0 100.0 C00006223X-3, 26-27.5 WR 156.91 58 1,544 59 3,09 40,993 16,292 2,461 46.2 28.0 50.7 -1.3 0.0 100.0 41.4 2.5.6 3.0 -1.3 0.0 100.0 85.0 32.0 2.2.4 40.6 0.0 100 C00066-23X-4, 0-1.5 WR 157.74 67 1,036 221 69 3,583 34,894 14,347 2,357 44.4 19.3 17.0 -1.2 0.0 80.7 55.0 24.0 10.0 100 C00066-23X-5,90-91.5 WR 158.98 57 1,461 284 69 2,649 3,17 2.6.0 3.7.2 2.5.0 3.8.0 100 100 100 105.1 37.7 2.6.0 3.7.2 2.6.0 3.8.1 8.0 10.0 100 100		C0006E-23X-1 65-66 5	W/R	154.00	58	1 043	226	90	3 4 5 3	37 956	16 166	3 1 5 4	44 3	21.1	19.4	_0.2	0.0	84.7	52.3	20.5	22.8	0.0	100
C0006E-23X-3, 26-27.5 WR 156.9 YR 156.9 YR 157.2 77 1,201 257 59 3,309 40,959 16,292 1,506 42.7 22.9 19.4 -2.3 0.0 85.0 50.3 7.0 22.4 40.6 0.0 100 C0006E-23X-4, 0-1.5 WR 157.24 77 1,036 221 69 3,583 34,894 14,347 2,357 44.4 19.3 17.0 -1.2 0.0 85.0 50.3 24.9 22.9 0.0 100 C0006E-23X-5, 90-91.5 WR 158.98 57 1,461 284 69 2,680 43,997 22,721 2,369 41.1 24.5 28.3 -1.1 0.0 93.8 43.8 24.0 13.0 10 0 C0006E-25X-6, 0-0 105.1 37.2 27.8 10.0 0 100 C0006E-25X-6, 0-0 105.1 37.2 27.0 3.8 0.0 100 C0006E-25X-6, 0-0 105.1 37.2 27.0 3.8 0.0 100 C0006E-25X-6, 0-0 105.1 37.2 25.0 37.8 0.0 100 C0006E-25X-6, 0-0 105.1 37.2 25.0 37.8 0.0 100 C0006E-25X-6, 0-0 105.1 37.2 25.0 37.8 0.0 100 C0006E-25X-6, 0-0 107.2 35.4 29.6 35.1 0.0 100 C0006E-25X-7, 0-1.5 WR 180.12 71 1,336 501 81 2,765 44.397 28,369 2,093 46.0 24.4 36.0 -1.7 0.0 106.4 43.2 23.0 3.8 0.0 100 C0006E-26X-7, 147.5-149 WR 183.81 64 1,262 309 64 2,912 39,421 21,342 1,897 42.6 21.8 26.5 -1.1 0.0 9.9 46.8 24.0 29.2 0.0 100 C0006E-26X-2, 118.5-120 W 184.90 58 1,261 463 28 1,989 44.49 32,105 1,673 41.0 24.4 41.3 -1.8 0.0 106.8 38.4 22.9 38.7 0.0 100 C0006E-26X-2, 118.5-120 W 185.01 73 1,009 211 79 3,671 32,510 2,518 47.7 17.8 17.7 -0.5 0.0 7.3 54.0 23.0 23.0 0.0 100 C0006E-26X-4, 0-1.5 WR 191.82 49 1,292 406 75 1,824 40,751 25,710 2,745 35.0 22.6 32.8 0.0 0.0 90.4 38.7 25.0 3.0. 1100 C0006E-27X-3, 113-5-120 WR 185.01 73 1,009 211 79 3,871 32,710 2,745 35.0 24.6 31.8 -1.1 0.0 85.1 33.9 24.1 21.9 0.0 100 C0006E-26X-4, 0-1.5 WR 191.82 49 1,292 406 75 1,824 40,751 25,710 2,745 35.0 24.6 31.8 -1.1 0.0 85.1 33.9 24.1 21.9 0.0 100 C0006E-27X-3, 113-115 W 195.79 66 1,902 286 71 3,589 38,491 19,598 2,337 48.1 21.2 24.0 -1.5 0.0 108.8 35.8 24.5 39.7 0.0 100 C0006E-27X-3, 113-115 W 195.79 66 1,902 286 71 3,589 38,491 19,598 2,337 48.1 21.2 24.0 -1.5 0.0 193.3 51.5 2.8 35.7 0.0 100 C0006E-27X-		$C0006E_{23}X_{-1}$ 101_102 5	W/R	154.40	77	1,045	413	71	2 4 6 9	46 027	26 194	2 185	41.5	25.5	33.0	_1 3	0.0	100.0	41 4	25.6	33.0	0.0	100
C0006E-23X-3, 67-68.5 WR 157.32 77 1,271 257 9 3,309 40,999 16,292 1,501 42.7 2,29 19.4 -2.3 0.0 85.0 50.3 24.7 9.0 100 C0006E-23X-3, 67-68.5 WR 157.74 67 1,036 221 69 3,509 40,999 16,292 1,506 42.7 2,29 19.4 -2.3 0.0 85.0 50.3 24.0 21.0 0.0 100 C0006E-23X-3, 09-1,5 WR 158.98 57 1,461 284 69 2,680 43,997 22,721 2,357 44.4 19.3 17.0 -1.2 0.0 85.0 50.3 24.0 21.0 0.0 100 C0006E-25X-4, 124-125 W 178.29 67 1,465 508 69 1,884 47,413 31,056 2,491 39.1 26.2 39.8 -0.7 0.0 105.1 37.2 25.0 37.8 0.0 100 C0006E-25X-5, 82-83 W 179.28 64 1,125 288 91 3,337 37,775 18,507 2,732 44.8 20.9 22.6 -0.7 0.0 105.1 37.2 25.0 37.8 0.0 100 C0006E-25X-5, 62-26.5 WR 180.17 1 1,36 501 81 2,765 44.397 28,369 2,093 46.0 24.4 3.6 -1.7 0.0 106.4 43.2 23.0 33.8 0.0 100 C0006E-25X-7, 0-1.5 WR 180.79 51 1,852 408 60 1,903 56,573 29,789 1,263 37.9 31.7 37.6 -2.6 0.0 107.2 35.4 29.6 35.1 0.0 100 C0006E-26X-1, 147.5-149 WR 183.81 64 1,262 309 64 2,912 39,421 21,342 1,897 42.6 21.8 26.5 -1.7 0.0 90.6 8.8 42.0 29.2 0.0 100 C0006E-26X-2, 08-109.5 W 184.90 58 1,261 463 28 1,989 44.29 32,105 1,673 41.0 24.4 41.3 -1.8 0.0 106.8 38.4 22.0 23.0 100 C0006E-26X-2, 08-109.5 W 184.09 58 1,261 463 28 1,989 44.29 32,105 1,673 41.0 24.4 41.3 -1.8 0.0 106.8 38.4 22.0 38.0 0 100 C0006E-26X-2, 08-109.5 W 184.09 58 1,261 463 27.6 32,253 14,755 2,658 41.7 17.8 17.7 -0.5 0.0 77.3 43.6 23.0 30.0 100 C0006E-26X-4, 0-1.5 WR 186.65 95 989 208 72 3,2263 14,751 2,710 2,745 30.2 32.8 0.0 0.9 90.4 38.7 23.0 30.1 100 C0006E-27X-3, 113-115 W 195.79 66 1,092 246 71 3,828 39,753 19,367 2,983 44.3 22.0 23.7 -0.4 0.0 90.0 43.2 23.0 30.1 100 C0006E-27X-3, 113-115 W 195.79 66 1,092 246 71 3,828 39,753 19,367 2,983 44.3 22.0 23.7 -0.4 0.0 90.0 43.2 24.5 26.3 0.0 100 C0006E-27X-3, 113-115 W 195.79 66 1,092 246 71 3,828 39,753 19,367 2,983 44.3 22.0 23.7 -0.4 0.0 90.0 43.2 24.5 26.3 0.0 100 C0006E-27X-1,18-120 W 200.10 44 1,406 483 49 1,691 48,215 33,551 1,909 39.0 26.6 43.2 -1.5 0.0 18.8 35.8 24.5 39.7 0.0 100 C0006E-27X-1,18-5-18 WR 196.75 53 1,494 425 7,168 49,804 2,849		C0006E-23X-3 26-27 5	W/R	156.91	58	1,510	598	88	2,402	51 086	39 205	2,105	46.2	28.0	50.7	_1.3	0.0	125.0	37.0	22.0	40.6	0.0	100
C0006E-23X-4, 0-1.5 WR 157.74 67 1,036 221 69 3,58 34,894 14,347 2,357 44.4 19.3 17.0 -1.2 0.0 80.7 55.0 24.0 21.0 0.0 100 C0006E-23X-5, 90-91.5 WR 158.98 57 1,461 284 69 2,680 43,997 22,721 2,369 41.1 24.5 28.3 -1.1 0.0 93.8 43.8 26.1 30.1 0.0 100 C0006E-23X-4, 124-125 W 178.29 67 1,465 508 69 1,884 47,413 31,056 2,491 39.1 26.2 39.8 -0.7 0.0 105.1 37.2 25.0 37.8 0.0 100 C0006E-23X-5, 82-83 W 179.28 64 1,125 258 91 3,337 37,775 18,507 2,732 44.8 209 22.6 -0.7 0.0 105.1 37.2 23.0 37.8 0.0 100 C0006E-25X-6, 25-26.5 WR 180.12 71 1,336 501 81 2,765 44,397 28,369 2,093 46.0 24.4 36.0 -1.7 0.0 106.4 43.2 23.0 33.8 0.0 100 C0006E-25X-7, 0-1.5 WR 180.79 51 1,852 408 60 42,912 39,421 21,342 1,897 42.6 21.8 26.5 -1.7 0.0 106.4 43.2 23.0 33.8 0.0 100 C0006E-26X-1, 147.5-149 WR 183.81 64 1,262 309 64 2,912 39,421 21,342 1,897 42.6 21.8 26.5 -1.7 0.0 106.8 38.4 22.9 38.7 0.0 100 C0006E-26X-2, 108-109.5 W 184.90 58 1,261 463 28 1,989 44,29 32,105 1,673 41.0 24.4 41.3 -1.8 0.0 106.8 38.4 22.9 38.7 0.0 100 C0006E-26X-4, 0-1.5 WR 186.05 95 989 208 72 3,276 3,2253 14,755 2,658 41.7 1.78 17.7 -0.5 0.0 7.73 54.0 23.0 23.0 0.0 100 C0006E-26X-4, 0-1.5 WR 186.5 95 989 208 72 3,276 3,2253 14,755 2,658 41.7 1.78 17.7 -0.5 0.0 90.4 43.7 25.0 36.3 0.1 100 C0006E-26X-4, 0-1.5 WR 191.82 49 1,292 406 75 1,824 40,751 25,710 2,745 35.0 2.6 32.8 0.0 0.0 90.4 38.7 25.0 36.3 0.1 100 C0006E-27X-1, 60-61.5 WR 191.82 49 1,292 406 75 1,824 40,751 25,710 2,745 35.0 2.6 32.8 0.0 0.0 90.4 38.7 25.0 36.3 0.1 100 C0006E-27X-1, 60-61.5 WR 191.82 49 1,292 406 75 1,824 40,751 25,710 2,745 35.0 2.6 32.8 0.0 0.0 90.4 38.7 25.0 36.3 0.1 100 C0006E-27X-1, 60-61.5 WR 191.82 49 1,292 406 75 1,824 40,751 25,710 2,745 35.0 2.6 32.8 0.0 0.0 90.4 38.7 25.0 36.3 0.1 100 C0006E-27X-1,16-1.5 WR 191.82 49 1,292 406 75 1,824 40,751 25,710 2,745 35.0 2.6 32.8 0.0 0.0 90.4 38.7 25.0 36.3 0.1 100 C0006E-27X-1,16-1.5 WR 191.62 53 1,498 422 57 1,898 49.48,499 1,715 35.1 27.8 36.1 -1.6 0.0 99.0 35.5 28.1 36.5 0.0 100 C0006E-27X-1,18120 W 20.01 4 4 1,406 483 4		C0006E-23X-3 67-68 5	W/R	157 32	77	1 201	257	59	3 309	40 959	16 292	1 506	42.7	22.0	19.4	-2.3	0.0	85.0	50.3	26.9	22.9	0.0	100
C0006E-23X-5, 90-91.5 WR 158.74 67 1,461 284 69 2,680 43,997 22,721 2,369 41.1 24.5 28.8 -1.1 0.0 93.8 42.1 0 21.0 0.0 100 C0006E-25X-4, 124-125 W 178.29 67 1,465 508 69 1,884 47,413 31,056 2,491 39.1 26.2 39.8 -0.7 0.0 105.1 37.2 25.0 37.8 0.0 100 C0006E-25X-5, 82-83 W 179.28 64 1,125 258 91 3,37 37,775 18,507 2,732 44.8 20.9 2.6 -0.7 0.0 18.3 50.8 21.7 25.0 3.8 0.0 100 C0006E-25X-7, 0-1.5 WR 180.79 51 1,852 408 60 1,903 56,573 29,789 1,263 37.9 31.7 37.6 -2.6 0.0 107.2 35.4 29.6 35.1 0.0 100 C0006E-26X-2, 108-109.5 WR 183.81 64 1,262 309 64 2,912 39,421 21,342 1,897 42.6 21.8 26.5 -1.7 0.0 90.9 46.8 24.0 29.2 0.0 100 C0006E-26X-2, 108-109.5 W 184.90 58 1,261 463 28 1,989 44,429 32,105 1,673 41.0 24.4 41.3 -1.8 0.0 106.8 38.4 22.9 38.7 0.0 100 C0006E-26X-2, 108-109.5 W 184.90 58 1,261 463 28 1,989 44,429 32,105 1,673 41.0 24.4 41.3 -1.8 0.0 106.8 38.4 22.9 38.7 0.0 100 C0006E-26X-2, 108-109.5 W 184.90 58 1,261 463 28 1,989 44,429 32,105 1,673 41.0 24.4 41.3 -1.8 0.0 106.8 38.4 22.9 38.7 0.0 100 C0006E-26X-2, 108-109.5 WR 186.65 95 989 208 72 3,276 32,253 14,755 2,658 41.7 17.8 17.7 -0.5 0.0 7.7.3 54.0 23.0 23.0 0.0 100 C0006E-26X-4, 0-1.5 WR 191.82 49 1,292 406 75 1,824 40,751 25,710 2,745 35.0 22.6 32.8 0.0 0.0 90.4 38.7 25.0 36.3 0.1 100 C0006E-27X-5, 16.5-18 WR 191.62 49 1,292 406 71 3,589 38,491 19,598 2,337 48.1 21.2 24.0 -1.5 0.0 93.3 51.5 22.8 25.7 0.0 100 C0006E-27X-5, 16.5-18 WR 197.65 53 1,498 422 57 1 3,589 38,491 19,598 2,337 48.1 21.2 24.0 -1.5 0.0 108.3 35.8 24.5 39.7 0.0 100 C0006E-27X-5, 16.5-18 WR 197.65 53 1,498 422 57 10,89 49,804 28,409 1,715 35.1 27.8 36.1 -1.6 0.0 99.0 35.5 28.1 36.5 0.0 100 C0006E-27X-5, 16.5-18 WR 197.65 53 1,498 422 57 10,89 49,804 28,409 1,715 35.1 27.8 36.1 -1.6 0.0 99.0 35.5 28.1 36.5 0.0 100 C0006E-27X-5, 16.5-18 WR 200.62 56 1,077 266 70 3,112 37,161 18,919 2,787 42.9 20.5 23.3 -0.5 0.0 86.7 49.5 23.7 26.8 0.0 100 C0006E-28X-1,75-77 W 202.08 88 1,683 411 59 1,687 37.7 2,199 49,846 28,409 1,715 35.1 27.8 36.1 -1.6 0.0 98.3 35.8 24.5 39.7 0.0 100 C00		C0006E-23X-4 0-1 5	W/R	157.52	67	1 036	221	69	3,502	34 894	14 347	2 3 5 7	44 4	19.3	17.4	_1 2	0.0	80.7	55.0	20.7	21.0	0.0	100
IIC C0006E-25X-4, 124-125 W 178.29 67 1/465 58 69 1,884 47,413 31,056 2,491 39.1 1.0 20.0 10.1 37.2 20.0 37.8 0.0 100 C0006E-25X-5, 82-83 W 179.28 64 1,125 258 91 3,33 37,775 18,507 2,732 44.8 20.9 2.6 -0.7 0.0 105.1 31.2 3.8 0.0 100 C0006E-25X-7, 0-1.5 WR 180.12 71 1,336 501 81 2,765 44,397 28,369 2,093 46.0 2.4.4 36.0 -1.7 0.0 106.4 43.2 23.0 33.8 0.0 100 C0006E-26X-7, 0-1.5 WR 183.81 64 1,262 309 64 2,912 39,421 21,342 1,897 42.6 21.8 2.65 -1.7 0.0 106.8 38.4 2.9 38.7 0.0 100 C0006E-26X-2, 108-109.5 W 185.01 73 1,099 211 79 3,61		C0006E-23X-5 90-91 5	W/R	158.98	57	1 461	284	69	2 680	43 997	22 721	2,357	41.1	24.5	28.3	_1.1	0.0	93.8	43.8	26.1	30.1	0.0	100
C0006E-25X-5, 82-83 W 179.28 64 1,125 238 91 3,337 37,775 18,507 2,732 44.8 20.9 22.6 -0.7 0.0 88.3 50.8 23.7 25.6 0.0 100 C0006E-25X-5, 82-86.5 WR 180.12 71 1,336 501 81 2,765 44,397 28,369 2,093 46.0 24.4 36.0 -1.7 0.0 106.4 43.2 23.0 33.8 0.0 100 C0006E-25X-7, 0-1.5 WR 180.79 51 1,852 408 60 1,903 56,573 29,789 1,263 37.9 31.7 37.6 2.6 0.0 100.7.2 35.4 2.0 23.7 2.0 100 C0006E-26X-2, 108-109.5 W 183.01 73 1,009 211 79 3.651 37.061 15,656 2,531 45.9 1.8 0.1 100 85.1 53.9 24.1 21.9 0.0 100 C0006E-26X-4, 0-1.5 WR 186.65 95 989 208 72	IIC	C0006E-25X-4 124-125	W	178 29	67	1 465	508	69	1 884	47 41 3	31 056	2,307	39.1	26.2	39.8	-0.7	0.0	105.1	37.2	25.0	37.8	0.0	100
C0006E-25X-6, 25-26.5 WR 180.12 71 1,33 501 81 2,765 44,397 28,369 2,092 46.0 24.4 36.0 100 106.4 32.2 23.0 33.8 0.0 100 C0006E-25X-7, 0-1.5 WR 180.12 71 1,336 64 1,262 39,421 21,342 1,897 42.6 21.8 26.5 -1.7 0.0 90.9 46.8 24.0 29.2 0.0 100 C0006E-26X-1, 147,5-149 WR 183.81 64 1,262 30 64 2,912 39,421 21,342 1,897 42.6 21.8 26.5 -1.7 0.0 90.9 46.8 24.0 29.2 0.0 100 C0006E-26X-2, 108-109.5 W 185.01 73 1,009 21.1 79 3,651 37,061 15,656 2,531 45.9 20.5 18.6 -1.1 0.0 85.1 23.0 23.0 23.0 23.0 23.0 23.0 23.0 23.0 23.0 23.0 23.0 23.0 23.0 23.0	iic	C0006E-25X-5 82-83	Ŵ	179.28	64	1 1 2 5	258	91	3 3 3 7	37 775	18 507	2 732	44.8	20.2	22.6	_0.7	0.0	88.3	50.8	23.0	25.6	0.0	100
C0006E-25X-6, D-15 WR 180.72 71 1,503 17,503 <td></td> <td>C0006E-25X-6 25-26 5</td> <td>\//R</td> <td>180 12</td> <td>71</td> <td>1 336</td> <td>501</td> <td>81</td> <td>2 765</td> <td>44 397</td> <td>28 369</td> <td>2,093</td> <td>46.0</td> <td>20.2</td> <td>36.0</td> <td>_1 7</td> <td>0.0</td> <td>106.4</td> <td>43.2</td> <td>23.0</td> <td>33.8</td> <td>0.0</td> <td>100</td>		C0006E-25X-6 25-26 5	\//R	180 12	71	1 336	501	81	2 765	44 397	28 369	2,093	46.0	20.2	36.0	_1 7	0.0	106.4	43.2	23.0	33.8	0.0	100
C0006E-26X-1, 147.5-149 VR 183.81 64 1,262 309 64 2,912 39,421 21,342 12,342 1,897 42.6 21.8 26.5 -1.7 0.0 90.9 46.8 24.0 29.2 0.0 100 C0006E-26X-2, 108-109.5 W 184.90 58 1,261 463 28 1,989 44,429 32,105 1,673 41.0 24.4 41.3 -1.8 0.0 106.8 38.4 22.9 38.7 0.0 100 C0006E-26X-2, 118.5-120 W 185.01 73 1,009 211 79 3,651 37,061 15,656 2,531 45.9 20.5 18.6 -1.1 0.0 85.1 53.9 24.1 21.9 0.0 100 C0006E-26X-4, 0-1.5 WR 186.65 95 989 208 72 3,276 32,253 14,755 2,658 41.7 17.8 17.7 -0.5 0.0 77.3 54.0 23.0 23.0 0.0 100 C0006E-26X-8, 94.5-96 WR 191.82 49 1,292 406 75 1,824 40,751 25,710 2,745 35.0 22.6 32.8 0.0 90.4 38.7 25.0 36.3 0.1 100 C0006E-27X-1, 60-61.5 WR 192.43 62 1,168 370 89 3,228 39,753 19,367 2,983 44.3 22.0 23.7 -0.4 0.0 90.0 49.2 24.5 26.3 0.0 100 C0006E-27X-5, 16.5-18 WR 197.65 53 1,498 422 57 1,689 49,804 28,409 1,715 35.1 27.8 36.1 -1.6 0.0 99.0 35.5 28.1 36.5 0.0 100 C0006E-27X-7, 118-120 W 200.10 44 1,406 483 49 1,691 48,215 33,551 1,909 39.0 26.6 43.2 -1.5 0.0 108.8 35.8 24.5 39.7 0.0 100 C0006E-27X-8, 30-31.5 WR 200.62 56 1,902 427 60 1,628 57.712 32,797 2,024 37.3 32.3 41.8 -1.5 0.0 101.8 35.8 24.5 39.7 0.0 100 C0006E-27X-8, 30-31.5 WR 200.62 56 1,072 260 7 3,112 37,161 18,919 2,787 42.9 20.5 23.3 -0.5 0.0 86.7 49.5 23.7 26.8 0.0 100 C0006E-28X-1, 75-77 W 202.08 88 1,683 411 59 1,877 50,779 32,349 1,832 39.8 28.2 41.4 -1.7 0.0 109.4 35.5 28.7 26.8 0.0 100 C0006E-28X-1, 75-77 W 202.08 88 1,683 411 59 1,877 50,779 32,349 1,832 39.8 27.8 35.3 -1.7 0.0 109.4 36.4 25.8 37.9 0.0 100 C0006E-28X-1, 75-77 W 202.08 88 1,683 411 59 1,877 50,779 32,349 1,832 39.8 27.8 35.3 -1.7 0.0 109.4 36.4 25.8 37.9 0.0 100 C0006E-28X-1, 91-92.5 WR 201.64 65 1,077 267 3,182 36,064 16,314 2,262 48.7 19.9 19.5 -1.6 0.0 88.1 55.3 22.6 22.2 0.0 100 C0006E-28X-1, 91-92.5 WR 201.64 65 1,077 26.7 3,182 36,064 16,314 2,262 48.7 19.9 19.5 -1.6 0.0 88.1 55.3 22.6 22.2 0.0 100 C0006E-28X-1, 91-92.5 WR 203.71 70 1,076 243 76 3,882 36,064 16,314 2,262 48.7 19.9 19.5 -1.6 0.0 88.1 55.3 22.6 22.2 0.0 100 C0006E-28X-3, 0-1.5 WR		C0006E-25X-7 0-1 5	W/R	180.72	51	1,550	408	60	1 903	56 573	20,302	1 263	37.9	31.7	37.6	_2.6	0.0	107.2	35.4	29.6	35.0	0.0	100
C0006E-26X-2, 108-1095 W 185.01 73 1,201 463 28 1,912		$C0006E_{25}(-7), 0 = 1.5$	W/R	183.81	64	1 262	309	64	2 912	39 4 21	21 342	1 897	42.6	21.8	26.5	_1 7	0.0	90.9	46.8	22.0	29.2	0.0	100
C0006E-26X-2, 118.5-120 W 185.01 73 1,009 211 79 3,651 37,061 15,656 2,531 45.9 20.5 18.6 -1.1 0.0 85.1 53.9 24.1 21.9 0.0 100 C0006E-26X-2, 118.5-120 WR 185.01 73 1,009 211 79 3,651 37,061 15,656 2,531 45.9 20.5 18.6 -1.1 0.0 85.1 53.9 24.1 21.9 0.0 100 C0006E-26X-4, 0-1.5 WR 191.82 49 1,292 406 75 1,824 40,751 25,710 2,745 35.0 22.6 32.8 0.0 0.0 90.4 38.7 25.0 36.3 0.1 100 C0006E-27X-1, 60-61.5 WR 192.43 62 1,168 370 89 3,228 39,753 19,367 2,983 44.1 21.2 24.0 -1.5 0.0 93.3 51.5 22.8 25.7 0.0 100 C0006E-27X-5, 165-18 WR 197.55 53 1,494		C0006E-26X-2 108-109 5	W/	184 90	58	1 261	463	28	1 989	44 4 29	32 105	1,673	41.0	24.4	<u>41</u> 3	_1.7	0.0	106.8	38.4	27.9	38.7	0.0	100
C0006E-26X-4, 0-1.5 WR 186.65 95 989 208 72 3,276 32,253 14,755 2,658 41.7 7.8 17.7 -0.5 0.0 73. 54.0 23.0 23.0 23.0 0.0 100 C0006E-26X-8, 94.5-96 WR 191.82 49 1,292 406 75 1,824 40,751 25,710 2,745 35.0 23.0 0.0 100 00 90.4 38.7 25.0 36.3 0.1 100 C0006E-26X-8, 94.5-96 WR 192.43 62 1,168 370 89 3,228 39,753 19,367 2,983 44.3 22.0 23.7 -0.4 0.0 90.0 49.2 24.5 26.3 0.0 100 C0006E-27X-3, 113-115 W 195.79 66 1,092 286 71 3,589 38,491 19,598 2,337 48.1 21.2 24.0 -1.5 0.0 93.3 51.5 22.8 25.7 0.0 100 C0006E-27X-5, 16.5-18 WR 197.65 53 1,498		$C0006E_{26X-2}, 100-107.5$	Ŵ	185.01	73	1 009	211	79	3 651	37 061	15 656	2 5 3 1	45.9	20.5	18.6	_1.0	0.0	85.1	53.9	24.7	21.9	0.0	100
C0006E-26X-8, 94.5-96 WR 191.82 49 1,292 406 75 1,824 40,751 25,710 2,745 35.0 22.6 32.8 0.0 90.4 38.7 25.0 36.3 0.1 100 C0006E-26X-8, 94.5-96 WR 191.82 49 1,292 406 75 1,824 40,751 25,710 2,745 35.0 22.6 32.8 0.0 90.4 38.7 25.0 36.3 0.1 100 C0006E-27X-1, 60-61.5 WR 192.43 62 1,168 370 89 3,228 39,753 19,367 2,983 44.3 20.0 2.7 -0.4 0.0 90.0 49.2 24.5 26.3 0.0 100 C0006E-27X-3, 113-115 W 195.79 66 1,092 286 71 3,589 38,491 19,598 2,337 48.1 21.2 24.0 -1.5 0.0 93.3 51.5 22.8 25.7 0.0 100 C0006E-27X-5, 16.5-18 WR 197.65 53 1,498 422 57 1,68		C0006E-26X-4 0-1 5	\//R	186.65	95	989	208	72	3 276	32 253	14 755	2,551	41 7	17.8	17.7	_0.5	0.0	77 3	54.0	23.0	23.0	0.0	100
C0006E-27X-1, 60-61.5 WR 192.43 62 1,168 370 89 3,228 39,753 19,867 2,983 44.3 22.0 23.7 -0.4 0.0 90.0 492 24.5 26.3 0.0 100 C0006E-27X-3,113-115 W 192.75 53 1,498 422 57 1,689 49,804 28,409 1,715 35.1 27.8 36.1 -1.6 0.0 99.0 35.5 28.8 39.7 0.0 100 C0006E-27X-5, 16.5-18 WR 197.65 53 1,498 422 57 1,689 49,804 28,409 1,715 35.1 27.8 36.1 -1.6 0.0 99.0 35.5 28.1 36.5 0.0 100 C0006E-27X-7, 118-120 W 200.10 44 1,406 483 49 1,691 48,215 33,551 1,909 39.0 26.6 43.2 -1.5 0.0 111.4 33.5 29.0 37.5 0.0 100 C0006E-27X-8, 30-31.5 WR 201.64 65 1,077 26		C0006E-26X-8 94 5 96	\//P	100.05	10	1 202	406	75	1 8 2 4	10 751	25 710	2,050	35.0	22.6	32.8	0.0	0.0	90 A	38.7	25.0	36.3	0.0	100
C0006E-27X-3, 113-115 W 192.19 66 1,092 286 71 3,589 38,491 19,598 2,37 48.1 21.2 24.0 -1.5 0.0 93.3 51.5 22.8 25.7 0.0 100 C0006E-27X-3, 113-115 WR 197.65 53 1,498 422 57 1,689 49,804 28,409 1,715 35.1 1.2 24.0 -1.5 0.0 93.3 51.5 22.8 25.7 0.0 100 C0006E-27X-5, 16.5-18 WR 197.65 53 1,498 422 57 1,689 49,804 28,409 1,715 35.1 1.2 2.4.0 -1.5 0.0 93.3 51.5 22.8 25.7 0.0 100 C0006E-27X-7, 118-120 W 200.10 44 1,406 483 49 1,691 48,215 33,551 1,909 39.0 26.6 43.2 -1.5 0.0 111.4 33.5 29.0 37.5 0.0 100 C0006E-28X-1, 31-32.5 WR 201.64 65 1,077 26		$C0006E_{27X-1} 60_{61.5}$	W/R	197.02	62	1 1 6 8	370	89	3 228	39 753	19 367	2,743	44 3	22.0	23.7	_0.4	0.0	90.9	49 2	22.0	26.3	0.1	100
C0006E-27X-5, 165-18 WR 197.65 53 1,498 422 57 1,689 49,804 28,409 1,715 35.1 27.8 36.1 -1.6 0.0 99.0 35.5 28.1 36.5 0.0 100 C0006E-27X-7, 118-120 W 200.10 44 1,406 483 49 1,661 48,215 33,551 1,909 39.0 26.6 43.2 -1.5 0.0 108.8 35.8 24.5 39.7 0.0 100 C0006E-27X-7, 118-120 W 200.10 44 1,406 483 49 1,661 48,215 33,551 1,909 39.0 26.6 43.2 -1.5 0.0 108.8 35.8 24.5 39.7 0.0 100 C0006E-27X-8, 30-31.5 WR 201.64 65 1,077 266 70 3,112 37,161 18,919 2,787 42.9 20.5 23.3 -0.5 0.0 86.7 49.5 23.7 26.8 0.0 100 C0006E-28X-1, 75-77 W 202.08 88 1,682 370		$C0006E_{27}X_{-1}, 00-01.5$	10/	105 70	66	1,100	286	71	3 5 8 9	38 / 01	10 508	2,203	48 1	22.0	24.0	-0.4	0.0	03.3	51.5	27.5	20.5	0.0	100
C0006E-27X-8, 10.3-10 WR 177.05 351 1,405 422 37 1,605 4,705 1,715 30.1 27.0 <t< td=""><td></td><td>$C0006E_{27}X_{-5}, 115_{-115}$</td><td>\\/D</td><td>197.65</td><td>53</td><td>1,072</td><td>200 422</td><td>57</td><td>1 689</td><td>10 801</td><td>28 /09</td><td>1 715</td><td>35 1</td><td>27.8</td><td>24.0</td><td>1.5</td><td>0.0</td><td>00 0</td><td>35.5</td><td>22.0</td><td>25.7</td><td>0.0</td><td>100</td></t<>		$C0006E_{27}X_{-5}, 115_{-115}$	\\/D	197.65	53	1,072	200 422	57	1 689	10 801	28 /09	1 715	35 1	27.8	24.0	1.5	0.0	00 0	35.5	22.0	25.7	0.0	100
C0006E-27X-8, 30-31.5 WR 200.62 56 1,902 427 60 1,628 57,712 32,797 2,024 37.3 32.3 41.8 -1.5 0.0 101.4 33.5 29.0 37.5 0.0 100 C0006E-27X-8, 30-31.5 WR 201.64 65 1,077 266 70 3,112 37,161 18,919 2,787 42.9 20.5 23.3 -0.5 0.0 111.4 33.5 29.0 37.5 0.0 100 C0006E-28X-1, 75-77 W 202.08 88 1,683 411 59 1,877 50,779 32,349 1,832 39.8 28.2 41.4 -1.7 0.0 109.4 36.4 25.8 37.9 0.0 100 C0006E-28X-1, 91-92.5 WR 202.24 59 1,462 370 57 2,199 49,846 27,936 1,876 39.8 27.8 35.3 -1.7 0.0 102.9 38.7 27.0 34.3 0.0 100 C0006E-28X-2, 97-99 W 203.71 70 1,076 2		$C0006E_{27}X_{-7}$ 118 120	10/	200.10	14	1,406	183	رد ۱۵	1,007	18 215	20,402	1 000	30.0	27.0	JU.1	-1.0	0.0	108.8	35.8	20.1	30.5	0.0	100
C0006E-28X-1, 31-32.5 WR 201.64 65 1,07 266 70 3,112 37,161 18,919 2,787 42.9 20.5 23.3 -0.5 0.0 86.7 49.5 23.7 26.8 0.0 100 C0006E-28X-1, 75-77 W 202.08 88 1,683 411 59 1,877 50,779 32,349 1,832 39.8 28.2 41.4 -1.7 0.0 109.4 36.4 25.8 37.9 0.0 100 C0006E-28X-1, 91-92.5 WR 202.24 59 1,462 370 57 2,199 49,846 27,936 1,876 39.8 27.8 35.3 -1.7 0.0 109.4 36.4 25.8 37.9 0.0 100 C0006E-28X-2, 97-99 W 203.71 70 1,076 243 76 3,882 36.04 16,314 2,262 48.7 19.9 19.5 -1.6 0.0 88.1 55.3 22.6 22.2 0.0 100 C0006E-28X-3, 0-1.5 WR 203.81 59 1,730 355 <td></td> <td>$C0006E_{27X-8} = 30 = 31 = 5$</td> <td>\\/D</td> <td>200.10</td> <td>56</td> <td>1 902</td> <td>405</td> <td> 60</td> <td>1,021</td> <td>57 712</td> <td>32 707</td> <td>2 024</td> <td>37.3</td> <td>20.0</td> <td>41.8</td> <td>-1.5</td> <td>0.0</td> <td>111 /</td> <td>33.5</td> <td>29.0</td> <td>37.5</td> <td>0.0</td> <td>100</td>		$C0006E_{27X-8} = 30 = 31 = 5$	\\/D	200.10	56	1 902	405	 60	1,021	57 712	32 707	2 024	37.3	20.0	41.8	-1.5	0.0	111 /	33.5	29.0	37.5	0.0	100
C0006E-28X-1, 75-77 W 202.08 88 1,683 411 59 1,877 50,779 32,349 1,832 39.8 28.2 41.4 -1.7 0.0 109.4 36.4 25.8 37.9 0.0 100 C0006E-28X-1, 91-92.5 WR 202.24 59 1,462 370 57 2,199 49,846 27,936 1,876 39.8 27.8 35.3 -1.7 0.0 109.4 36.4 25.8 37.9 0.0 100 C0006E-28X-1, 91-92.5 WR 202.24 59 1,462 370 57 2,199 49,846 27,936 1,876 39.8 27.8 35.3 -1.7 0.0 102.9 38.7 27.0 34.3 0.0 100 C0006E-28X-2, 97-99 W 203.71 70 1,076 243 76 3,882 36,064 16,314 2,262 48.7 19.9 19.5 -1.6 0.0 88.1 55.3 22.6 22.2 0.0 100 C0006E-28X-3, 0-1.5 WR 203.81 59 1,730 355<		C0006E 28X 1 21 22 5		200.02	65	1,702	727	70	2 112	27 161	18 010	2,024	120	20.5	22.2	-1.5	0.0	86.7	10.5	22.0	26.8	0.0	100
C0006E-28X-1, 9-7/ W 202.06 88 1,93 1,97 50,77 52,549 1,832 59.8 28.2 41.4 -1.7 0.0 109.4 30.4 23.8 57.9 0.0 100 C0006E-28X-1, 91-92.5 WR 202.24 59 1,462 370 57 2,199 49,846 27,936 1,876 39.8 27.8 35.3 -1.7 0.0 102.9 38.7 27.0 34.3 0.0 100 C0006E-28X-2, 97-99 W 203.71 70 1,076 243 76 3,882 36,064 16,314 2,262 48.7 19.9 19.5 -1.6 0.0 88.1 55.3 22.6 22.2 0.0 100 C0006E-28X-3, 0-1.5 WR 203.81 59 1,730 355 47 3,029 51,358 26,402 1,475 46.8 28.6 32.9 -2.9 0.0 108.3 43.2 26.4 30.4 0.0 100 C0006E-28X-4 76 58 1,794 355 71 2,755 53.304		C0006E 28X 1 75 77	10/	201.04	80	1,077	411	50	1 977	50 770	22 2/0	1 9 2 2	20.9	20.5	23.J 11 1	-0.5	0.0	100.7	36.4	25.9	20.0	0.0	100
C0006E-28X-1, 91-92.5 WR 202.24 59 1,076 37 2,199 49,040 27,950 1,076 39.8 27.0 39.7 27.0 39.7 27.0 39.7 27.0 39.7 27.0 39.7 27.0 39.7 27.0 39.7 27.0 39.7 27.0 30.7 27.0 39.7 27.0 30.7 27.0 30.7 27.0 30.7 27.0 30.7 27.0 30.7 27.0 30.7 27.0 30.7 27.0 30.7 27.0 30.7 27.0		C0006E 28X - 1, 73 - 77	۷۷ ۱۸/D	202.00	50	1,005	370	57	2 100	10 816	27 026	1,052	20.8	20.2	25.2	-1.7	0.0	102.4	28.7	27.0	3/.9	0.0	100
C0006E-28X-3, 0-1.5 WR 203.81 59 1,730 355 47 3,029 51,358 26,402 1,475 46.8 28.6 32.9 -2.9 0.0 108.3 43.2 26.4 30.4 0.0 100 C0006E-28X-4 75_76 5 WR 203.81 59 1,730 355 47 3,029 51,358 26,402 1,475 46.8 28.6 32.9 -2.9 0.0 108.3 43.2 26.4 30.4 0.0 100		C0002-207-1, 71-72.3	۷۷K ۱۸/	202.24	57 70	1,402	2/2	76	2,177 2,000	36 061	27,750 16 21 A	7 262	57.0 19.7	27.0 10.0	55.5 10 5	-1./	0.0	102.7 80 1	55.7	27.0 22.6	כ.דיכ ררכ	0.0	100
C0006E-267-3, U=1.3 WR 203.61 37 1,730 333 47 3,027 31,530 20,402 1,473 40.6 26.6 32.7 -2.7 0.0 100.3 43.2 20.4 30.4 0.0 100 C006E-28X.4 75_765 WR 204.92 58 1,794 355 71 2,755 53 304 24,961 1,703 43.0 29 8,309 -2.4 0.0 103 7 41.4 28 2,98 0.0 100		C0006E-28X-2, 97-99		203.71	50	1,070	245	/0	2,002	50,004	26 402	2,202	40.7	19.9	220	-1.0	0.0	00.1 109.2	33.5 42.2	22.0	22.2	0.0	100
		C0002-207-3, 0-1.3		203.01	59 59	1,730	255	4/ 71	3,029 2,755	52 204	20,402	1,4/3	40.0	20.0 20.9	32.9	-2.7	0.0	100.5	43.Z	∠0.4 20.9	20.4	0.0	100
		COUDE-20A-4, / 3-/0.3		204.92 212 11	0 C	1,794	333	7 I 90	2,133	33,304 40 720	24,901 16 001	1,703	43.0	29.0 22.0	20.9	-2.4	0.0	103./ 00.F	41.4	20.0 25.2	27.0 22.5	0.0	100
CUUDUL-277-2, 04.3-50 WK 213.11 04 1,207 230 07 3,004 40,737 10,094 2,003 40.7 22.0 20.2 -1.7 0.0 09.3 32.2 23.3 22.3 0.0 100 CODACE 207 2 117 110 W 213 43 44 1429 505 50 1910 50513 24194 2004 405 77 0 440 140 142 350 240 240 201 00 100		C0004E 20X 2 117 110	VVK	213.11	04 44	1,209	230	07 60	2,004 1 010	40,/39	10,094 21 101	2,003	40.7	22.0	20.2	-1.9	0.0	07.3 112 /	32.Z	23.3 24.0	22.3	0.0	100
$C0000(z_27x_2, 117-117) = VV = 213.453 = 44 + 1,450 = 363 = 60 + 1,610 = 30,312 = 24,164 = 2,074 = 40.5 = 27.7 = 44.0 = -1.4 = 0.0 = 112.4 = 360. = 24.7 = 37.1 = 0.0 = 100 = 0.0 $		COODE-23A-2, 117-119 COODE 208 2 126 129	VV \\/	213.43	44	1,40	260	51	1,010	20 051	16 201	2,094	40.5	27.9	44.0 20.2	-1.4 2.4	0.0	112.4 86.0	50.0	24.9	22.1	0.0	100
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		$C0006E_{29}X_{-2}, 120-120$	\//R	213.52	87	1 218	209	74	3,477	39 4 28	17 905	2 3 5 2	44.9 45 0	21.7	20.3 21.7	-2.4 _1 4	0.0	89.5	51./	23.0 24.4	23.4 24.2	0.0	100

Table T4 (continued). (Continued on next page.)

													,	Abunda	ance ca	lculate	d from S	VD norn	nalizati	on fact	or	
				Peak	intensity	(counts	s/step)	Integra	ated peak	area (tota	l counts)		Calcul	ated ab	undan	ce (wt	%)	Nor	malize	d abun	dance ((wt%)
						se				se				se		q				se		
Unit	Hole, core, section, interval (cm)	Core type	Depth CSF (m)	Clay	Quartz	Plagiocla	Calcite	Clay	Quartz	Plagiocla	Calcite	Clay	Quartz	Plagiocla	Calcite	Correcte calcite	Absolute total	Clay	Quartz	Plagiocla	Calcite	Relative total
	C0006E-30X-1, 10–11	W	220.43	58	1,385	586	51	1,587	44,060	39,704	1,839	42.6	24.0	51.9	-1.6	0.0	118.5	36.0	20.2	43.8	0.0	100
	C0006E-30X-1, 107–108.5	WR	221.40	80	1,175	313	69	3.228	40,554	21,895	1.552	46.0	22.4	27.2	-2.4	0.0	95.6	48.2	23.4	28.4	0.0	100
	C0006E-30X-2, 46-47	W	222.20	89	528	123	200	3,029	17,910	8,619	8,288	35.8	9.7	10.1	7.7	7.7	63.2	56.5	15.3	15.9	12.2	100
	C0006E-30X-3, 0–1.5	WR	223.16	85	1,154	252	78	4,053	37,885	15,384	1,674	49.6	21.0	18.1	-2.5	0.0	88.7	55.9	23.7	20.4	0.0	100
	C0006E-30X-8, 80.5-82	WR	229.63	77	1,157	248	127	, 4,154	37,942	17,113	4,381	52.0	20.9	20.4	0.9	0.9	94.2	55.2	22.2	21.7	0.9	100
	C0006E-31X-1, 122–124	W	231.05	39	1,585	1,311	73	575	45,163	54,444	2,615	43.3	24.1	72.4	-0.4	0.0	139.8	31.0	17.3	51.8	0.0	100
	C0006E-31X-3, 0-1.5	WR	232.32	52	1,496	711	64	751	47,107	40,802	1,739	35.0	25.8	53.5	-1.2	0.0	114.3	30.6	22.6	46.8	0.0	100
	C0006E-31X-4, 65-66.5	WR	233.34	60	1,080	364	83	2,116	, 37,307	22,932	2,484	36.0	20.6	29.1	-0.3	0.0	85.7	42.0	24.1	33.9	0.0	100
	C0006E-31X-5, 113-115	W	235.24	64	682	211	163	3,146	23,408	15,218	5,695	41.3	12.6	18.8	3.8	3.8	76.6	53.9	16.5	24.6	5.0	100
	C0006E-32X-4, 0-1.5	WR	243.21	82	937	238	96	2,951	32,818	16,511	3,237	39.8	18.1	20.2	0.4	0.4	78.6	50.7	23.1	25.7	0.6	100
	C0006E-32X-5, 23-24.5	WR	243.82	80	1,085	237	66	3,467	38,351	17,230	1,856	45.1	21.3	20.8	-1.9	0.0	87.2	51.8	24.4	23.9	0.0	100
	C0006E-32X-5, 91.5-93	WR	244.51	57	1,112	405	52	2,283	39,770	27,710	1,626	41.0	21.8	35.4	-1.8	0.0	98.2	41.7	22.2	36.1	0.0	100
	C0006E-32X-6, 18.5-20	WR	245.19	58	1,026	310	101	2,802	39,872	21,771	2,757	41.8	22.1	27.1	-0.5	0.0	91.0	45.9	24.2	29.8	0.0	100
	C0006E-32X-7, 55-57	W	246.97	61	788	461	150	2,395	26,624	25,769	5,417	41.4	14.2	33.4	3.6	3.6	92.5	44.8	15.3	36.1	3.8	100
	C0006E-32X-8, 27-29	W	247.60	10	1,089	639	92	1,183	35,005	34,565	3,685	35.4	18.9	45.4	1.6	1.6	101.3	34.9	18.7	44.8	1.6	100
	C0006E-34X-1, 0-5	W	258.33	39	106	52	46	1,584	3,632	2,785	1,828	17.6	1.8	3.2	1.0	1.0	23.6	74.7	7.5	13.5	4.3	100
	C0006E-34X-2, 115-117	W	260.89	85	1,058	275	70	3,426	38,634	19,995	2,782	46.8	21.3	24.6	-0.8	0.0	92.7	50.5	23.0	26.5	0.0	100
	C0006E-34X-3, 94–95.5	WR	262.09	53	1,150	286	90	2,957	36,732	18,434	2,395	41.0	20.3	22.7	-0.9	0.0	84.1	48.8	24.2	27.0	0.0	100
	C0006E-34X-4, 44-45.5	WR	263.01	79	1,195	361	96	3,352	40,832	23,098	2,714	48.2	22.5	28.8	-1.0	0.0	99.4	48.5	22.6	28.9	0.0	100
	C0006E-34X-5, 0-1.5	WR	263.62	58	1,284	278	63	3,362	40,543	18,880	1,952	45.2	22.5	23.0	-1.9	0.0	90.7	49.8	24.8	25.4	0.0	100
	C0006E-35X-2, 0–1.5	WR	268.69	72	954	443	81	1,624	33,409	32,992	3,004	38.6	18.0	43.2	0.5	0.5	100.3	38.5	17.9	43.1	0.5	100
	C0006E-35X-3, 51–52	W	269.57	51	1,647	485	60	1,485	50,511	36,493	1,768	38.9	27.9	47.2	-1.7	0.0	114.1	34.1	24.5	41.4	0.0	100
	C0006E-35X-3, 59–60	W	269.65	63	1,138	318	86	2,695	41,605	22,360	2,279	41.1	23.1	27.9	-1.1	0.0	92.1	44.6	25.1	30.3	0.0	100
	C0006E-35X-3, 118-119.5	WR	270.24	65	1,580	368	82	2,900	47,647	24,798	2,838	44.6	26.5	30.9	-0.8	0.0	102.0	43.7	26.0	30.3	0.0	100
	C0006E-35X-4, 10–11.5	WR	270.56	59	1,162	384	83	2,798	40,532	25,803	3,406	44.7	22.3	32.6	0.2	0.2	99.8	44.8	22.3	32.7	0.2	100
	C0006E-36X-1, 100–101.5	WR	278.33	81	1,349	258	1	3,868	40,495	14,103	1,661	46.7	22.6	16.3	-2.5	0.0	85.6	54.6	26.4	19.0	0.0	100
	C0006E-36X-1, 125–127	W	278.58	57	1,069	276	72	2,934	38,242	17,862	2,337	40.3	21.3	21.8	-0.9	0.0	83.4	48.4	25.5	26.2	0.0	100
	C0006E-36X-4, 0–1.5	WR	281.56	74	1,064	270	88	3,426	37,694	18,056	2,834	45.4	20.8	22.0	-0.6	0.0	88.2	51.5	23.6	24.9	0.0	100
	C0006E-36X-6, 69–71	W	283.65	46	1,899	543	81	1,638	56,562	34,538	1,722	38.8	31.5	44.2	-2.0	0.0	114.5	33.9	27.5	38.6	0.0	100
	C0006E-37X-2, 78.5-80	WR	289.03	67	1,015	254	103	3,281	35,846	17,548	4,087	43.7	19.8	21.4	1.2	1.2	86.1	50.8	23.0	24.8	1.4	100
	C0006E-37X-4, 18.5–20	WR	291.25	64	1,120	322	91	2,511	38,119	23,234	2,599	40.1	21.0	29.3	-0.5	0.0	90.4	44.3	23.3	32.4	0.0	100
	C0006E-37X-4, 58–59.5	WR	291.65	69	1,024	189	56	4,248	35,673	14,424	1,578	50.9	19.7	16.8	-2.7	0.0	87.4	58.2	22.5	19.3	0.0	100
	C0006E-37X-5, 0–1.5	WR	292.12	58	1,238	359	73	1,721	42,883	27,439	2,443	35.1	23.8	35.1	-0.4	0.0	93.9	37.3	25.3	37.4	0.0	100
	C0006E-37X-6, 124–126	W	293.73	69	1,016	247	101	3,231	34,465	15,971	3,548	42.1	19.1	19.3	0.6	0.6	81.1	51.9	23.5	23.8	0.7	100
	C0006E-37X-CC, 14–16	W	295.75	60	1,240	547	93	1,824	40,298	33,625	2,439	40.7	22.0	43.7	-0.6	0.0	106.4	38.3	20.7	41.1	0.0	100
	C0006E-38X-2, 0–1.5	WR	296.70	74	1,103	323	45	3,031	37,491	20,667	1,360	43.3	20.7	25.7	-2.4	0.0	89.7	48.3	23.1	28.6	0.0	100
	C0006E-38X-CC, 21–23	W	297.50	68	610	212	162	2,701	23,777	17,201	6,632	38.4	12.8	21.7	5.3	5.3	78.2	49.1	16.4	27.7	6.8	100
	C0006E-38X-CC, 42–43	W	297.71	44	921	494	104	1,324	30,798	30,567	4,369	34.1	16.6	40.1	2.7	2.7	93.4	36.5	17.8	42.9	2.9	100
	C0006E-39X-1, 131–133	WR	307.14	78	789	220	121	2,615	31,467	17,281	3,995	37.1	17.4	21.4	1.7	1.7	77.6	47.8	22.4	27.6	2.2	100
	C0006E-39X-3, 71–72.5	WR	309.36	72	982	238	69	3,421	34,962	16,997	1,894	44.7	19.3	20.7	-1.7	0.0	84.6	52.8	22.8	24.4	0.0	100
	C0006E-39X-4, 0–1.5	WR	309.69	60	1,051	263	127	3,049	33,798	17,640	3,961	41.6	18.6	21.7	1.2	1.2	83.2	50.0	22.4	26.1	1.5	100
	C0006E-39X-CC, 31–33	WR	315.66	48	940	301	119	2,270	34,906	22,690	4,156	37.5	19.2	28.8	1.9	1.9	87.3	42.9	22.0	33.0	2.1	100
	C0006E-40X-3, 29–31	W	318.45	41	941	276	105	1,897	30,875	18,268	3,354	30.8	17.1	23.0	1.4	1.4	72.2	42.6	23.6	31.9	1.9	100
	C0006E-40X-3, 51–53	W	318.67	79	983	284	64	3,348	39,421	17,331	2,101	44.0	21.9	20.9	-1.6	0.0	86.8	50.7	25.2	24.1	0.0	100
	C0006E-40X-7, 0–1.5	WR	322.01	69	1,141	322	65	3,393	39,152	21,995	2,102	47.8	21.5	27.3	-1.8	0.0	96.7	49.5	22.3	28.3	0.0	100
	C0006E-40X-8, 60–61.5	WR	323.01	66	1,190	329	82	3,140	40,743	20,881	1,875	44.4	22.6	25.8	-1.9	0.0	92.8	47.9	24.3	27.8	0.0	100

Table T4 (continued). (Continued on next page.)

													/	Abunda	ince ca	lculate	d from S	VD norn	nalizati	on fact	or	
				Peak i	ntensity	(counts	/step)	Integra	ted peak	area (tota	l counts)		Calcula	ated ab	undan	ce (wt%	6)	Nor	malized	d abun	dance (wt%)
					-	e				e				e		-				e		
					N	clas			N	clas	0		N	clas		tec	Ite		N	clas		e
	Hole, core, section,	Core	Depth	>	artz	ĝ	cite	>	artz	ġ	cite	>	artz	ĝ	cite	rec		>	artz	<u>j</u> ö	cite	al iv
Unit	interval (cm)	type	CSF (m)	Cla	Ŋ	Plac	Cal	Cla	Ŋ	Plac	Cal	Cla	Ŋ	Place	Cal	cal C	Abs tot	Cla	Ŋ	Pla	Cal	Rela
	000075 /11/ 0 71 70		224.24														4.0.0.0					
	C0006E-41X-2, 71-73	W	326.96	3/	1,146	645 261	/5	8//	37,811	39,539	2,130	35.8	20.4	52.Z	-0.5	0.0	108.3	33.0 50.2	18.8	48.2	0.0	100
	C0006E-41X-3, 44-46		328.09	49	1,045	201	72	3,040	33,132	17,770	2,341	41.5	19.4	21.0	-0.7	0.0	02.0	50.2	23.3	20.4	0.0	100
	C0006E-41X-4, 0-1.5	VVK	320.03	//	1,001	214	/5	3,433	22,044	16,000	2,021	43.0	19.2	10.0	-0.8	0.0	01.0	55.0	23.4	25.0	0.0	100
	C0006E-42X-1, 118-119	VV	220.50	60	1,008	245	110	3,003	33,070	10,337	3,340	41.0	10.3	20.2	0.0	0.0	60.Z	51.1	22.0	25.2	0.9	100
	C0006E-42X-5, 0=1.5		242.26	23	040	214	139	1,020	22,422	15 244	4,371	32.0	10.4	20.2	2.3	2.5	0Z.U	40.0	22.5	24.4	5.1 1.7	100
	C0006E-42X-8, 36.3-38	VVR	242.20	6/	930	214	133	3,827	32,801	15,244	4,390	47.0	10.0	10.2	1.4	1.4	00.Z	33.9	21.2	21.4	1.0	100
	C0006E-43X-5, 0-1.5	VVK	249.11	51	1,102	213	00	2,009	40,734	12 467	2,731	39.4	12.0	20.4	-0.4	0.0	00.4	44.0	23.0	29.0	0.0	100
	C0006E-43X-CC, 28-29		352.30 257.24	54 02	020	1/2	1/0	2,020	22,327	12,407	0,091	24.3	12.2	15.2	5.9	5.9	0/./	50.7	10.0	22.5	0.0	100
	C0006E-44X-5, 117-119		357.34	60 50	1,030	243	11/	3,043	33,423	10,390	3,33Z	42.1	10.4	22.7	0.7	0.7	03.9	30.2	21.9	27.1	0.8	100
	C0006E-44X-5, 0=1.5		262 21	39	997	200	75	2,442	25,020	20,760	1,000	37.0	20.4	20.0	-1.5	0.0	04.U	44.0	24.2	27.4	0.0	100
	C0006E-43X-1, 37.3-39		266.27	70	1,044	203	101	3,090	24 (47	16,151	2,320	45.0	19.7	23.7	-1.0	0.0	00.4	49.0	22.9	27.4	0.0	100
	C0006E-45X-5, 65.5-65		200.27	73	1,091	240	101	3,144	34,047	10,309	3,000	41.7	19.2	20.2	0.0	0.8	01.9	51.0	23.4	24.7	1.0	100
	C0006E 45X - 3, 81.3 - 83		266 66	70	1,129	212	07	2,003	27 721	21,240	1,070	42.0	21.0	20.1	-2.4	0.0	99.Z	JI./	22.0	20.5	0.0	100
	C0006E 45X - 4, 0 - 1.3		270.00	70 61	1,120	233	80	3,003	37,721 43,621	25 4 70	2,015	42.9	20.9	24.Z	-1.5	0.0	00.0	40.0	23.7	426	0.0	100
	C0006E 45X 8 50 51	VV \\\/	370.90	76	756	102	02	2 1 6 4	42,031 27 1 4 7	15 752	2 0 2 2	11 G	23.3	10.5	-1.1	0.0	75.0	54.8	10.5	42.0	0.0	100
	C0006E 46X 1 0 5	VV \\\/	272 22	20	20	64	9Z 13	1 104	27,147	2 802	2,933	12.0	14.0	2.5	0.1	0.1	170	72 /	19.5	10.6	0.1	100
	C0006E 46X - 1, 0 - 3	VV \\\/	372.33	67	022	212	101	2 084	22 672	2,072	/ 013	12.9	19.4	26.8	1.2	1.2	01.0	/2.4	20.2	20 /	1.2	100
	C0006E 46X - 3, 107 - 108	\\/D	376.55	62	1 245	220	72	2,004	20 25 2	25 201	2 4 20	44.0	21.6	20.0	0.0	0.0	91.0	49.1	20.2	22.4	0.0	100
	C0006E-46X-5, 0.1.5	\A/D	377.60	77	1,245	365	88	2,002	<i>JJJZJZ</i>	23,301	2,720	42.4 12.0	21.0	31 /	-0.5	0.0	97.1	1/ T	22.5	324	0.0	100
	C0006E-47X-3 53 54	10/	385.18	67	1,277	255	105	3 004	35 873	18 3//	2,737 A 155	42.2	10.8	22.5	-0.0 1 /	1 /	86.2	10 3	23.4	26.2	1.6	100
	C0006E-47X-3, 93-94 5	\//R	385 58	65	1,170	318	126	2 892	33 648	22 228	4 944	43.4	18.4	22.5	2.5	2.5	923	47.0	19.9	30.4	2.7	100
	C0006E-47X-4 14 5-16	W/R	386.20	60	974	244	202	2,072	32 317	17 227	7 4 9 8	39.6	17.8	20.0	6.1	6.1	84.8	46.8	21.0	25.0	7.2	100
	C0006E-47X-5_0-1_5	W/R	386 72	77	1 1 5 6	299	86	3 251	38 637	22 109	2 942	46.6	21.3	27.5	-0.6	0.0	95.4	48.8	22.3	28.9	0.0	100
	C0006E-48X-1 70-72	W	392.03	56	1 1 9 9	323	151	2 842	38 485	21 025	4 009	41.8	21.3	26.2	1 2	1.2	90.4	46.2	23.5	28.9	13	100
IID	C0006E-1B-1, 130–132	Ŵ	396.30	79	1.089	228	54	3,512	37,830	17,587	1,493	45.8	20.9	21.3	-2.5	0.0	88.1	52.0	23.8	24.2	0.0	100
	C0006F-48X-5_0-1_5	WR	396.98	64	1.099	333	91	3,385	37,436	21.124	2,566	47.2	20.6	26.2	-1.1	0.0	94.0	50.2	21.9	27.9	0.0	100
	C0006E-49X-3, 95–97	W	404.60	70	1.204	297	65	2.919	38,158	20.312	2.535	42.0	21.1	25.2	-0.8	0.0	88.3	47.6	23.9	28.5	0.0	100
	C0006E-49X-4, 0–1.5	WR	404.68	66	1,235	312	75	3,257	39,817	22,615	2,132	46.9	21.9	28.2	-1.7	0.0	97.0	48.4	22.6	29.0	0.0	100
	COOOSE 20 2 0 1 5	\A/D	405 52	72	, 1 1 2 4	200	60	2827	, 11 3 70	20.857	2 506	11 1	22.0	25.8	0.0	0.0	00.2	15 0	25 5	28.6	0.0	100
	$C0006F_2R_2, 0=1.5$	10/	405.52	70	1,104	263	57	2,007	38 270	20,007	2,300	44.2	23.0	25.0	-0.2	0.0	01 /	48.3	23.5	28.6	0.0	100
	$C0006F_3R_1 0_1 5$	\//R	414 00	65	1,147	205	94	3,021	37 918	18 651	3 3 28	42.9	21.1	20.1	0.2	0.0	87.0	40.5	24.2	26.0	0.0	100
	C0006F-3R-2 53 5-55	W/	414.00	66	875	211	105	3 4 5 8	32 899	16 246	3 762	44 7	18.1	19.7	0.2	0.2	83.2	53.7	21.2	23.7	0.2	100
	C0006F-4R-1 86-88	Ŵ	424 36	71	1 291	249	69	3 5 5 9	39 766	17 605	1 837	46.2	22.1	21.2	-2.1	0.0	89.5	51.7	24.6	23.7	0.0	100
	C0006F-4R-2, 33–34 5	WR	425.24	66	972	217	108	3,952	33,434	16.048	3,484	49.4	18.3	19.3	0.0	0.0	87.0	56.7	21.1	22.1	0.0	100
	C0006F-5R-1, 117–118.5	WR	434.17	67	1.132	226	56	2,978	36,503	18,254	1,810	41.1	20.2	22.4	-1.6	0.0	83.7	49.1	24.1	26.8	0.0	100
	C0006F-6R-1, 120–121.5	WR	439.20	71	789	167	265	3.710	26.227	12.760	9.340	45.2	14.3	15.1	8.2	8.2	82.8	54.5	17.3	18.3	9.9	100
	C0006F-7R-1, 10–11	W	447.60	82	890	231	216	4.129	29.342	12.974	6.831	49.2	16.1	15.2	4.5	4.5	84.9	57.9	18.9	17.9	5.3	100
	C0006F-7R-1, 90–91.5	WR	448.40	69	784	168	251	3.718	25.800	10.527	10.951	43.7	14.2	12.1	10.4	10.4	80.3	54.4	17.6	15.0	12.9	100
Ш	C0006F-8R-1, 12.5–14	WR	457.13	93	1.077	182	48	5.552	35,419	12.488	1.550	62.4	19.4	13.8	-3.6	0.0	95.7	65.3	20.3	14.5	0.0	100
	C0006F-8R-1. 50–51	W	457.50	69	1,009	198	60	5,007	32,666	13,230	1,253	57.7	17.8	15.1	-3.6	0.0	90.7	63.6	19.7	16.7	0.0	100
	C0006F-8R-1, 103–104.5	WR	458.03	88	1,049	229	48	5,125	34,510	14,402	1,004	59.6	18.9	16.6	-4.1	0.0	95.1	62.7	19.8	17.5	0.0	100
	C0006F-8R-2, 42.5–44	WR	458.84	84	864	241	157	5,052	28,535	12,675	6,546	58.1	15.4	14.5	3.5	3.5	91.6	63.5	16.9	15.9	3.8	100
	C0006F-9R-1, 53.5–55	WR	467.04	94	961	179	52	6,016	31,322	12,614	1,053	67.3	16.9	14.1	-4.5	0.0	98.3	68.5	17.2	14.3	0.0	100
	C0006F-9R-1, 105.5–106	WR	467.56	98	953	190	151	4,803	30,754	12,115	4,954	55.1	16.8	13.7	1.5	1.5	87.2	63.2	19.3	15.8	1.8	100
	C0006F-9R-1, 105.5–106	WR	467.56	73	653	158	127	3,977	22,600	9,296	4,382	45.2	12.3	10.5	1.8	1.8	69.8	64.8	17.6	15.1	2.5	100

Table T4 (continued).

													ŀ	Abunda	nce ca	lculated	d from S	VD norn	nalizati	on fact	or	
				Peak i	intensity	(counts	/step)	Integra	ated peak	area (tota	l counts)		Calcula	ated ab	undan	ce (wt%	6)	Nor	malize	d abun	dance (wt%)
Unit	Hole, core, section, interval (cm)	Core type	Depth CSF (m)	Clay	Quartz	Plagioclase	Calcite	Clay	Quartz	Plagioclase	Calcite	Clay	Quartz	Plagioclase	Calcite	Corrected calcite	Absolute total	Clay	Quartz	Plagioclase	Calcite	Relative total
	C0006F-9R-2, 41.5-43	WR	468.42	74	1,167	247	80	5,423	37,194	14,063	2,609	62.3	20.4	15.9	-2.3	0.0	98.6	63.1	20.7	16.2	0.0	100
	C0006F-10R-1, 27.5–29	WR	476.28	83	, 935	171	60	5,504	32,107	11,648	1.409	61.5	17.5	12.8	-3.6	0.0	91.8	66.9	19.1	14.0	0.0	100
	C0006F-10R-1, 89-90	W	476.89	82	922	191	58	5,557	32.254	13,280	1.466	63.2	17.5	15.1	-3.7	0.0	95.8	66.0	18.3	15.7	0.0	100
	C0006F-10R-1, 124.5–126	WR	477.25	79	931	171	21	5.006	29.953	11.452	1.706	56.5	16.3	12.8	-2.8	0.0	85.7	66.0	19.1	15.0	0.0	100
	C0006F-11R-1, 0–1.5	WR	485.50	103	944	218	54	5,480	33.890	13,193	1.365	62.3	18.5	14.9	-3.8	0.0	95.7	65.1	19.3	15.6	0.0	100
	C0006F-11B-1_60-61_5	WR	486.10	91	952	186	67	5,790	33,086	12,809	1,851	65.1	18.0	14.3	-3.3	0.0	97.4	66.9	18.5	14.7	0.0	100
	C0006F-11R-2, 46-47, 5	WR	487.48	74	1.022	218	64	3,941	34,656	14.653	2,491	48.1	19.1	17.3	-1.3	0.0	84.6	56.9	22.6	20.5	0.0	100
	C0006F-11R-CC 19 5-21	W/R	488.01	89	742	172	101	4 631	32 181	12 017	3 4 2 3	53.2	177	13.6	_0.4	0.0	84 5	63.0	20.9	16.1	0.0	100
	C0006F-12B-1 62 5-64	W/R	495.63	85	958	209	39	5 241	33 356	12,017	1 408	59.2	18.3	13.6	_3.5	0.0	91.0	65.0	20.2	14.9	0.0	100
	C0006E-12B-2 0-1 5	W/R	496 44	86	996	207	47	4 314	34 687	13 422	1 599	50.9	10.5	15.5	_2 7	0.0	85.5	59.5	20.1	18.1	0.0	100
	$C0006E_{13}R_{-1}$ 119_120 5	W/R	505.69	84	940	203	74	5 236	33 807	11 997	2 585	59.1	18.5	13.3	_2.0	0.0	90.9	65.0	20.4	14.7	0.0	100
	C0006E-13B-2 20-21 5	W/R	506.10	108	1 007	148	74	5 6 5 5	32 024	11 074	2,303	62.6	17.5	12.0	_2.0	0.0	92.1	68.0	19.0	13.1	0.0	100
	C0006E-13B-2 47-50	W/	506.10	36	130	57	344	342	2 760	2 018	28 364	5.9	17.5	2.0	36.7	36.7	46.6	12.7	3.4	5.2	78.7	100
	$C0006E_{13}R_{-2}$ 86 87 5	\\/P	506.76	75	1 017	200	56	5 512	33 540	13 100	20,304	62.7	18.3	1/ 0	21	0.0	95.8	65 /	10.1	15.5	0.0	100
	$C0006F_{14}R_{-1}$ 104-105 5	W/R	515.04	72	916	165	58	4 674	29 545	12 746	2,455	53.7	16.5	14.7	_2.1	0.0	84.6	63.5	19.1	17.4	0.0	100
	$C0006F_{14}R_{-1}$ 111_113	W/	515.04	81	1 050	189	78	4 792	35 923	12,740	2,132	54.7	19.1	13.7	_1.8	0.0	88.3	62.0	22.5	15.5	0.0	100
	$C0006E_{14}R_{-2} 0_{-1} 5$	\//R	515.11	72	782	147	75	4 4 1 8	24 613	11 358	1 864	50.9	13.3	13.7	_2.0	0.0	77 3	65.8	17.2	17.0	0.0	100
	$C0006E_14R_2$ 37 38 5		515.88	96	902	203	50	4 561	23,268	13 206	2 006	53.3	18.3	15.1	-2.0	0.0	86.8	61 /	21.1	17.0	0.0	100
	$C0006E_14R_3 225 24$		517.24	86	822	18/	60	1 930	28 364	10,200	2,000	55 /	15.4	11.2	-2.5	0.0	82.6	67.1	18.7	1/.5	0.0	100
	$C0006E_{15}E_{1} 0 15$		523 50	70	1 077	226	56	5 3 9 6	20,304	13 /15	1 584	61.6	10.1	15.2	-1.0	0.0	02.0	64.2	10.7	15.8	0.0	100
	C0006E-15E-1 35 37	10/	523.50	75	1,077	100	66	5 201	36 5 28	13,413	2 3 2 2 2	50.3	20.1	14.7	-J.J 2 4	0.0	9/1	63.1	21 4	15.6	0.0	100
	C0006E 15P 1 121 122 5	\\/D	524 71	100	024	204	71	5 1 9 2	22 615	12 097	2,322	50.3	17.9	14.7	-2.4	0.0	01.0	64.6	10 /	16.1	0.0	100
	C0006F15R-1, 121-122.5		525 57	87	909	151	10	5 2 2 5	22,013	10 514	2,025	58.0	12.0	14.7	-1.0	0.0	21.2	66.8	20.4	12.1	0.0	100
	C0006F-15R-2, 57-58.5	10/	522.37	101	1 1 / 2	191	71	5 741	25 042	12 060	2 502	64.0	10.0	12.2	-3.1	0.0	06.2	66.1	20.4	12.0	0.0	100
	C0006F-16R-1, 22-24	۷۷ ۱۸/D	534.00	68	070	165	86	1 6 2 4	22 616	10 717	2,302	52.1	19.7	11.2	-2.5	0.0	90.9 91.0	63.6	20.3	14.4	0.0	100
	C0006F + 10R + 1, 100 - 101.3		54265	00 20	970	130	50	4,024	25 6 50	10,/1/	2,413	50 2	10.0	11.0	-1./	0.0	01.9	61.0	22.0	14.4	0.0	100
	C0006F 17R - 1, 13 - 10.3		542.05	00	1,220	170	30 77	5,237	22,020	12272	2 104	20.0	19.0	12.2	-5.1	0.0	90.4	04.0 47.1	21.7	13.3	0.0	100
	C0006F 19P 1 10 12	VV \\\/	552 10	20	930	216	55	5,050	24 707	12,372	1 1 5 5	62.0	10.5	12.7	-1.0	0.0	97.5	66.5	10.9	14.0	0.0	100
	C0006F 10R 1 112 114 5	VV	552.10	99 72	955	10/	33	5116	24,/0/	12,011	2 6 5 1	03.9 50 A	19.0	13.2	-4.2	0.0	90.1	64.0	19.0	15.7	0.0	100
	C0006F-10R-1, 113-114.3		562 72	102	934	164	90	5 6 7 4	22,700	10 514	1 015	20.4	17.9	15.0	-0.5	0.0	09.9	64.9	20.0	13.1	0.0	100
	C0006F-19R-1, 122.3-124		502.75	105	094	109	04	3,0/4	33,40Z	10,514	1,915	02.3 54.3	10.5	11.2	-3.1	0.0	91.0	67.9	19.9	12.2	0.0	100
	C0006F - 19R - 2, 78.3 - 80		564 21	00	007	102	61	4,755	24 402	12,100	2,093	55.0	10.0	13.7	-2.2	0.0	00.3	62.7	21.5	15.9	0.0	100
	C0000F-19R-3, 0-1.3		504.51	01	907	200	02	4,907	25,492	12,107	2,000	55.9	19.0	12.0	-2./	0.0	00.3	05.1	21.5	13.4	0.0	100
	C0006F-19R-3, 43.3-43	VVR	504.75	65	1,120	200	90	5,219	33,300	10,170	3,009	50.0	19.0	12.9	-1.4	0.0	91.1	04.4	21.5	14.1	0.0	100
	C0006F-19R-4, 8-10	VV	565.80	90	947	191	0/	5,430	20,000	10,179	1,600	59.7	10.0	10.0	-3.1	0.0	69.U	07.1	20.8	12.1	0.0	100
	C0006F-19R-CC, 13.3-13	VVK	507.04	107	9/5	152	44	5,429	30,980	10,121	1,070	39.7	10.9	10.0	-3.9	0.0	07.4	00.3	19.4	12.4	0.0	100
	CUUUDF-ZUK-1, U-1.5	VVK	5/1.00	10/	1,031	139	51 011	3,664	54,415	1 4/7	1,543	62.I	18.9	11.1	-5.6	0.0	92.1	6/.4	20.5	12.1	0.0	100
	CUUU6F-20K-1, 10-12	VV	5/1.10	14	//	44	911	616	2,518	1,46/	39,14/	8./	1.4	1.6	50.6	50.6	62.3	14.0	2.3	2.5	81.2	100
		VV	5/2.//	91	9/5	200	48	5,/24	36,977	11,154	986	63.1	20.4	11.9	-4.5	0.0	95.3	66.2	21.4	12.5	0.0	100
	CUUU6F-22K-1, U-1.5	VVR	590.00	82	80/	13/	181	4,834	27,896	8,923	11,340	53.5	15.3	9.5	10.1	10.1	88.3	60.6	1/.3	10./	11.4	100
	CUUU6F-23K-1, 49-50.5	VVR	593.99	92	850	1/4	83	5,368	32,520	11,569	2,827	60.1	17.8	12.8	-1./	0.0	90.7	66.3	19.6	14.1	0.0	100
	CUUU6F-23R-1, /4-/6	vv	594.24	91	8/8	165	164	5,021	31,617	10,612	6,081	56.2	17.4	11.6	2.9	2.9	88.0	63.9	19.7	13.2	3.3	100

Notes: CSF = core depth below seafloor. SVD = singular value decomposition. WR = whole-round, W = working half.

Table T5. XRD mineralogy by unit. (See table note.)

Mineral	Maximum	Minimum	Average	Standard deviation
Unit I				
Clay	52.7	27.9	39.5	6.5
Quartz	32.9	19.1	26.3	3.2
Plagioclase	47.3	24.1	33.0	6.7
Calcite	7.5	0.0	1.2	2.1
Calcite	7.5	0.2	3.2	2.4
Subunit IIA				
Clay	55.0	28.5	42.3	6.6
Quartz	28.6	20.4	24.1	2.5
Plagioclase	46.1	21.0	33.4	6.9
Calcite	2.7	0.0	0.2	0.6
Calcite	2.7	0.5	1.5	1.0
Subunit IIB				
Clay	52.3	31.9	43.1	6.7
Quartz	26.9	22.2	25.4	1.7
Plagioclase	41.6	22.8	31.5	7.4
Calcite	0.0	0.0	0.0	0.0
Calcite	0.0	0.0	0.0	0.0
Subunit IIC				
Clay	74.7	30.6	46.5	7.9
Quartz	29.6	7.5	22.7	3.5
Plagioclase	51.8	13.5	30.0	7.4
Calcite	12.2	0.0	0.8	2.0
Calcite	12.2	0.1	2.7	2.9
Subunit IID				
Clay	57.9	45.9	51.1	3.7
Quartz	25.5	17.3	22.3	2.5
Plagioclase	29.0	15.0	24.6	4.5
Calcite	12.9	0.0	2.0	4.1
Calcite	12.9	0.2	5.1	5.3
Unit III				
Clay	68.5	56.9	64.7	2.4
Quartz	22.6	16.9	19.9	1.4
Plagioclase	20.5	10.7	14.9	1.8
Calcite	11.4	0.0	0.5	1.8
Calcite	11.4	1.8	4.5	3.9

Note: For each subunit, calcite results are first presented for all samples, and then for only those samples containing calcite.



Table T6. Occurrence of carbonate-cemented ash, Site C0006. (See table notes.)

Core, section,	Depth	Rubble/				Mine	ral compositi	on (%)	
interval (cm)	CSF (m)	In situ	XRD	Description	Clay	Quartz	Plagioclase	Calcite	Total
316-C0006E-									
30X-1, 0–5	220.33	Rubble		First occurrence in core? Noted by driller; includes small amount of interlaminated mud.					
34X-1, 0–5	258.33	Rubble	Dolomite	3 fragments; 1 includes interlaminated mud.	17.6	1.8	3.2	1.0	23.6
38X-1, 0–5	296.33	Rubble		Fragment displays fine laminations.					
42X-3, 0–5	334.33	Rubble		2 fragments; both have mud-filled burrows; small one shows possible mineral lining.					
46X-1, 0–5	372.33	Rubble	Dolomite	Sample has fine laminations.	12.9	1.4	3.5	0.0	17.9
46X-1, 3–5	372.30	Rubble							
47X-1, 0–4	381.83	Rubble		Sample has fine laminations.					
316-C0006F-									
12R-1, 7–32	496.40	In situ		Layered at top, burrows in lower part.					
13R-2, 47-50	506.30	In situ	Calcite	Central layer has fine laminations.					
15R-CC, 29–30	527.02	Rubble?		2 fragments; both have possible mud-filled burrows.					
20R-1, 10–12	571.10	In situ?	Calcite	Possible soft-sediment deformation in laminated layer.					
23R-CC, 2–5	594.30	Rubble?		Two rounded pebble-size pieces.					

Notes: Singular value decomposition was used to compute mineral composition factors, following the procedure of Fisher and Underwood (1995). Most samples archived under sample code "316SPCHIP;" also under XRD and PP codes. CSF = core depth below seafloor. XRD = X-ray diffraction.



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Table T7. Calcareous nannofossil range chart of age-diagnostic fossils, Hole C0006E. (See table notes.) (Continued on next page.)

	1		-																					
Epoch	Nani z	nofossil one	Core, section, interval (cm)	Do Top	epth CSF (r Bottom	n) Mean	Abundance	Preservation	Calcidiscus macintyrei	Ceratolithus acutus	Discoaster brouweri	Discoaster pentaradiatus	Discoaster surculus	Emillania huxieyi Genhuroransa soo laraa (>5.5 um)	Contructors sphericage (>3.3 pm)	Gephyrocapsa spp. medium II (>4–5.5 µm)	<i>Gephyrocapsa</i> spp. smaller (<3.5 µm)	Helicosphaera sellii	Pseudoemiliania lacunosa	Reticulofenestra asanoi	Reticulofenestra pseudoumbilicus (5–7 μm)	Reticulofenestra pseudoumbilicus (>7 µm)	Sphenolithus abies	Age interval estimated (Ma)
			316-C0006E- 1H-1, 0			0.01	В																	
	N	N21	1H-CC, 0–5 2H-1, 34	5.13	5.18	5.16 5.19	A	M M	F		Т			F? R?	- [- [D		F	R			R	>0.063-<0.291
	N	N20	2H-CC, 10–15	15.19	15.24	15.22	C	М	R					I	= (C C	C	R	F	R				>0 291-<0 436
		1	3H-2, 112			17.22	B	м	- -							· •			c					>0.2)1 (0.150
			3H-4, 79 3H-CC, 0–5			24.80	R	P	1					1	= (A A C C	A C	Т	c					
			4H-3, 23			27.27	D	M						I	λ	A A	A		Ā	т	т	т		
			4H-CC, 47–52	33.29	33.34	33.31	Т	М						-	г -	ГТ			Т					
			5H-4, 63			36.69	A	M	Т					I	- /	A A	A		A	R	R	R		
			5H-5, 16 5H-CC 0 5	38 / 7	38 52	37.00		M			т				י ר כ	к к = с	K E		R E	P	т	т		>0.436 <0.9
			6H-1, 1	50.47	50.52	38.53	A	M	т		Ť				` c	c c	A		Ċ	Т	•	Ť		20.7-0.7
		NN19	6H-CC, 0–5	38.58	38.63	38.61	С	М			Т			-	Г	c c	С		C			т		
			7H-CC, 0–5	48.63	48.68	48.66	А	М	т					I	२ (C C	С		С		Т			
			8H-CC, 0–5	(2.00		58.13	C	Μ						ļ	- (C C	F		C	_	Т	Т		
Pleistocene			9H-CC, 0-5	63.98 64.51	64.03 64.56	64.01 64.54		P	т					-	- I - I	KA DE	C E		C E	к				
Fleistocerie	istocene		11H-CC. 0–5	71.33	71.38	71.35	A	M	'					1	- (с С	A		г С	R	R	R	R	
	NN110		12H-CC, 0–5	78.15	78.20	78.18	С	Р						Ī	2 (c c	R?		F	F				. 0.0 .1.079
	ININ 19		13H-CC, 0–5			79.20	С	Р						-	ГС	C C	R		С	R	R	Т		>0.9-<1.078
			15X-CC, 0–5	85.49	85.54	85.52	C	М	Т		-			-	r i	ξ C	C	-	C	R	R	R	-	
			16X-CC, 0-5	90.70	90.75	90.73		P			I				1	(F 5 C	R		F			к	F	
			17X-CC, 6–11	107.76	107.81	107.79	R	P							Í	R R	R	Ľ	R				'	
			19X-CC, 0–5	120.88	120.93	120.91	D	М	R					I	र।	F	D	R	С			т	Т	
			20X-4, 100			130.59	F	Р	т					I	R I	R R	F	Т	F			R		
		Reversed	20X-CC, 0–5	133.18	133.23	133.20	F	Р	T	-					l	R R	F	-	F		52		-	>1.078-<1.617?
	Epoch Nannofossil Zone NN21 NN20 NN19 NN19		21X-5, 2	130.28	120 33	139.13		M		I	т				(- C	A P		A		R? 27	т	I T	
			21X-6, 97	137.20	107.00	150.97	c	P	R			т		-	ГІ	R R	F	Τ	c		R?	'	'	
			22X-CC, 0–5	151.39	151.44	151.41	F	M	Т						l	۲.	F		F		R?			
			23X-3, 107			157.72	D	М	С					I	- (C C	Α		А		R?	R	Т	
			23X-CC, 15–20	162.39	162.44	162.41	C	M	R		т				۱ X	C C	F	Т	C	р	R?	R	R	>0.0 <1.04
	1	1	247-1,90	1		104.29		٢			1						F	1	C	к	F	I.		>0.9-<1.04



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Notes: CSF = core depth below seafloor. Abundance: D = dominant, A = abundant, C = common, F = few, R = rare, T = trace, B = barren. Preservation: G = good, M = medium, P = poor. ? = uncertain determination.

Epoch	Nanı z	nofossil one	Core, section, interval (cm)	De Top	epth CSF (r Bottom	n) Mean	Abundance	Preservation	Calcidiscus macintyrei	Ceratolithus acutus Discoaster brouweri	Discoaster pentaradiatus	Discoaster surculus	Emiliania huxleyi	Gephyrocapsa spp. large (>5.5 µm)	Gephyrocapsa spp. medium I (>3.5–4 µm)	<i>Gephyrocapsa</i> spp. medium II (>4–5.5 µm)	<i>Gephyrocapsa</i> spp. smaller (<3.5 µm)	Helicosphaera sellii	Pseudoemiliania lacunosa	Reticulofenestra asanoi	Reticulofenestra pseudoumbilicus (5–7 µm)	Reticulofenestra pseudoumbilicus (>7 µm)	Sphenolithus abies	Age interval estimated (Ma)
		Reversed part of NN19	24X-CC, 0–5 25X-5, 65 25X-CC, 0–5 26X-3, 15	164.49 181.55	164.54 181.60	164.51 179.11 181.57 185.39	F B C C	P P M	T R F	T T T	-			т	C F	F C	R C C		R C C		R F	т		>1.078-<1.617?
Pleistocene	NN19	NN19	26X-CC, 32–37 27X-7, 66 27X-CC, 42–47 28X-CC, 0–5 29X-CC, 0–5 30X-CC, 36.2–41.2 31X-5, 65 31X-CC, 0–5 32X-CC, 0–5 32X-CC, 0–5 35X-CC, 0–5 35X-CC, 0–5 35X-CC, 0–5 39X-CC, 0–5 40X-CC, 0–5 41X-CC, 0–5 41X-CC, 0–5 41X-CC, 0–5 41X-CC, 0–5 41X-CC, 0–5 41X-CC, 0–5 41X-CC, 0–5 45X-5, 65 45X-CC, 6–11 46X-3, 99 46X-CC, 0–5 47X-CC, 4–9	192.43 201.89 205.02 220.59 230.24 235.40 248.08 266.63 286.86 295.61 297.29 315.35 323.76 331.64 343.83 352.08 362.89 380.23 391.38	192.48 201.94 205.07 220.64 230.29 235.45 248.13 266.68 286.91 295.66 297.34 315.40 323.81 331.69 343.88 352.13 362.94 380.28 391.43	192.45 199.58 201.92 205.04 220.61 234.76 234.76 235.42 248.10 266.65 271.12 286.88 295.64 297.32 315.37 343.86 352.11 358.08 362.91 367.70 372.41 376.16 380.25 391.40	D B C C C C D C C C C A A D A A D D A C F A F D B A	$\begin{tabular}{lllllllllllllllllllllllllllllllllll$	R TT T TTTTT TT TRTRTR T	T T T	- - -	т		R T T T T T T T T R R T C?	C FOOFOFFFOOOCOCOCFORC F	A CCCFCFFFCCCCCCCCCCFC C R	D F?CCF?DF?R?CCAADAADCDC?RARD C	т	A CCCCACCCCAAAAAAACFCFA A	F FFFCFFFFCCCCCCCCCFCRC C	R T R R	R RRRRRRFR R TRRCR	R R T T T T T R R R R R R	>0.9-<1.04
			48X-CC, 0–5 49X-5, 54 49X-CC, 0–5 49X-CC, 18	400.84 406.74 406.74	400.89 406.79 406.79	400.86 405.63 406.76 406.92	A D C D	M P P M	I R R T					R T	к R R		C D R C		A A F D	C C R C		к R	r R	>1.04-<1.078

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Table T8. Calcareous nannofossil range chart of age-diagnostic fossils, Hole C0006F. (See table notes.) (Continued on next page.)

Epoch	Nannofossil zone	Core, section, interval (cm)	De Top	epth CSF (ι Bottom	m) Mean	Abundance	Preservation	Amaurolithus delicatus Amaurolithus tricorniculatus	Calcidiscus macintyrei	Ceratolithus acutus	Ceratolithus rugosus	Discoaster asymmetricus	Discoaster brouweri	Discoaster pentaradiatus	Discoaster quinqueramus	Discoaster surculus	Discoaster tarrialis	uepnyrocapsa spp. large (>>.5 µm)	Confirmation spp. Integrating (>3.3-4 pm)		uepriyrocapsa spp. smaller (<3.3 µm)	Helicosphaera sellii	Pseudoemiliania lacunosa	Reticulofenestra asanoi	Reticulofenestra haqii-minutula Beticulofenestra nseradorumhilicus (5_7 um)	Vertranorerrestra pseudourrenteuros (2-7 min)	Keticulotenestra pseudoumbilicus (>/ µm) Sphenolithus abies	Age interval estimated (Ma)
		316-C0006F-	396.87	396.92	306.00	C	D		D)	-		-	-	-	-	-	т	D	~ .	C	-	с С	C	с.			>0.9 <1.04
		2R-1.76	390.87	390.92	396.90 405.26	c	P		F	:								ı R	ĸ	-	F		c	F?	F			>0.9-<1.04
		2R-CC, 0–5	406.94	406.99	406.97	Т	P		•														Т	•••	T			?
		3R-1, 25			414.25	F	Р		Т	-								Т					F	F	R			
		3R-CC, 10–15			415.81	С	Р			Т											F		F	F	F			
Pleistocene	NN19	4R-1, 135	425 40	425 45	424.85	D	М												-		D		A	C	C		-	>1.04-<1.078
		4R-CC, 0-5	425.40	423.43 434 74	425.42 434 71	Δ	M		R	,								т	I		A C		c	c	C I	a	т	
		6R-2.9	434.07	434.74	439.50		P		C	-								' C		~	A		A	C		R	•	
		6R-CC, 0–5	439.70	439.75	439.73	D	M		C	_								c		2	A		A		C F	R		>1.24-<1.46
		7R-CC, 0–5	449.67	449.72	449.70	D	Р		R	ł								С	R	2	С		С		С			
		8R-CC, 0–5	458.98	459.03	459.01	С	Р		R	₹Т			F	F		R	Т				R	Т	F		FΕ	R	R	
		9R-2, 24–26			468.25	С	М			Т			F	F		R	Т				Т		С		CI	R		>2.87-<3.65
		9R-CC, 0–5	468.58	468.63	468.60	B																						
	NN16	10R-1, 24 10R-1 98			476.24	В	м		D	,		D	E	c		P	т				c		c		c		т	
		10R-CC 10-11			477.87	B	IVI			`		ĸ	'	C		IX I	'				C		C		C			
		10R-CC, 0–5	477.77	477.82	477.80	В																						>3.65-<3.79
		11R-1, 38			485.88	В																						
		11R-2, 65			487.67	С	Р	Т 1	R	R R	Т	Т	С	F		F					R	Т			С		F R	
		11R-CC, 0–5	487.81	487.86	487.84	Т	Р						Т										Т		Т		Т	
	NN15-NN13	12R-1, 24			495.24	A	М	Т	? F	R	Т		С	С		R					Т	Т	R		A		с с	>3.97-<5.12
		12R-CC, 0-5	497.67	497.72	497.70	B			г	. т	р		c	c		-									c		c c	
Pliocene		13R-1, 91-92 13R-CC 31	507.41	507.53	507.51	R	R		F	. 1	ĸ		т	т		F									C		R	
		14R-1, 65–68	507.40	507.55	514.66	В	Ň						'														ĸ	
		14R-3, 38			517.40	В																						
		14R-CC, 0–5	518.22	518.27	518.25	Т	Р						Т														т т	
		15R-1, 5			523.55	Т	Р		Т				Т														Т	
		15R-2, 76–77			525.76	Α	М		R	2			F	F											С		с с	
	NN12	15R-CC, 0–5	526.73	526.78	526.75	T	Р		-	_			-	-													T	>5.12-<5.32
		10K-1, 3/ 16R-CC 0 5	535 12	535 19	535.3/ 535.14		P		I T	-			Т Т	I													г	
		17R-1, 11–12	333.13	333.10	542.61	B	F		1				'															
		17R-2, 1			543.89	R	Р		Т	-			R	R													RR	
		17R-CC, 0–5	544.38	544.43	544.40	С	Р	Т	Т			Т	F	F													с с	
		18R-2, 36			553.75	Т	Р																		Т		Т	



66

Table T8 (continued).

Epoch	Nannofossil zone	Core, section, interval (cm)	De Top	epth CSF (r Bottom	n) Mean	Abundance	Preservation	Amaurolithus delicatus	Amaurolithus tricorniculatus Calcidiscus macintyrei	Ceratolithus acutus	Ceratolithus rugosus	Discoaster asymmetricus	Discoaster brouweri	Discoaster pentaraalatus Discoaster auinaueramus	Discoaster surculus	Discoaster tamalis	<i>Gephyrocapsa</i> spp. large (>5.5 µm)	Gephyrocapsa spp. medium l (>3.5–4 µm)	<i>Gephyrocapsa</i> spp. medium II (>4–5.5 µm)	<i>Gephyrocapsa</i> spp. smaller (<3.5 µm)	Helicosphaera sellii	Pseudoemiliania lacunosa	Reticulofenestra asanoi	Reticulofenestra haqii-minutula	Reticulofenestra pseudoumbilicus (5–7 µm)	Reticulofenestra pseudoumbilicus (>7 µm)	Sphenolithus abies	Age interval estimated (Ma)
Pliocene	NN12	18R-CC, 0–5 19R-4, 23 19R-CC, 27 20R-CC, 0–5 21R-CC, 0–5	553.83 567.98 573.36 580.50	553.88 568.03 573.41 580.55	553.86 565.95 568.00 573.39 580.53	T C T B C	Р М	т	т	- т - т			T F	F										T C	F	т с с	T C C	>5.12-<5.32
Miocene		22R-2, 3–4 22R-CC, 12 23R-CC, 4	592.04 594.31	592.09 594.36	591.45 592.06 594.33	C B C	M M		T T	-			F	F	т									C C	F	с с	c c	>5.32-<5.59

Notes: CSF = core depth below seafloor. Abundance: D = dominant, A = abundant, C = common, F = few, R = rare, T = trace, B = barren. Preservation: G = good, M = medium, P = poor. ? = uncertain determination.



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Table T9. Recognized nannofossil events, Holes C0006E and C0006F. (See table notes.)

			Тор		Bottom		Mean
Nannofossil zone	Age (Ma)	Nannofossil event	Core, section, interval (cm)	Depth CSF (m)	Core, section, interval (cm)	Depth CSF (m)	depth CSF (m)
			316-C0006E-		316-C0006E-		
NN21	0.063	X Gephyrocapsa spp. (>3.5 μm)—Emiliania huxleyi	1H-1, 1	0.01	1H-CC, 0–5	5.16	2.59
NN20	0.291	FO Emiliania huxleyi	2H-1, 34	5.19	2H-CC, 10–15	15.22	10.21
NN19	0.436	LO Pseudoemiliania lacunosa	3H-2, 112	17.22	3H-4, 79	18.31	17.76
	0.9	LCO Reticulofenestra asanoi	10H-CC, 0–5	64.54	11H-CC, 0–5	71.35	67.94
	1.078	FO Reticulofenestra asanoi	15X-CC, 0–5	85.52	16X-CC, 0–5	90.73	88.12
Reversed part	1.24	LO Gephyrocapsa spp. large (>5.5 μm)	19X-CC, 0–5	120.91	20X-4, 100	130.59	125.75
of NN19	1.6	LO Calcidiscus macintyrei (≥11 µm)	20X-CC, 0–5	133.20	21X-5, 2	139.13	136.16
	1.617	FO Gephyrocapsa spp. large (>5.5 μm)	23X-CC, 15–20	162.41	24X-1, 96	164.29	163.35
	0.9	LCO Reticulofenestra asanoi	23X-CC, 15–20	162.41	24X-1, 96	164.29	163.35
	1.04	RE Gephyrocapsa spp. (4 µm)	24X-1, 96	164.29	24X-CC, 0–5	164.51	164.40
NN19	0.9	LCO Reticulofenestra asanoi	26X-3, 15–20	185.39	26X-CC, 32–37	192.45	188.92
	1.04	RE Gephyrocapsa spp. (4 µm)	47X-CC, 4–9	391.40	48X-CC, 0–5	400.86	396.13
			316-C0006F-		316-C0006F-		
NN19	1.04	RE Gephyrocapsa spp. (4 µm)	1R-CC, 0–5	396.90	2R-1, 76	405.26	401.08
	1.078	FO Reticulofenestra asanoi	5R-CC, 0–5	434.71	6R-2, 9	439.50	437.11
	1.24	LO Gephyrocapsa spp. large (>5.5 μm)	6R-2, 9	439.50	6R-CC, 0–5	439.73	439.61
	1.46	FCO <i>Gephyrocapsa</i> spp. large (>5.5 μm)	7R-CC, 0–5	449.70	8R-CC, 0–5	459.01	454.35
NN16	2.06	LO Discoaster brouweri	7R-CC, 0–5	449.70	8R-CC, 0–5	459.01	454.35
	2.512	LO Discoaster pentaradiatus	7R-CC, 0–5	449.70	8R-CC, 0–5	459.01	454.35
	2.52	LO Discoaster surculus	7R-CC, 0–5	449.70	8R-CC, 0–5	459.01	454.35
	2.87	LO Discoaster tamalis	7R-CC, 0–5	449.70	8R-CC, 0–5	459.01	454.35
	3.65	LO Sphenolithus spp.	10R-1, 24	476.24	10R-1, 98	476.98	476.61
NN13-NN15	3.79	LO Reticulofenestra pseudoumbilicus (>7 μm)	11R-1, 38	485.88	11R-2, 65	487.67	486.78
	5.12	FO Ceratolithus rugosus	13R-1, 91–92	505.42	13R-CC, 31	507.51	506.46
NN12	5.32	FO Ceratolithus acutus	21R-CC, 0–5	580.53	22R-2, 3–4	591.45	585.99

Notes: CSF = core depth below seafloor. X = crossover in abundance, FO = first occurrence, LO = last occurrence, LCO = last consistent occurrence, RE = reentrance, FCO = first consistent occurrence.

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1H-2	1.27	1.48	1.37	8.0	20.13	1.33900	33.11	559	558	0.88	0.00	507	7.8	27.47	2.86	82	2791
1H-6	5.97	6.19	6.08	7.8	18.93	1.33909	33.61	563	_	_	_	_	9.9	33.98	3.81	90	3547
316-C000	6D-																
1H-2	1.21	1.43	1.32	8.3	17.05	1.33914	33.89	558	558	0.86	1.66	468	11.8	42.70	5.98	42	1001
1H-5	4.04	4.26	4.15	8.0	20.99	1.33895	32.83	558	558	0.88	0.00	489	10.2	34.81	3.67	68	2459
316-C000	6E-																
1H-2	1.21	1.43	1.32	8.0	7.08	1.33923	34.39	563	562	0.86	25.19	495	11.8	47.49	8.76	11	268
1H-5	4.24	4.47	4.36	8.2	21.79	1.33912	33.78	559	559	0.86	4.46	485	11.7	41.18	4.90	32	1039
2H-3	7.79	8.02	7.91	8.2	25.78	1.33912	33.78	562	561	0.85	2.14	484	12.0	42.08	5.11	45	1379
2H-7	12.09	12.33	12.21	8.0	21.49	1.33900	33.11	559	558	0.90	0.00	482	11.3	38.10	4.02	64	2575
3H-3	17.29	17.52	17.40	7.8	18.96	1.33896	32.89	560	559	0.91	0.00	489	10.4	33.83	3.97	89	3694
3H-7	21.66	21.89	21.77	7.8	18.78	1.33892	32.67	563	562	0.92	0.00	490	9.6	34.09	4.57	57	4303
4H-5	29.92	30.16	30.04	77	19 23	1 33901	33 17	564	563	0.96	0.00	491	97	33.86	4 89	68	4751
5H-3	35.84	36.06	35.95	77	19 71	1 33901	33 17	564	563	0.96	0.00	491	89	33.85	5 24	69	4820
7H-4	42.92	43.16	43.04	7.8	20.48	1 33903	33.28	568	567	0.99	0.00	493	8.8	34 37	5.88	60	5194
8H-4	51 79	52.03	51 91	7.8	19.50	1 33907	33.50	565	564	0.96	0.00	493	9.1	32 79	5.84	34	5136
0H-5	62 /1	62.64	62.53	7.0	10.30	1 33907	33.50	569	568	1.06	0.00	105	2.1 8.7	32.77	6 1 5	30	5285
104.9	64.51	64.67	64 50	7.9	10.27	1 22027	22 17	568	567	0.06	0.00	407	0.7	21.24	5 00	26	58/1
	67.70	67.07	27.01	7.0	19.37	1.33737	22 61	540	560	1 01	0.00	497	9.0	22.54	5.55	20	5120
110-4 100 2	76 21	76 50	76 41	7.7	19.50	1.33909	21 21	509	500	0.02	0.00	495	0.5	22.20	5.52	44	5220
120-0	70.31 01 72	70.32 01.07	70.41 01 07	7.7	17.11	1.33001	22 52	527	520	1.02	0.00	405	7.0 0.0	20.74	2.32	10	5570
10A-4	01./0	00.24	01.0/	7.0	17.79	1.33913	33.3Z	500	507	1.02	0.00	497	0.0	20.00	0.21	13	55/0
107-2	90.11	90.54	90.25	7.0	17.57	1.33919	33.30	509	500	0.99	0.00	497	0.4	30.98	0.24	12	2020
1/X-3	110.30	100.55	100.43	7.8	16.30	1.33940	33.66	5/2	5/1	0.98	0.00	503	8.1	29.29	0.19	2 17	6042
198-5	119.76	120.08	119.92	7.8	16.28	1.33908	33.30	566	202	1.02	0.00	496	/./	29.27	7.04	17	5458
20X-7	132.85	133.18	133.01	7.8	14.75	1.33937	33.47	567	566	1.02	0.00	501	8./	26.02	6.70	2	6098
218-3	137.38	137.70	137.54	7.8	14.28	1.33907	33.19	562	561	1.00	0.00	493	7.6	27.57	7.03	/	568/
22X-3	146.83	147.18	147.00	7.9	13.96	1.33902	33.22	565	564	1.03	0.00	495	/.8	27.84	7.35	2	5/45
23X-4	157.74	158.08	157.91	7.8	13.66	1.33907	33.13	568	56/	1.02	0.00	503	6.9	25.50	7.30	9	5//5
25X-/	180.79	181.13	180.96	7.9	13.25	1.33911	33.29	566	565	1.02	0.00	500	8.0	24.24	8.66	11	5514
26X-4	186.65	186.96	186.80	/./	12.41	1.33901	32.45	565	564	1.03	0.00	503	7.1	22.05	8.68	9	5/58
27X-5	197.49	197.87	197.68	7.8	11.34	1.33898	33.00	567	566	1.02	0.00	498	7.2	24.64	9.32	6	5387
28X-3	203.81	204.17	203.99	7.9	11.64	1.33893	32.72	561	560	1.03	0.00	501	7.3	20.74	8.86	3	5010
29X-7	219.04	219.38	219.21	7.7	10.32	1.33896	32.89	564	563	0.98	0.00	503	7.2	20.69	8.97	7	4378
30X-3	223.16	223.54	223.35	7.7	10.39	1.33899	32.67	556	555	1.00	0.00	497	7.0	19.37	9.01	4	4984
31X-3	232.32	232.69	232.50	7.6	8.24	1.33922	32.68	565	564	0.98	0.00	508	7.1	17.56	8.94	4	5273
32X-4	243.21	243.59	243.40	7.6	10.12	1.33889	32.50	560	559	0.99	0.00	502	6.9	19.41	8.79	3	4700
34X-5	263.62	264.00	263.81	7.5	10.57	1.33931	32.60	559	558	0.98	0.00	504	6.6	16.53	9.80	3	5228
35X-2	268.69	269.06	268.87	7.5	10.51	1.33930	32.61	559	558	0.99	0.00	504	6.3	16.73	10.18	3	5334
36X-4	281.56	281.92	281.74	7.7	9.97	1.33907	32.18	543	542	0.96	0.00	490	6.5	16.25	9.67	3	4825
37X-5	292.12	292.49	292.30	8.0	10.06	1.33889	31.96	534	533	0.96	0.00	481	6.8	16.33	9.44	1	4642
38X-2	296.70	296.91	296.80	_	_	1.33905	32.27	553	552	0.97	0.00	491	6.8	15.68	9.61	1	4787
39X-4	309.69	310.07	309.88	7.7	9.09	1.33933	32.22	550	549	0.97	0.00	500	6.6	13.70	9.78	4	5312
40X-7	322.01	322.41	322.21	7.8	9.74	1.33909	32.38	550	549	0.97	0.00	501	5.9	14.93	9.68	3	4308
41X-4	328.83	329.21	329.02	7.9	9.33	1.33882	32.11	552	551	0.95	0.00	495	6.5	17.68	9.96	3	3819
42X-5	339.58	339.99	339.78	7.6	8.94	1.33930	32.17	552	551	0.94	0.00	501	6.3	13.92	10.55	0	4838
43X-5	349.11	349.49	349.30	7.7	8.54	1.33906	32.12	551	550	0.96	0.00	496	6.7	15.44	10.78	1	4237

Table T10. Corrected geochemistry results from interstitial waters, Site C0006. (See table notes.) (Continued on next page.)

Salinity

35.00

Chlorinity Cl

(mM)

552

(mM)

552

Refractive

index

1.33635

Alkalinity

(mM)

2.69

SO₄ (mM)

29.10

Na

(mM)

479

Κ

(mM)

9.5

Mg (mM)

52.39

Ca

(mM)

9.90

 PO_4

(µM)

3

 NH_4

(μM)

0

Br

(mM)

0.83

Depth CSF (m)

Bottom

NA

Average

NA

рΗ

7.8

Core,

section

Seawater

316-C0006C-

Тор

NA



Table T10 (continued).

Core,	D	epth CSF (i	m)		Alkalinity	Refractive		Chlorinity	Cl	Br	SO₄	Na	к	Mq	Ca	PO₄	NH₄
section	Тор	Bottom	Average	рН	(mM) ´	index	Salinity	(mM) [´]	(mM)	(mM)	(mM)	(mM)	(mM)	(mM)	(mM)	(µM)	(µM)
45X-4	366.66	367.05	366.86	7.5	7.80	1.33883	32.17	550	549	0.96	0.00	492	6.6	16.88	10.78	1	3427
46X-5	377.60	377.99	377.80	8.2	6.26	1.33882	32.11	543	542	0.96	0.00	488	6.8	15.10	10.11	3	3595
47X-5	386.72	387.10	386.91	7.9	7.08	1.33889	32.50	549	548	_	0.00	485	6.8	18.71	11.46	1	3224
48X-5	396.98	397.40	397.19	8.2	5.76	1.33887	31.92	542	541	0.93	0.00	486	6.6	15.48	10.58	1	3238
49X-4	404.68	405.09	404.89	8.4	6.37	1.33877	31.83	544	543	0.94	0.00	488	7.5	14.89	11.06	0	2985
316-C000	6F-																
2R-2	405.52	405.91	405.72	8.2	7.12	1.33876	31.78	553	552	0.95	0.00	498	5.6	15.19	11.29	0	2385
3R-1	414.00	414.39	414.20	8.1	5.82	1.33872	31.56	545	544	0.94	0.00	490	5.9	15.16	10.95	3	2234
4R-2	424.91	425.27	425.09	8.1	6.18	1.33896	32.16	546	545	0.92	0.00	489	6.5	15.64	11.18	4	2680
5R-1	434.25	434.50	434.37	7.8	6.12	1.33874	31.67	545	544	0.93	0.00	493	6.1	14.45	10.45	4	2252
6R-1	439.08	439.41	439.25	7.9	4.26	1.33888	31.76	551	550	0.90	0.00	493	6.7	16.43	10.06	0	1860
7R-1	448.40	448.66	448.53	7.5	6.34	1.33869	31.39	544	543	0.94	0.00	493	5.7	13.71	10.75	0	1634
8R-1	458.03	458.41	458.22	7.6	6.88	1.33869	31.39	542	541	0.89	0.00	490	5.1	14.00	12.02	3	1607
9R-1	467.04	467.45	467.24	7.6	8.17	1.33876	31.78	545	544	0.91	0.00	492	5.6	14.62	12.23	4	1563
10R-1	477.25	477.50	477.37	7.8	7.75	1.33875	31.72	544	543	0.92	0.00	493	5.8	12.83	12.78	4	1256
11R-1a	485.50	485.64	485.57	8.1	6.16	1.33896	32.09	542	541	0.88	0.00	482	6.9	16.79	12.24	4	908
11R-1b	485.88	486.20	486.04	0.0	_	1.33869	31.39	_	_	_	0.00	_	6.6	12.78	12.47	_	_
12R-2	496.44	496.84	496.64	8.1	6.91	1.33873	31.61	544	543	0.91	0.00	492	5.7	12.37	13.32	5	1271
13R-2	505.90	506.30	506.10	8.2	4.70	1.33871	31.07	541	540	0.89	0.00	481	6.1	14.92	13.56	3	1193
14R-2	516.58	517.02	516.80	8.0	6.03	1.33887	31.98	542	541	0.90	0.00	488	6.1	12.66	13.85	1	1045
15R-1	523.50	523.90	523.70	8.0	5.08	1.33873	31.18	542	541	0.89	0.00	485	4.2	13.13	15.45	4	1030
16R-1	534.00	534.42	534.21	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC
17R-1	542.65	543.06	542.86	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC
18R-1	553.11	553.50	553.31	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC
19R-3	565.26	565.67	565.46	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC
20R-1	571.18	571.49	571.34	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC
22R-1	590.00	590.42	590.21	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC	NC

Notes: CSF = core depth below seafloor. Na calculated from charge balance. — = not analyzed, NC = not corrected (values are in Table T12 and are plotted in the figures).



 Table T11. Corrected concentrations of minor elements in interstitial waters, Site C0006. (See table notes.)

 (Continued on next page.)

6	D	epth CSF (m)			Mino	r elemer	nts (um)		
section	Тор	Bottom	Average	Li	В	Sr	Ва	Si	Fe	Mn
Seawater	NA	NA	NA	25.8	395	79	0.0	3	0.23	0.26
316-C000	6C-									
1H-2	1.27	1.48	1.37	11.7	443	66	10.3	744	0.52	0.57
1H-6	5.97	6.19	6.08	10.5	442	68	10.2	642	0.66	1.50
316-C000	6D-		4.20							
1H-2	1.21	1.43	1.32	20.5	494	74	2.4	613	0.27	0.59
IH-5	4.04	4.26	4.15	14.5	461	70	10.8	/64	0.28	0.54
316-C000	6E-	1 42	1 2 2	21.0		00	0.6	427	0.72	6.01
1H-2	1.21	1.43	1.32	31.8	556	80	0.6	43/	0.72	6.91
1 Π-3 2 Ц 2	4.24	4.47 0.02	4.30	23.9	514	74	5.0 7 1	201	0.00	0.64
2H-7	12.00	12 33	12 21	15.5	704 704	70	127	695	0.40	0.08
3H-3	17.09	17.55	17.40	13.1	456	77	12.7	563	4 88	1 30
3H-7	21.66	21.89	21.77	15.2	484	80	10.9	595	39.96	3.29
4H-5	29.92	30.16	30.04	12.6	433	79	10.3	524	2.33	4.66
5H-3	35.84	36.06	35.95	11.6	419	83	11.7	468	5.02	4.55
7H-4	42.92	43.16	43.04	13.4	409	89	12.1	471	1.93	4.17
8H-4	51.79	52.03	51.91	14.8	437	89	12.3	568	8.85	5.24
9H-5	62.41	62.64	62.53	14.5	413	91	12.4	538	6.46	7.46
10H-8	64.51	64.67	64.59	13.5	446	92	14.3	492	14.60	16.13
11H-4	67.70	67.91	67.81	13.4	416	93	12.7	490	28.21	7.08
12H-6	76.31	76.52	76.41	7.3	404	74	9.0	465	23.04	5.81
15X-4	81.76	81.97	81.87	9.7	395	79	8.9	529	0.91	3.25
16X-2	90.11	90.34	90.23	15.0	311	80	10.0	462	1.88	5.48
17X-3	100.30	100.55	100.43	12.8	370	80	12.2	537	1.02	4.81
19X-5	119.76	120.08	119.92	13.7	389	81	10.4	593	4.86	5.22
20X-7	132.85	133.18	133.01	32.9	231	80	12.0	369	10.76	5.10
21X-3	137.38	137.70	137.54	12.9	248	74	9.4	573	0.64	3.57
22X-3	146.83	147.18	147.00	14.8	223	76	9.6	417	0.55	3.15
23X-4	157.74	158.08	157.91	13.3	248	77	9.3	675	0.78	4.11
25X-/	180.79	181.13	180.96	28.1	233	85	13.8	535	1.2/	5.14
268-4	107.40	107.90	186.80	15./	230	/9	12.4	/ 32	2./1	5.26
27 - 3	202.81	204 17	202.00	20.2 15.7	205	0Z 91	12.1	4/1 5/2	50.03	4.94
207-2	203.01	204.17	203.99	13./	1//	01 97	12.2	54Z	0.91	0.70 5.54
297-7	219.04	219.30	219.21	27.0	178	86	13.2	675	1.05	5.61
31X-3	223.10	223.54	223.55	21.0	170	85	13.6	676	0.21	5.26
32X-4	232.32	232.07	232.30	21.2	219	85	12.3	741	0.45	4 46
34X-5	263.62	264.00	263.81	25.5	157	91	14.8	649	8.07	6.35
35X-2	268.69	269.06	268.87	18.3	142	89	14.4	571	2.59	8.40
36X-4	281.56	281.92	281.74	19.2	200	81	13.5	765	2.96	6.59
37X-5	292.12	292.49	292.30	21.2	173	86	13.3	653	0.77	4.32
38X-2	296.70	296.91	296.80	22.1	191	85	13.4	764	0.67	4.71
39X-4	309.69	310.07	309.88	28.3	163	89	15.4	693	2.36	5.34
40X-7	322.01	322.41	322.21	23.7	179	91	13.7	830	0.50	5.86
41X-4	328.83	329.21	329.02	26.2	141	92	12.6	763	2.09	4.42
42X-5	339.58	339.99	339.78	25.6	157	97	15.1	759	13.84	7.04
43X-5	349.11	349.49	349.30	32.0	134	98	14.2	450	3.42	6.55
44X-5	358.99	359.37	359.18	29.7	174	104	15.8	723	0.82	7.90
45X-4	366.66	367.05	366.86	31.0	170	102	15.4	715	0.78	6.68
46X-5	377.60	377.99	377.80	29.8	147	105	19.0	385	0.59	3.39
47X-5	386.72	387.10	386.91	34.3	162	117	24.3	573	0.60	6.89
48X-5	396.98	397.40	397.19	38.8	147	115	35.7	454	0.52	5.54
49X-4	404.68	405.09	404.89	54.6	169	116	25.7	328	0.43	5.49
316-C000	6F-									
2R-2	405.52	405.91	405.72	41.9	186	124	66.6	560	0.95	9.28
3R-1	414.00	414.39	414.20	44.5	166	125	93.7	764	0.18	7.97
4K-2	424.91	425.27	425.09	5/.0	133	114	25.0	544	0.13	4.13
SR-1	434.25	434.50	434.37	64.4	166	109	35.4	651	0.12	5.23
6K-1	439.08	439.41	439.25	/1.5	1/0	105	32./	/64	0.22	3.8/
/K-I 0D 1	448.40	448.66	448.55	80.4	155	119	/4./	911	0.92	4.03
0K-1 0D 1	430.03	430.41 167 15	4J0.22 167 24	92.1	104 164	107	41.ð 11.0	702 077	U.15 2 77	0.30 11 44
211-1 10P-1	407.04	407.43	407.24	20.0 102 Q	167	11/	95.0	723 978	5.Z/ 2.45	19 10
11R-1a	485.50	485.64	485.57	94.7	131	96	26.1	581	0.13	10.19
							- 2			



Table T11 (continued).

Core	De	epth CSF (i	m)			Mino	r elemen	ıts (µm)		
section	Тор	Bottom	Average	Li	В	Sr	Ва	Si	Fe	Mn
11R-1b	485.88	486.20	486.04	101.7	69	104	31.4	393	0.00	6.40
12R-2	496.44	496.84	496.64	111.5	140	107	52.5	743	0.25	16.78
13R-2	505.90	506.30	506.10	110.6	111	97	27.8	576	0.11	7.16
14R-2	516.58	517.02	516.80	124.1	111	102	42.6	470	0.00	8.39
15R-1	523.50	523.90	523.70	119.3	118	107	44.9	648	0.00	21.98
16R-1	534.00	534.42	534.21	NC	NC	NC	NC	NC	NC	NC
17R-1	542.65	543.06	542.86	NC	NC	NC	NC	NC	NC	NC
18R-1	553.11	553.50	553.31	NC	NC	NC	NC	NC	NC	NC
19R-3	565.26	565.67	565.46	NC	NC	NC	NC	NC	NC	NC
20R-1	571.18	571.49	571.34	NC	NC	NC	NC	NC	NC	NC
22R-1	590.00	590.42	590.21	NC	NC	NC	NC	NC	NC	NC

Notes: CSF = core depth below seafloor. NA = not applicable, NC = not corrected (see Table T13 for values).



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Core, _ section	Depth CSF (m)				Alkalinity	/ Refractive		Chlorinity	Cl	Br	SO4	Na	к	Mg	Ca	PO ₄	NH_4
	Тор	Bottom	Average	рН	(mM) ໌	index	Salinity	(mM)	(mM)	(mM)	(mM)	(mM)	(mM)	(mM)	(mM)	(µm)	(µm)
316-C0006	6C-																
1H-2	1.27	1.48	1.37	8.0	20.13	1.33900	33.11	559	558	0.88	0.00	507	7.8	27.50	2.86	82	2791
1H-6	5.97	6.19	6.08	7.8	18.93	1.33909	33.61	563					9.9	34.00	3.81	90	3547
316-C0006	6D-																
1H-2	1.21	1.43	1.32	8.3	17.05	1.33914	33.89	558	558	0.86	1.66	468	11.8	42.70	5.98	42	100
1H-5	4.04	4.26	4.15	8.0	20.99	1.33895	32.83	558	558	0.88	0.00	489	10.2	34.80	3.67	68	2459
316-C0006	6E-																
1H-2	1.21	1.43	1.32	8.0	7.08	1.33923	34.39	563	562	0.86	25.19	495	11.8	47.50	8.76	11	268
1H-5	4.24	4.47	4.36	8.2	21.79	1.33912	33.78	559	559	0.86	4.46	485	11.7	41.20	4.90	32	1039
2H-3	7.79	8.02	7.91	8.2	25.78	1.33912	33.78	562	561	0.85	2.14	484	12.0	42.10	5.11	45	1379
2H-7	12.09	12.33	12.21	8.0	21.49	1.33900	33.11	559	558	0.90	0.00	482	11.3	38.10	4.02	64	257
3H-3	17.29	17.52	17.40	7.8	18.96	1.33896	32.89	560	559	0.91	0.00	489	10.4	33.80	3.97	89	3694
3H-7	21.66	21.89	21.77	7.8	18.78	1.33892	32.67	563	562	0.92	0.00	490	9.6	34.10	4.57	57	4303
4H-5	29.92	30.16	30.04	7.7	19.23	1.33901	33.17	564	563	0.96	0.00	491	9.7	33.90	4.89	68	4751
5H-3	35.84	36.06	35.95	7.7	19.71	1.33901	33.17	564	563	0.96	0.00	491	8.9	33.90	5.24	69	4820
7H-4	42.92	43.16	43.04	7.8	20.48	1.33903	33.28	568	567	0.99	0.00	493	8.8	34 40	5.88	60	5194
8H-4	51.79	52.03	51.91	7.8	19.50	1.33907	33.50	565	564	0.96	0.00	493	9.1	32.80	5.84	34	5136
9H-5	62 41	62.63	62 53	77	19.24	1 33907	33 50	569	568	1.06	0.00	495	87	33 20	615	39	5284
10H-8	64 51	64.67	64 59	7.8	17.83	1 33909	33.61	567	566	0.94	2.69	495	9.1	33.80	6 3 5	24	5301
11H_/	67 70	67.07	67.81	7.0	19.36	1 33909	33.61	569	568	1 01	0.00	495	83	33.60	6.42	44	5120
1246	76 21	76.52	76 41	7.7	16.42	1 2 2 8 6 0	21 20	520	528	0.01	1 40	463	70	20.00	5.72	15	1071
157 4	70.31 01 72	70.JZ 01.07	70.41 01.07	7.7	17.42	1.33009	22 56	529	520	1.02	0.71	403	7.5	29.90	6 20	13	511
120-4	01.70	01.97	01.07	7.0	17.42	1.33900	22 41	500	567	0.02	0.71	497	0.0	21.20	6.50	15	5442
107-2	90.11	100 55	90.23	7.0	17.07	1.33909	22.01	500	507	0.90	0.90	497	0.5	21.70	0.50		5400
1/ 1/ 1/ 1/ 1/ 1/ 1/ 1/ 1/ 1/ 1/ 1/ 1/ 1	100.50	100.33	110.45	7.0	16.29	1.33912	22.70	5/1	570	1.02	2.00	100	0.2	20.20	7.04	17	549
197-2	119.70	120.00	119.92	7.0	10.20	1.33908	22.20	500	202	1.02	0.00	490	/./	29.50	7.04	17	5450
20X-7	132.85	133.18	133.01	7.8	13.63	1.33909	33.01	566	565	1.00	2.70	499	8.8	28.50	6.99	2	5532
218-3	137.38	137.70	137.54	7.8	14.07	1.33902	33.22	562	561	0.99	0.52	493	7.6	28.02	7.09	/	5583
228-3	146.83	147.18	147.00	7.9	13.96	1.33902	33.22	565	564	1.03	0.00	495	7.8	27.84	7.35	2	5/43
238-4	157.74	158.08	157.91	7.8	13.42	1.33901	33.17	568	56/	1.01	0.62	503	6.9	26.07	7.35	9	565
25X-/	180.79	181.13	180.96	7.9	12.99	1.33904	33.33	566	565	1.02	0.72	499	8.0	24.90	8.69	11	53/8
26X-4	186.65	186.96	186.80	7.7	11.99	1.33890	32.56	565	564	1.02	1.26	502	7.2	23.36	8.73	9	5510
27X-5	197.49	197.87	197.68	7.8	11.34	1.33898	33.00	567	566	1.02	0.00	498	7.2	24.64	9.32	6	5387
28X-3	203.81	204.17	203.99	7.9	11.64	1.33893	32.72	561	560	1.03	0.00	501	7.3	20.74	8.86	3	5010
29X-7	219.04	219.38	219.21	7.7	10.32	1.33896	32.89	564	563	0.98	0.00	503	7.2	20.69	8.97	7	4378
30X-3	223.16	223.54	223.35	7.7	10.23	1.33893	32.72	556	555	1.00	0.62	497	7.1	20.07	9.03	4	4878
31X-3	232.32	232.69	232.50	7.6	7.73	1.33896	32.89	564	563	0.97	2.65	505	7.3	20.73	9.02	4	4793
32X-4	243.21	243.59	243.40	7.6	10.12	1.33889	32.50	560	559	0.99	0.00	502	6.9	19.41	8.79	3	4700
34X-5	263.62	264.00	263.81	7.5	9.63	1.33896	32.89	558	557	0.96	3.46	501	7.0	20.80	9.81	3	4607
35X-2	268.69	269.06	268.87	7.6	9.61	1.33896	32.89	558	557	0.97	3.37	501	6.7	20.86	10.15	3	4717
36X-4	281.56	281.92	281.74	7.7	9.43	1.33887	32.39	544	543	0.95	2.18	489	6.7	18.96	9.69	3	4463
37X-5	292.12	292.49	292.30	8.0	9.83	1.33881	32.06	535	534	0.96	0.91	481	6.9	17.46	9.45	1	4497
38X-2	296.70	296.91	296.80	_	_	1.33888	32.44	553	552	0.96	1.81	490	6.9	17.97	9.63	1	4488
39X-4	309.69	310.07	309.88	7.8	8.19	1.33891	32.61	550	549	0.95	4.09	497	7.0	19.14	9.80	4	4564
40X-7	322.01	322.41	322.21	7.8	9.26	1.33890	32.56	551	550	0.96	1.99	499	6.1	17.49	9.69	3	4014
41X-4	328.83	329.21	329.02	7.9	9.33	1.33882	32.11	552	551	0.95	0.00	495	6.5	17.68	9.96	3	3819
42X-5	339.58	339.99	339.78	7.6	8.09	1.33890	32.56	552	551	0.93	3.94	498	6.7	19.13	10.46	0	4183
43X-5	349.11	349.49	349.30	7.7	8.12	1.33886	32.33	551	550	0.95	2.11	495	6.9	18.12	10.71	1	3929
44X-5	358.99	359.37	359.18	7.7	8.04	1.33885	32.28	548	547	0.93	3.55	495	6.9	17.86	10.78	0	3717
45X-4	366.66	367.05	366.86	7.5	7.80	1.33883	32.17	550	549	0.96	0.00	492	6.6	16.88	10.78	1	3427
46X-5	377 60	377 99	377 80	8.2	6.26	1 33882	32.11	543	542	0.96	0.00	488	6.8	15 10	10.11	3	3595

 Table T12. Uncorrected geochemistry results from interstitial waters, Site C0006. (See table notes.) (Continued on next page.)



Table T12 (continued).

Core, Depth CSF (m)		m)		Alkalinity	Refractive		Chlorinity	Cl	Br	SO₄	Na	к	Ma	Ca	PO₄	NH	
section	Тор	Bottom	Average	рН	(mM)	index	Salinity	(mM)	(mM)	(µm)	(μm)						
47X-5	386.72	387.10	386.91	7.9	7.08	1.33889	32.50	549	548	_	0.00	485	6.8	18.71	11.46	1	3224
48X-5	396.98	397.40	397.19	8.2	5.68	1.33880	32.00	542	541	0.93	0.76	486	6.7	16.45	10.56	1	3153
49X-4	404.68	405.09	404.89	8.4	6.37	1.33877	31.83	544	543	0.94	0.00	488	7.5	14.89	11.06	_	2985
316-C000	6F-																
2R-2	405.52	405.91	405.72	8.2	7.12	1.33876	31.78	553	552	0.95	0.00	498	5.6	15.19	11.29	0	2385
3R-1	414.00	414.39	414.20	8.1	5.82	1.33872	31.56	545	544	0.94	0.00	490	5.9	15.16	10.95	3	2234
4R-2	424.91	425.27	425.09	8.1	6.04	1.33885	32.28	546	545	0.92	1.20	489	6.6	17.15	11.13	4	2570
5R-1	434.25	434.50	434.37	7.8	6.12	1.33874	31.67	545	544	0.93	0.00	493	6.1	14.45	10.45	4	2252
6R-1	439.08	439.41	439.25	7.9	4.20	1.33878	31.89	551	550	0.90	1.19	493	6.8	17.90	10.06	0	1784
7R-1	448.40	448.66	448.53	7.5	6.34	1.33869	31.39	544	543	0.94	0.00	493	5.7	13.71	10.75	0	1634
8R-1	458.03	458.41	458.22	7.6	6.88	1.33869	31.39	542	541	0.89	0.00	490	5.1	14.00	12.02	3	1607
9R-1	467.04	467.45	467.24	7.6	8.17	1.33876	31.78	545	544	0.91	0.00	492	5.6	14.62	12.23	4	1563
10R-1	477.25	477.50	477.37	7.8	7.75	1.33875	31.72	544	543	0.92	0.00	493	5.8	12.83	12.78	4	1256
11R-1a	485.50	485.64	485.57	8.1	6.00	1.33884	32.22	542	542	0.88	1.30	482	7.0	18.39	12.13	4	868
11R-1b	485.88	486.20	486.04	_	_	1.33869	31.39	_	0	—	0.00	_	6.6	12.78	12.47	_	_
12R-2	496.44	496.84	496.64	8.1	6.91	1.33873	31.61	544	543	0.91	0.00	492	5.7	12.37	13.32	5	1271
13R-2	505.90	506.30	506.10	8.2	4.65	1.33865	31.17	541	540	0.89	0.69	481	6.2	15.81	13.48	3	1165
14R-2	516.58	517.02	516.80	8.0	5.95	1.33881	32.06	543	542	0.90	0.71	488	6.1	13.62	13.75	2	1020
15R-1	523.50	523.90	523.70	8.0	5.02	1.33867	31.28	542	542	0.89	0.72	485	4.3	14.10	15.31	4	1005
16R-1	534.00	534.42	534.21	7.5	4.02	1.33892	32.67	562	562	0.88	1.85	499	4.8	15.67	16.86	3	1020
17R-1	542.65	543.06	542.86	7.6	3.89	1.33869	31.39	535	534	0.86	5.83	488	4.7	12.42	15.81	4	784
18R-1	553.11	553.50	553.31	7.7	3.34	1.33876	31.78	538	538	0.88	4.74	492	3.6	10.90	16.69	3	700
19R-3	565.26	565.67	565.46	_	_	1.33856	30.67	521	520	0.83	6.03	469	3.8	11.96	17.69	3	890
20R-1	571.18	571.49	571.34	_	_	1.33849	30.28	519	518	0.84	4.12	468	3.2	9.80	17.96	3	769
22R-1	590.00	590.42	590.21	7.8	3.32	1.33870	31.44	532	531	0.86	4.01	477	4.8	13.85	16.16	_	656

Notes: CSF = core depth below seafloor. Na calculated from charge balance. — = not analyzed.



 Table T13. Uncorrected concentrations of minor elements in interstitial waters, Site C0006. (See table notes.)

 (Continued on next page.)

Core	D	epth CSF (i	m)	Minor elements (µm)									
section	Тор	Bottom	Average	Li	В	Sr	Ba*	Ba†	Si	Fe	Mn		
316-C000)6C-												
1H-2	1.27	1.48	1.37	11.73	443	66	10.3	10.3	744	0.52	0.57		
1H-6	5.97	6.19	6.08	10.53	442	68	10.2	10.2	642	0.66	1.50		
316-C000	6D-												
1H-2	1.21	1.43	1.32	20.55	494	74	2.4	2.5	613	0.27	0.59		
1H-5	4.04	4.26	4.15	14.53	461	70	10.8	10.8	764	0.28	0.54		
316-C000	06E-	1.42	1 2 2	21 70			0.6	0.5	427	0.70	6.01		
1H-2 1H-5	1.21	1.43	1.32	31./8 23.85	556 514	80 74	0.6	0.5 3.4	437	0.72	6.91 0.64		
2H-3	7.79	8.02	7.91	19.91	554	76	7.1	6.7	646	0.08	0.68		
2H-7	12.09	12.33	12.21	15.10	494	75	12.7	12.5	695	0.80	0.74		
3H-3	17.29	17.52	17.40	13.20	456	77	11.7	11.0	563	4.88	1.30		
3H-7	21.66	21.89	21.77	15.67	484	80	10.9	10.1	595	39.96	3.29		
4H-5 5H-3	29.92	30.16	30.04	12.56	433 ⊿10	/9 83	10.3	9.7	524 468	2.33	4.66		
7H-4	42.92	43.16	43.04	13.42	409	89	12.1	11.3	471	1.93	4.17		
8H-4	51.79	52.03	51.91	14.82	437	89	12.3	10.9	568	8.85	5.24		
9H-5	62.41	62.64	62.53	14.49	413	91	12.4	11.3	538	6.46	7.46		
10H-8	64.51	64.67	64.59	14.65	442	91	12.9	12.2	447	13.27	14.66		
11H-4 12H 6	6/./0 76.21	67.91	6/.81 76.41	13.43	416	93 74	12.7	11.3	490	28.21	7.08		
1211-0 15X-4	81.76	81.97	81.87	10.1	395	79	8.7	9.0	517	0.90	3.18		
16X-2	90.11	90.34	90.23	15.3	314	80	9.7	10.4	447	1.82	5.30		
17X-3	100.30	100.55	100.43	14.0	372	80	11.0	11.6	488	0.95	4.39		
19X-5	119.76	120.08	119.92	13.7	389	81	10.4	10.4	593	4.86	5.22		
20X-7	132.85	133.18	133.01	32.2	246	80	10.9	12.0	335	9.78	4.65		
218-3	127.20	137.70	137.34	13.1	221	74	9.2	10.0	203 417	0.65	3.51		
23X-4	157.74	158.08	157.91	13.6	251	77	9.1	9.9	661	0.55	4.02		
25X-7	180.79	181.13	180.96	28.0	237	85	13.5	14.1	522	1.25	5.02		
26X-4	186.65	186.96	186.80	16.1	238	79	11.9	13.1	701	2.60	5.04		
27X-5	197.49	197.87	197.68	20.2	203	82	12.1	12.1	471	6.65	4.94		
28X-3	203.81	204.17	203.99	15./	1//	81	11.3	12.1	542 636	50.91	8.70		
297-7 30X-3	213.04	219.50	219.21	27.8	183	86	12.7	14.0	661	1.03	5.50		
31X-3	232.32	232.69	232.50	22.2	194	85	12.3	14.0	615	0.21	4.80		
32X-4	243.21	243.59	243.40	22.2	219	85	12.3	13.3	741	0.45	4.46		
34X-5	263.62	264.00	263.81	25.6	185	89	13.0	13.9	572	7.14	5.63		
35X-2	268.69	269.06	268.87	19.2	171	87	12.7	13.5	505	2.32	7.46		
378-5	201.30	201.92	201.74	19.7 21.4	215 180	86	12.5	13.0	633	2.76	0.11 4 19		
38X-2	296.70	296.91	296.80	22.3	204	85	12.6	14.0	717	0.64	4.43		
39X-4	309.69	310.07	309.88	27.9	196	88	13.2	15.2	596	2.06	4.62		
40X-7	322.01	322.41	322.21	23.8	194	91	12.8	13.5	774	0.48	5.48		
41X-4	328.83	329.21	329.02	26.2	141	92	12.6	13.2	763	2.09	4.42		
42X-5	339.58 340 11	339.99	339.78	25.6 31.5	189	95	13.1	16.3 14.4	657 417	12.00	6.12		
43X-5 44X-5	358.99	359.37	359.18	29.2	201	101	13.2	14.4	635	0.75	6.97		
45X-4	366.66	367.05	366.86	31.0	170	102	15.4	15.8	715	0.78	6.68		
46X-5	377.60	377.99	377.80	29.8	147	105	19.0	19.4	385	0.59	3.39		
47X-5	386.72	387.10	386.91	34.3	162	117	24.3	13.4	573	0.60	6.89		
48X-5	396.98	397.40	397.19	38.5	153	114	34./	12.6	443	0.52	5.40		
497-4	404.00	403.09	404.09	54.0	109	110	23.7	0.0	520	0.45	5.49		
316-C000	10F- 105 50	105 01	105 72	<i>A</i> 1 0	194	124	66 C	7 5	560	0.05	0 20		
∠r-∠ 3r-1	403.52	403.91	403.72	41.9	166	124	00.0 93.7	11.3	500 764	0.95	9.20 7.97		
4R-2	424.91	425.27	425.09	55.8	144	113	24.0	2.3	522	0.14	3.97		
5R-1	434.25	434.50	434.37	64.4	166	109	35.4	3.4	651	0.12	5.23		
6R-1	439.08	439.41	439.25	69.6	180	104	31.4	2.3	733	0.22	3.72		
7R-1	448.40	448.66	448.53	80.4	155	119	74.7	10.7	911	0.92	4.03		
8K-1 0p 1	458.03	458.41	458.22	92.7 04 0	164	117	41.8	1.7	982 022	0.15	8.56		
9K-1 10R-1	407.04 477.25	407.43 477.50	407.24 477.37	90.8 102.9	104 167	107 114	11.9 95.0	5.5 77	923 978	5.27 2.45	11.65		
11R-1a	485.50	485.64	485.57	91.6	142	95	24.9	6.9	555	0.13	9.75		
11R-1b	485.88	486.20	486.04	101.7	69	104	31.4	4.2	393	0.00	6.40		
12R-2	496.44	496.84	496.64	111.5	140	107	52.5	2.8	743	0.25	16.78		


Table T13 (continued).

Core.	D	epth CSF (i	m)			١	Minor ele	ments (µ	m)		
section	Тор	Bottom	Average	Li	В	Sr	Ba*	Ba†	Si	Fe	Mn
13R-2	505.90	506.30	506.10	108.6	118	96	27.2	4.2	562	0.11	6.99
14R-2	516.58	517.02	516.80	121.7	118	102	41.6	3.2	459	0.00	8.20
15R-1	523.50	523.90	523.70	117.0	125	106	43.8	2.7	632	0.06	21.44
16R-1	534.00	534.42	534.21	113.5	175	106	14.1	5.6	543	0.21	36.71
17R-1	542.65	543.06	542.86	126.0	123	106	48.1	4.5	533	0.00	16.85
18R-1	553.11	553.50	553.31	129.2	133	108	19	3	698	0.32	18.49
19R-3	565.26	565.67	565.46	123.1	102	104	8	5	166	0	13.31
20R-1	571.18	571.49	571.34	133.0	94	109	17	2	191	0	9.19
22R-1	590.00	590.42	590.21	126.6	167	101	7	2	453	0	17.84

Notes: * = shipboard ICP-AES, \dagger = shore-based ICP-MS. CSF = core depth below seafloor.



Table T14. Uncorrected concentrations of trace elements and δ^{18} O in interstitial waters, Site C0006. (See table notes.) (Continued on next page.)

Core	D	epth CSF (i	m)	V	Cu	Zn	Ph	Mo	C	Ph		v	8 ¹⁸ O
section	Тор	Bottom	Average	(nM)	(nM)	(nM)	(μM)	(μM)	(nM)	(nM)	(nM)	(pM)	(‰)
316-C0006	iC-												
1H-2	1.27	1.48	1.37	_	_	75	1.31	46	_	_	_	_	-0.42
1H-6	5.97	6.19	6.08	—	_	60	1.34	53	_	—	—	_	-0.51
316-C0006	D-												
1H-2	1.21	1.43	1.32	30.4	722.6	311	1.54	31	3.7	0.6	17.6	1.66	-0.02
TH-5	4.04	4.26	4.15	40.3	87.2	119	1.41	28	4.9	0.7	0.5	2.1	-0.35
316-C0006	6E-	1.42	1 2 2	20.0	1241	170	1 70			0.6	25 7	1 00	0.1.0
1H-2 1H-5	1.21	1.43	1.32	29.9	136.1 140.0	179	1.70	84 20	4.4	0.6	25./	1.88	0.19
2H-3	7.79	8.02	7.91	18.1	57.0	78	1.33	29	4.5	0.4	0.7	2.0	-0.20
2H-7	12.09	12.33	12.21	40.4	210.4	202	1.36	32	4.4	0.6	1.5	6.4	-0.51
3H-3	17.29	17.52	17.40	81.4	70.7	125	1.29	121	4.9	7.4	1.3	2.5	-0.88
3H-7	21.66	21.89	21.77	89.5	65.4	121	1.24	366	5.8	1.1	4.9	0.80	-0.95
4H-5	29.92	30.16	30.04	63.1	61./	/3	1.22	149	6.4	0.5	2.9	1./3	-1./6
3⊓-3 7H-4	42.92	43.16	43.04	56.0	1 265 2	233	1.12	126	5.1	0.8	2.9	2.0	-2.02
8H-4	51.79	52.03	51.91	31.9	74.6	144	1.05	29	5.7	1.5	0.7	0.46	-2.30
9H-5	62.41	62.64	62.53	18.6	68.4	215	1.10	88	5.1	0.4	1.1	3.8	-2.60
10H-8	64.51	64.67	64.59	24.6	75.2	132	1.08	185	4.9	0.9	2.7	0.72	-2.52
11H-4	67.70	67.91	67.81	29.4	164.8	341	1.01	139	4.4	1.5	0.9	1.18	-2.85
12H-6 15X-4	76.31 81.76	/6.52 81.97	/6.41 81.87	29.4 47.4	3,220.9	319	1.03	153	5.2	0.9	1.4	2./	-2.68
16X-4	90.11	90.34	90.23	18.5	380.0	260	1.22	54	7.1	0.0	0.9		-2.99
17X-3	100.30	100.55	100.43	36.1	628.3	634	1.09	320	6.6	1.2	2.2	2.6	-2.81
19X-5	119.76	120.08	119.92	30.7	613.9	184	0.88	58	5.8	1.7	1.1	1.06	-3.02
20X-7	132.85	133.18	133.01	16.0	141.3	406		133	8.7	2.2	1.2	1.20	-2.83
21X-3	137.38	137.70	137.54	26.4	6,115.2	565	0.95	124	5.0	9.8	1.1		-3.23
22A-3 23X-4	140.05	147.18	147.00	23.9 42.3	2,207.2	232 606	0.92	89	5.1 4.7	0.5	0.9	2.3 1.37	-3.20 -3.30
25X-7	180.79	181.13	180.96	12.0	7,708.8	242		56	7.6	0.3	1.5	1.04	-3.21
26X-4	186.65	186.96	186.80	12.1	299.3	207	0.96	49	5.3	0.6	0.5	1.84	-3.32
27X-5	197.49	197.87	197.68	11.9	1,473.3	249	0.99	164	4.5	2.1	0.8	0.60	-2.88
28X-3	203.81	204.17	203.99	15.7	366.5	64	0.96	850	4.9	1.6	0.2	0.96	-3.52
29X-7	219.04	219.38	219.21	13.1	1,606.8	4/6	1.02	108	4.4	0.3	1.5	2./	-3.64
30X-3	232.32	223.34	223.55	21.6	4 409 4	182	0.90	496	4.0 5.0	0.2	1.2	1.50	-3.36
32X-4	243.21	243.59	243.40	33.8	8,465.8	1,085	0.84	143	4.2	0.7	1.4	2.0	-3.85
34X-5	263.62	264.00	263.81	6.9	6,049.0	498	0.89	85	5.5	0.3	0.4	0.75	-3.48
35X-2	268.69	269.06	268.87	19.0	2,064.0	662	0.83	260	4.4	0.3	0.8	1.31	-3.41
36X-4	281.56	281.92	281.74	9.4	278.0	104	0.89	87	5.0	0.7	0.5	1.06	-3.63
3/X-3	292.12	292.49	292.30	17.5	223.8	205	0.92	217	5.5	0.1	2./	0.63	-3.70
39X-4	309.69	310.07	309.88	18.5	4.766.2	324	1.07	378	5.6 6.6	0.2	1.2	2.3	-3.70
40X-7	322.01	322.41	322.21	26.3	2,268.1	473	0.78	59	4.1	0.5	0.8	0.55	-3.99
41X-4	328.83	329.21	329.02	19.1	3,660.1	579	0.83	88	3.9	5.4	1.3	0.59	-4.01
42X-5	339.58	339.99	339.78	11.5	266.7	443	0.89	634	5.4	0.2	0.6	0.59	-3.65
43X-5	349.11	349.49	349.30	8.1	2,499.3	265	1.00	841 708	5./	0.7	1.1	0.26	-3.84
447-3 45X-4	366.66	367.05	366.86	8.1	298.8	519	1.01	279	3.0 4.9	0.3	1.0	0.44	-3.39
46X-5	377.60	377.99	377.80	26.7	4,746.4	445	1.00	424	5.1	0.9	2.5	0.97	-4.04
47X-5	386.72	387.10	386.91	7.8	1,848.8	227	0.94	215	5.1	0.4	0.7	1.17	-3.61
48X-5	396.98	397.40	397.19	14.6	324.9	78	0.98	845	5.1	0.3	1.6	1.03	-3.65
49X-4	404.68	405.09	404.89	19.3	1,253.1	555	1.03	635	5.3	16	5.5	0.82	-3.28
316-C0006	δF-												
2R-2	405.52	405.91	405.72	22.1	696.1	322	0.75	125	3.2	0.3	1.2	1.17	-3.42
3K-1 ⊿p ว	414.00	414.39 425 27	414.20	17.8 27 2	1,468.3	345	0.75	210	3.2 ⊿ 1	0.7	1.1 2 4	1.24	_
-+r∠ 5R-1	434.25	434.50	434.37	27.5 29.6	28.901.5	1,136	0.85	123	4.1 3.6	2.2	3.1	0.45 1.17	-3.57
6R-1	439.08	439.41	439.25	37.2	6,070.4	436	0.81	432	3.3	1.8	3.9	0.53	-1.60
7R-1	448.40	448.66	448.53	25.8	18,698.9	1,210	0.66	265	2.5	3.3	3.1	0.43	_
8R-1	458.03	458.41	458.22	12.1	23,097.6	1,294	0.53	48	2.0	0.8	4.2	0.74	_
9R-1	467.04	467.45	467.24	15.2	18,023.9	879	0.64	94	2.5	2.7	3.2	0.86	_
10K-1	4//.25	4/7.50	4/7.37	7.0 19 7	2,208.6	478	0.61	54 107	1.8 2.2	1.3	1.5	0.83	-3.06
11R-1a 11R-1h	403.30 485.88	403.04 486.20	403.37 486.04	10.7	1,259.7	239 93	0.75	691	∠.3 23	2.1	9.Z 5.7	0.30	-5.54
12R-2	496.44	496.84	496.64	10.6	10,622.0	589	0.67	593	2.4	1.8	5.2	0.51	-3.23



Table T14 (continued).

Core.	De	Depth CSF (m)			Cu	Zn	Rb	Мо	Cs	Pb	U	Y	δ ¹⁸ Ο
section	Тор	Bottom	Average	(nM)	(nM)	(nM)	(µM)	(µM)	(nM)	(nM)	(nM)	(pM)	(‰)
13R-2	505.90	506.30	506.10	11.7	10,011.7	431	0.71	330	2.7	1.0	5.1	0.30	-4.19
14R-2	516.58	517.02	516.80	10.6	2,327.5	449	0.60	434	2.4	1.5	1.9	0.92	_
15R-1	523.50	523.90	523.70	4.7	4,813.4	365	0.53	237	2.3	2.4	1.8	1.63	-3.23
16R-1	534.00	534.42	534.21	11.5	10,284.5	280	0.57	145	2.4	0.9	2.4	0.52	-3.25
17R-1	542.65	543.06	542.86	10.9	25,404.6	393	0.49	168	2.0	5.5	2.4	0.43	-3.48
18R-1	553.11	553.50	553.31	8.1	21,107.7	463	0.46	476	2.2	1.6	4.7	0.30	_
19R-3	565.26	565.67	565.46	7.0	11,281.7	204	0.45	727	2.6	2.5	5.1	0.24	_
20R-1	571.18	571.49	571.34	7.3	19,487.9	284	0.50	505	2.7	0.9	3.6	0.41	_
22R-1	590.00	590.42	590.21	7.1	31,892.9	465	0.68	455	3.0	0.8	4.4	0.15	_

Notes: CSF = core depth below seafloor. — = not analyzed.



Table T15. Headspace gas composition for safety monitoring in sediments, Site C0006. (See table notes.)

Core, section.	Depth	Headspace g	Jas (ppmv)	
interval (cm)	CSF (m)	Methane	Ethane	C_1/C_2
316-C0006C-				
1H-1, 119–123	1.21	12,302.3	0.0	_
316-C0006D-				
1H-1, 117–121	1.19	31.7	0.0	_
316-C0006E-				
1H-1, 116.5–120.5	1.19	24.4	0.0	_
2H-1, 136.5–140.5	6.58	29.1	0.0	_
3H-1, 136.5–140.5	16.08	12,246.0	0.0	_
4H-1, 139.5–143.5	25.61	14,685.1	0.0	_
5H-1, 139–143	34.63	8,907.5	0.0	_
7H-1, 136.5–140.5	40.08	5,113.1	0.0	_
8H-1, 135.5–139.5	49.57	14,032.3	0.0	_
9H-1, 136–140	59.09	12,884.1	0.0	_
11H-1, 137–141	66.06	10,654.1	0.0	_
12H-1, 44–48	71.94	7,469.1	2.1	3,517
15X-1, 137–141	80.72	7,606.9	0.0	_
16X-1, 124–128	90.09	7,364.0	0.0	_
17X-1, 137–141	99.72	16,704.7	3.4	4,954
18X-1, 133–137	107.68	5,975.1	2.3	2,654
19X-1, 105–109	116.90	5,779.5	1.9	3,113
20X-1, 137.5–141.5	126.73	6,740.1	2.7	2,458
21X-1, 141–145	136.26	4,579.5	0.0	—
22X-1, 137–141	145.72	11,339.1	2.8	3,983
23X-1, 136.5–140.5	155.22	8,212.8	2.6	3,209
25X-1, 136.5–140.5	174.22	6,219.2	5.3	1,177
26X-1, 145–149	183.80	7,271.5	4.1	1,767
27X-1, 137–141	193.22	9,126.2	4.1	2,239
28X-1, 137–141	202.72	3,199.4	4.1	788
29X-1, 139–143	212.24	5,573.7	3.1	1,809
30X-1, 137–141	221.72	9,382.3	3.7	2,540
31X-1, 140–144	231.25	5,334.5	2.5	2,106
32X-1, 138.5–142.5	240.74	2,522.6	0.0	_
34X-1, 137–141	259.72	14,442.0	5.3	2,705
35X-1, 82–86	268.67	11,395.3	2.9	3,976

Core, section	Depth	Headspace g	as (ppmv)	
interval (cm)	CSF (m)	Methane	Ethane	C_{1}/C_{2}
36X-1, 136.5–140.5	278.72	6,248.9	4.4	1,411
37X-1, 137.5–141.5	288.23	16,875.6	4.8	3,483
39X-1, 137–141	307.22	14,871.2	5.1	2,916
40X-1, 137–141	316.72	9,146.1	4.6	2,007
41X-1, 137.5–141.5	326.23	12,603.1	4.1	3,101
42X-1, 135.5–139.5	335.71	13,216.5	4.4	2,983
43X-1, 137–141	345.22	14,818.3	5.1	2,910
44X-1, 138–142	354.73	13,718.4	5.8	2,374
45X-1, 135.5–139.5	364.21	13,194.5	6.0	2,199
46X-1, 138–142	373.73	11,021.8	4.9	2,264
47X-1, 136–140	383.21	6,373.1	3.7	1,701
48X-1, 137–141	392.72	15,742.5	6.9	2,274
49X-1, 137–141	402.22	5,867.8	4.8	1,232
316-C0006F-				
2R-1, 98–102	405.50	4,976.0	2.5	1,964
4R-1, 136–140	424.89	8,711.0	2.7	3,169
5R-1, 136–140	434.40	8,654.5	2.8	3,089
6R-1, 137–141	439.39	3,772.9	0.0	_
7R-1, 137–141	448.89	7,236.0	2.2	3,280
9R-1, 146–150	467.98	11,497.2	2.7	4,239
11R-1, 146–150	487.00	10,743.3	2.7	3,968
12R-1, 139–143	496.42	8,029.7	2.5	3,248
13R-1, 136–140	505.88	3,496.0	0.0	_
14R-1, 146.5–150.5	515.49	7,471.0	2.9	2,578
15R-1, 146–150	524.98	4,585.3	2.4	1,884
16R-1, 137–141	534.39	11,021.8	5.6	1,980
17R-1, 133.5–137.5	543.86	4,013.9	2.5	1,624
18R-1, 135–139	553.37	10,666.8	5.7	1,879
19R-1, 136–140	562.88	2,456.1	1.9	1,261
20R-1, 137–141	572.39	3,755.5	2.5	1,525
22R-1, 41.5–45.5	591.40	2,614.3	2.0	1,334

Notes: CSF = core depth below seafloor. — = not applicable.



 Table T16. Hydrocarbon gas concentration from additional headspace gas analysis, Site C0006. (See table notes.) (Continued on next page.)

		Headspace	nas (nnmv)		Headspace gas (µM)		
Core, section, interval (cm)	Depth CSF (m)	Methane	Ethane	C_1/C_2	Methane	Ethane	
				-17 -2			
316-C0006C-	1 10	21 007 5	0.0		5 061	0.00	
1H-1, 119–123 1H-5, 145–149	5.91	21,907.5	0.0	_	5 260	0.00	
	5.71	11,000.1	0.0		5,200	0.00	
316-C0006D- 1H-1 117_121	1 1 7	523	0.0	_	11.0	0.00	
1H-4, 116,5–120,5	4.00	21.288.0	0.0	_	5.173	0.00	
216 C0006E		,					
1H-1, 116,5–120,5	1.19	29.7	0.0	_	5.7	0.00	
1H-4, 137–141	4.22	106.1	0.0	_	24.7	0.00	
2H-2, 115.5–119.5	7.77	202.1	0.0	_	45.1	0.00	
2H-6, 117–121	12.07	23,883.0	0.0	—	5,455	0.00	
2H-8, 143.5–147.5	13.78	22,839.9	0.0		6,435	0.00	
3H-2, 115-119 3H-6, 118 5-122 5	21 64	10,939.5	0.0	_	6,075 3,832	0.00	
3H-9, 147–151	24.79	4.745.0	0.0	_	2.139	0.00	
4H-4, 144–148	29.90	7,343.8	0.0	_	2,029	0.00	
4H-6, 132.5–136.5	31.50	12,054.6	0.0		3,094	0.00	
5H-4, 140.5–144.5	37.48	7,499.7	0.0		2,264	0.00	
5H-2, 115–119	35.82	17,520.6	0.0		4,285	0.00	
/H-1, 136.5–140.5 7H-3 137 141	40.08	24,332.3 10 073 1	0.0		6,001 5,704	0.00	
8H-1 135 5-139 5	42.90	14 912 1	0.0	_	3,704 4 499	0.00	
8H-3, 74–78	51.77	13,847.4	0.0		4,010	0.00	
9H-3, 0–4	60.51	8,220.7	0.0		2,933	0.00	
9H-4, 129–133	62.38	11,637.2	0.0		3,057	0.00	
10H-4, 0–4	64.53	10,320.9	0.0	—	3,711	0.00	
11H-3, 72.4–76.4	67.68	17,734.9	0.0		4,579	0.00	
11H-6, 137.5-141.5	70.30	16,/69.0	0.0		4,641	0.00	
12H-5, 137-141	76.29	21 160 0	2.7	7 91 3	5,127 7 554	0.00	
15X-1, 137–141	80.72	14.472.0	0.0		4.835	0.00	
15X-6, 137–141	83.36	27,384.3	6.3	4,340	8,433	1.94	
16X-1, 124–128	90.09	21,578.3	2.6	8,153	6,370	0.78	
17X-2, 52–56	100.28	27,237.1	4.2	6,457	10,934	1.69	
18X-1, 133–137	107.68	17,538.6	3.4	5,091	5,806	1.14	
19X-1, 105-109	116.90	12,035./	2.6	4,639	3,83/	0.83	
20X-3, 28.3-52.5	120.00	17,377.3	2.0	3 873	3 308	0.76	
20X-6, 39–43	132.83	16.051.8	2.6	6.179	5,009	0.81	
21X-2, 106–110	137.36	7,399.8	2.3	3,282	3,156	0.96	
22X-2, 105–109	146.81	4,260.0	0.0	_	2,225	0.00	
22X-5, 137–141	149.98	6,549.7	3.0	2,211	2,255	1.02	
23X-3, 105.5–109.5	157.72	10,014.7	2.2	4,546	3,100	0.68	
23X-5, 137-141	159.4/	12,251.1	1.9	6,535	5,362	0.82	
247-1, 0-3 25X-4 136 7-140 7	178 44	4,095.0 9 846 7	2.5	4 030	3 941	0.98	
25X-6, 88–92	180.77	9,902.0	4.1	2,440	3,285	1.35	
26X-5, 0–4	186.98	16,277.1	4.1	3,987	6,373	1.60	
26X-7, 137.5–141.5	190.86	9,498.2	3.1	3,025	4,688	1.55	
27X-2, 137.5–141.5	194.64	12,639.8	3.0	4,262	4,171	0.98	
27X-4, 137–141	197.47	8,246.1	4.7	1,759	3,366	1.91	
20X-2, 102.5-106.5 20X-3 137 111	203.79	8,026./ 5 622 7	3.9 2 1	2,0/3	2,038 2,386	1.27	
29X-6, 105–109	219.00	9,924.8	∠.1 3.9	2,095	2,300	1.39	
30X-2, 137.5–141.5	223.14	4,561.7	0.0		2,894	0.00	
30X-5, 137–141	225.97	9,971.6	3.6	2,755	3,948	1.43	
31X-2, 101–105	232.30	11,540.2	4.4	2,597	4,107	1.58	
32X-6, 137–141	246.40	4,251.5	2.1	2,045	3,276	1.60	
34X-2, 137–141	261.13	10,089.7	3.8	2,671	2,415	0.90	
34X-4, 100.5-104.4	263.59	9,346./ 7027 2	4.6 2 Q	2,045	2,006 2 211	0.98	
35X-1, 82-86	203.39	13,539.7	3.0 3.6	3,745	4,598	1.21	
35X-3, 136.5–140.5	270.44	6,425.6	3.9	1,631	3,489	2.14	
36X-3, 137–141	281.54	14,284.5	5.3	2,693	5,149	1.91	
36X-6, 138–142	284.36	7,907.9	4.0	1,979	4,709	2.38	
37X-4, 101–105	292.10	13,934.6	5.0	2,811	6,065	2.16	



Table T16 (continued).

Core. section	Depth Headspace gas (ppmv)				Headspace	gas (µM)
interval (cm)	CSF (m)	Methane	Ethane	C_1/C_2	Methane	Ethane
39X-3, 99.5–103.5	309.67	16,369.8	3.6	4,576	12,611	2.76
39X-6, 137–141	312.87	7,292.3	3.5	2,065	2,596	1.26
40X-4, 98.5–102.5	320.57	8,756.7	4.7	1,861	4,376	2.35
40X-6, 98–102	321.99	9,787.3	4.2	2,310	4,476	1.94
40X-8, 131–135	323.74	4,617.2	3.8	1,217	1,776	1.46
41X-3, 113.5–117.5	328.81	9,981.8	4.1	2,411	3,548	1.47
41X-5, 122.3–126.3	330.45	14,518.2	5.0	2,920	4,005	1.37
42X-2, 138–142	337.13	17,148.4	5.9	2,902	4,109	1.42
42X-4, 98.5–102.5	339.56	8,541.3	3.9	2,174	2,033	1.05
42X-7, 137–141	342.77	9,216.8	4.3	2,127	2,617	1.38
43X-1, 137–141	345.22	8,328.1	4.0	2,088	2,753	1.47
43X-4, 100.5–104.5	349.09	6,717.5	3.7	1,797	1,682	1.04
44X-2, 137.5–141.5	356.15	8,110.9	2.7	2,950	3,376	1.27
44X-4, 137.5–141.5	358.97	10,146.4	3.9	2,573	3,961	1.71
45X-3, 99–103	366.64	9,002.4	4.6	1,945	3,276	1.87
45X-7, 138–142	371.28	10,490.3	5.4	1,946	3,480	1.99
46X-2, 137.5–141.5	375.15	19,443.5	7.4	2,616	4,862	2.08
46X-4, 99–103	377.58	5,472.2	4.0	1,379	1,680	1.36
47X-5, 34–38	387.08	9,345.1	3.8	2,470	3,784	1.70
47X-8, 137.5–141.5	390.30	5,263.2	2.8	1,877	1,299	0.78
48X-4, 136.5–140.5	396.96	7,693.9	3.9	1,993	3,386	1.88
49X-3, 99–103	404.66	9,805.1	5.3	1,838	1,890	1.17
49X-6, 59.5–63.5	406.72	7,848.9	4.0	1,976	2,240	1.27
316-C0006F-						
2R-1, 98–102	405.50	6,563.5	3.8	1,736	2,658	1.53
4R-1, 136–140	426.29	8,363.1	2.9	2,854	3,164	1.11
5R-1, 136–140	434.38	6,721.3	2.6	2,539	3,890	1.53
6R-1, 137–141	439.39	4,402.6	0.0	—	1,867	0.00
7R-1, 137–141	448.89	9,475.0	2.9	3,217	2,282	0.71
8R-1, 137–141	458.39	9,287.2	2.9	3,216	2,159	0.67
9R-1, 146–150	467.98	4,317.3	1.7	2,510	1,172	0.47
11R-1, 146–150	486.98	10,397.0	2.7	3,904	3,538	0.91
12R-1, 139–143	496.41	12,133.7	3.5	3,503	3,575	1.02
13R-1, 136–140	505.88	3,933.7	0.0		2,326	0.00
14R-1, 146.5–150.5	515.49	3,676.0	3.6	1,008	2,194	2.18
15R-1, 146–150	524.98	8,299.7	7.8	1,058	2,492	2.35
15R-2, 99–103	526.01	6,897.3	4.1	1,672	1,640	0.98
16R-1, 137–141	534.39	9,614.0	6.2	1,546	2,207	1.43
17R-1, 133.5–137.5	543.86	5,512.5	4.3	1,283	1,500	1.17
18R-1, 135–139	553.37	10,094.8	5.4	1,877	3,918	2.09
19R-1, 136–140	562.88	5,680.1	4.7	1,221	1,610	1.32
20R-1, 137–141	572.39	6,602.8	4.5	1,463	1,844	1.26
21R-CC, 0–5	580.53	8,323.7	5.2	1,599	2,393	1.50
22R-2, 38–42	591.82	6,648.5	4.0	1,666	1,364	0.82

Notes: CSF = core depth below seafloor. — = not applicable.



Table T17. Carbonate, carbon, nitrogen, and sulfur in sediments, Site C0006. (See table notes.) (Continued on next page.)

Core, section, interval (cm)	Depth CSF (m)	CaCO ₃ (wt%)	TOC (wt%)	TN (wt%)	C/N	TS (wt%)		Core, section, interval (cm)	Depth CSF (m)	CaCO ₃ (wt%)	TOC (wt%)	TN (wt%)	C/N	TS (wt%)
316-C0006C-							-	25X-6, 25–26.5	180.12	1.88	0.35	0.05	7.68	0.15
1H-2, 0–1.5	1.27	5.83	0.41	0.05	7.67	0.37		25X-7, 0–1.5	180.79	0.76	0.22	0.03	7.51	0.15
1H-6, 0–1.5	5.98	2.34	0.35	0.05	7.70	0.43		26X-1, 147.5–149	183.81	1.86	0.53	0.06	9.60	0.18
316-C0006D-								26X-4, 0-1.5	186.65	2.19	0.41	0.06	7.16	0.08
1H-2, 0–1.5	1.22	2.59	0.19	0.04	4.92	0.67		267-8, 94.5-96	191.83	1.65	0.35	0.05	7.59	0.86
1H-2, 20–21.5	1.42	2.06	0.40	0.04	9.97	0.81		27X-1, 00-01.5	192.44	0.90	0.39	0.00	7.02	0.13
1H-5, 0–1.5	4.05	4.24	0.49	0.05	8.94	0.34		27X-8, 30–31.5	200.62	0.74	0.16	0.03	4.95	0.11
316-C0006E-								28X-1, 31-32.5	201.65	2.43	0.39	0.06	6.74	0.11
1H-2, 0–1.5	1.21	1.07	0.52	0.05	10.57	0.66		28X-1, 91–92.5	202.25	1.76	0.33	0.05	7.29	0.10
1H-4, 69.5–71	3.53	1.01	0.43	0.04	9.67	0.68		28X-3, 0–1.5	203.81	0.84	0.30	0.04	7.39	0.18
1H-5, 0–1.5	4.25	0.32	0.21	0.03	7.65	0.47		28X-4, 75–76.5	204.92	1.09	0.30	0.04	7.48	0.10
1H-6, 49.5–51	4.97	4.64	0.62	0.05	11.69	0.53		29X-2, 84.5–86	213.11	2.72	0.48	0.05	8.90	0.10
2H-3, 0-1.5	7.80	2.50	0.50	0.05	10.42	0.50		29X-7, 0–1.5	219.05	2.17	0.51	0.06	8.45	0.14
2H-4, 113.3-117 2H-7 0 1 5	9.10	5.06	0.30	0.03	8 98	0.34		30X-1, 107-108.5	221.41	1.51	0.42	0.06	6.22	0.16
3H-3 0-1 5	17 29	0.72	0.45	0.03	9.52	1 75		30X-3, 0-1.3	223.10	2.50	0.41	0.07	7 23	0.03
3H-6, 55–56.5	20.99	2.65	0.33	0.05	6.70	0.06		31X-3, 0-1, 5	232.33	1.24	0.10	0.00	3.82	0.05
3H-6, 95–96.5	21.39	6.15	0.62	0.06	11.01	0.14		31X-4, 65–66.5	233.34	1.79	0.39	0.05	7.36	0.28
3H-7, 0–1.5	21.66	0.16	0.28	0.03	9.07	0.58		32X-4, 0–1.5	243.22	3.09	0.71	0.07	9.53	0.26
4H-4, 29.5–31	28.74	1.86	0.49	0.04	10.96	0.12		32X-5, 23–24.5	243.83	1.27	0.44	0.07	6.61	0.15
4H-5, 0–1.5	29.93	1.35	0.34	0.04	8.32	0.11		32X-5, 91.5–93	244.51	0.92	0.40	0.05	7.47	0.20
5H-1, 126.5–128	34.49	0.92	0.44	0.06	7.40	0.09		32X-6, 18.5–20	245.20	2.17	0.50	0.05	9.09	0.21
5H-3, 0–1.5	35.85	0.78	0.25	0.03	9.67	0.12		34X-3, 94–95.5	262.10	1.68	0.39	0.05	7.24	0.15
5H-4, 20–21.5	36.26	1.00	0.25	0.03	7.40	0.19		34X-4, 44–45.5	263.02	2.56	0.44	0.05	8.77	0.16
5H-5, /0-/1.5	38.21	0.63	0.19	0.02	9.69	0.12		34X-5, 0–1.5	263.62	1.79	0.40	0.05	7.61	0.08
7H-2, 113.3-117	41.20	0.79	0.22	0.03	5 51	0.10		35X-2, U-1.5	268.70	2.06	0.17	0.03	5.19	0.13
7H-4 20 5-22	43.13	0.05	0.15	0.02	7.81	0.07		358-3, 110-115	270.24	2.24	0.39	0.04	9.1Z 7.70	0.08
8H-1, 55–56.5	48.75	3.84	0.45	0.05	8.73	0.06		36X-1 100-101 5	278.34	2.24	0.32	0.05	8 70	0.07
8H-2, 86.5-88	50.46	0.74	0.12	0.02	5.38	0.09		36X-4, 0–1.5	281.56	2.22	0.55	0.07	8.05	0.16
8H-4, 0–1.5	51.80	1.76	0.39	0.04	9.98	0.12		37X-2, 78.5-80	289.04	2.94	0.54	0.07	8.17	0.08
9H-2, 93–94.5	60.04	1.21	0.35	0.05	7.68	0.08		37X-4, 18.5–20	291.26	2.01	0.47	0.05	9.51	0.19
9H-5, 0–1.5	62.42	0.90	0.25	0.03	8.54	0.14		37X-4, 58–59.5	291.65	0.52	0.48	0.07	7.18	0.07
10H-8, 0–1.5	64.52	0.84	0.26	0.03	8.99	0.40		37X-5, 0–1.5	292.12	1.68	0.40	0.05	8.63	0.15
11H-1, 79–81	65.4/	0.64	0.34	0.05	6.84	0.07		38X-2, 0–1.5	296.70	0.43	0.30	0.04	6.84	0.10
11H-4, 0-1.5	0/./I 76.21	0.93	0.23	0.03	7.49 8.01	0.22		39X-3, /1-/2.5	309.37	0.94	0.37	0.06	6.60	0.08
15X-4 0-1 5	81 77	1 01	0.42	0.03	6.97	0.20		397-4, 0-1.5 308-CC 31 33	315.67	2.75	0.55	0.05	8 73	0.10
16X-1, 96.5–98	89.80	0.77	0.25	0.03	8.00	0.20		40X-7 0-1 5	372.02	1.58	0.43	0.05	7.88	0.22
16X-2, 0–1.5	90.12	1.20	0.34	0.04	7.91	0.15		40X-8, 60-61.5	323.02	2.57	0.14	0.05	3.02	0.18
17X-1, 115.5–117	99.49	0.43	0.31	0.05	6.66	0.07		41X-4, 0–1.5	328.83	1.12	0.82	0.07	12.09	0.11
17X-3, 0–1.5	100.31	0.66	0.33	0.03	9.88	0.16		42X-5, 0–1.5	339.58	5.02	0.36	0.05	7.41	0.14
17X-5, 27.5–29	101.46	2.67	0.86	0.05	16.85	0.31		42X-8, 56.5–58	343.36	4.69	0.35	0.05	6.46	0.13
19X-3, 113.5–115	118.40	0.94	0.47	0.04	10.87	0.30		43X-5, 0–1.5	349.12	2.55	0.41	0.05	8.27	0.11
19X-4, 95.5–97	119.63	0.29	0.41	0.05	/.81	0.11		44X-5, 0–1.5	359.00	1.75	0.44	0.05	8.22	0.10
197-3, 0-1.3	170.70	2.40	0.30	0.06	0.02	0.13		45X-1, 37.5-39	303.21	2.27	0.51	0.05	10.23	0.15
20X-1 38 5-40	125.70	0.95	0.71	0.00	8 4 5	0.10		43A-3, 03.3-03 45X-3 81 5 83	366.45	5.55 1 1 0	0.05	0.00	7.03	0.20
20X-1, 118.5–120	126.52	0.40	0.36	0.05	7.63	0.08		45X-4, 0-1.5	366.67	2.27	0.47	0.05	8.47	0.14
20X-2, 121.5–123	127.97	1.63	0.58	0.07	8.38	0.13		45X-7, 30–31	370.18	1.24	3.80	0.10	38.08	1.80
20X-3, 0-1.5	128.17	1.85	0.53	0.07	7.88	0.24		45X-7, 79–80	370.67	1.45	6.87	0.15	46.14	2.66
20X-5, 33.5–35	131.35	2.66	0.50	0.07	7.59	0.11		45X-7, 117–118	371.05	1.20	3.91	0.10	37.31	2.32
20X-5, 108–109.5	132.09	2.21	0.42	0.05	7.79	0.17		46X-3, 138–140	376.56	1.74	0.37	0.04	8.18	0.18
20X-7, 0–1.5	132.85	1.29	0.14	0.03	4.86	0.09		46X-5, 0–1.5	377.61	1.25	0.27	0.04	6.28	0.18
21X-3, 0-1.5	137.39	1.69	0.38	0.05	8.4/	0.16		47X-3, 93–94.5	385.58	4.39	0.41	0.05	8.25	0.10
22X-2, 33-34.3	146.08	2.17	0.38	0.05	7.81	0.15		4/X-4, 14.5–16	386.21	6.48	0.37	0.06	6./1	0.09
22X-3, 0-1.3	140.04	2.37	0.39	0.03	8.87	0.12		47 A-3, 0-1.3	206.72 206.00	2.15	0.33	0.05	0.33 6.76	0.10
22X-4, 30-31.3	148.33	1.36	0.39	0.07	9.42	0.16		467-3, 0-1.3	390.99 404 69	0.98	0.27	0.04	6.70	0.08
22X-4, 115-110.5	150.20	1.55	0.34	0.04	9.25	0.15		497-4, 0-1.5	404.09	0.98	0.50	0.04	0.99	0.21
22X-6, 66–67.5	150.66	0.99	0.33	0.04	8.76	0.11		316-C0006F-				o c -		
23X-1, 65–66.5	154.49	3.21	0.49	0.06	7.85	0.11		ZR-2, 0-1.5	405.53	2.10	0.33	0.05	6.36	0.06
23X-1, 101–102.5	154.85	1.55	0.30	0.04	7.93	0.10		3K-1, U-1.5	414.01	2.21	0.33	0.06	5.68 5.17	0.04
23X-3, 26–27.5	156.91	0.99	0.24	0.04	6.57	0.14		5R-1 117_118 5	434 18	2.40 1 04	0.30	0.00	7.60	0.40
23X-3, 67–68.5	157.32	1.97	0.43	0.06	7.12	0.06		6R-1, 120–121.5	439.21	5,80	0.31	0.05	5,99	0.07
23X-4, 0–1.5	157.75	2.89	0.47	0.06	7.59	0.11		7R-1, 90–91.5	448.41	7.87	0.25	0.04	5.69	0.10
238-5, 90–91.5	158.98	1.75	0.35	0.05	7.57	0.08		,						-



Expedition 316 Site C0006

Table T17 (continued).

Core, section, interval (cm)	Depth CSF (m)	CaCO ₃ (wt%)	TOC (wt%)	TN (wt%)	C/N	TS (wt%)
8R-1, 12.5–14	457.13	0.33	0.44	0.07	6.55	0.15
8R-1, 103–104.5	458.04	0.27	0.44	0.07	6.39	0.24
8R-2, 42.5–44	458.84	5.16	0.37	0.06	6.12	0.16
9R-1, 53.5–55	467.04	0.30	0.43	0.07	6.62	0.17
9R-1, 105.5–106	467.56	3.45	0.38	0.06	6.12	0.21
9R-2, 41.5–43	468.42	1.41	0.45	0.07	6.48	0.22
10R-1, 27.5–29	476.28	0.42	0.49	0.07	7.23	0.21
10R-1, 124.5–126	477.25	0.45	0.32	0.06	5.16	0.14
11R-1, 60-61.5	486.11	1.02	0.37	0.06	5.77	0.19
11R-2, 46–47.5	487.49	1.24	0.47	0.07	6.70	0.10
11R-CC, 19.5–21	488.01	2.82	0.40	0.06	6.35	0.27
12R-1, 62.5–64	495.63	0.37	0.46	0.07	6.17	0.36
12R-2, 0–1.5	496.44	0.31	0.47	0.08	6.10	0.34
13R-1, 119–120.5	505.70	1.75	0.31	0.06	5.12	0.35
13R-2, 20–21.5	506.11	0.87	0.33	0.07	5.01	0.77
13R-2, 86–87.5	506.77	1.82	0.33	0.07	5.09	0.52
14R-1, 104–105.5	515.05	1.84	0.30	0.06	5.32	0.56
14R-2, 0–1.5	515.51	0.60	0.30	0.06	5.13	0.20
14R-2, 37–38.5	515.88	1.22	0.32	0.06	5.08	0.36
14R-3, 22.5–24	517.25	1.45	0.28	0.06	4.98	0.51
14R-CC, 13–17	518.37	1.26	0.42	0.07	5.95	0.45
15R-1, 0–1.5	523.51	1.19	0.34	0.06	5.99	0.55
15R-1, 121–122.5	524.72	1.98	0.37	0.07	5.58	0.40
15R-2, 57–58.5	525.58	0.97	0.36	0.07	5.45	0.61
16R-1, 100–101.5	534.01	2.17	0.37	0.08	4.86	0.31
17R-1, 15–16.5	542.66	3.01	0.30	0.06	5.02	0.20
18R-1, 113–114.5	553.14	2.84	0.33	0.06	5.04	0.48
19R-1, 122.5–124	562.73	2.06	0.37	0.07	5.49	0.63
19R-2, 78.5–80	563.69	1.28	0.35	0.07	5.07	0.27
19R-3, 0–1.5	564.32	2.33	0.37	0.07	5.20	0.60
19R-3, 43.5–45	564.75	3.08	0.42	0.07	5.77	0.21
19R-CC, 13.5–15	567.85	1.37	0.34	0.06	5.50	0.59
20R-1, 0-1.5	571.01	4.53	0.39	0.07	5.58	0.16
22R-1, 0–1.5	590.01	14.23	0.19	0.06	3.40	0.05
23R-1, 49-50.5	594.00	4.31	0.30	0.06	5.01	0.18

Notes: CSF = core depth below seafloor. TOC = total organic carbon, TN = total nitrogen, TS = total sulfur.



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Table T18. Sample depth and processing for microbiological and biogeochemical studies, Site C0006. (See table notes.) (Continued on next page.)

Core	Depth	Fro	zen	Anaerobic	Slurry	/ (–20°C)	Core.	Depth	Fro	zen	Anaerobic	Slurry	√ (−20°C)
section	CSF (m)	–80°C	–20°C	pack (4°C)	FISH	Acetone	section	CSF (m)	-80°C	–20°C	pack (4°C)	FISH	Acetone
316-C00	06C-						25X-4	177.15	Х			Х	х
1H-1	0.57	х			Х	Х	25X-4	177.30	х			Х	х
1H-1	0.71			х			25X-4	177.46			Х		
1H-1	0.75	Х		х	Х		25X-4	177.53	Х		Х	Х	
1H-1	0.92	Х					25X-4	177.57	Х				
1H-1	0.99		v	Х			25X-/	181.11	X			X	v
1 III-1 1 III-5	1.15	Y	^		v	Y	278-4	193.33	^		Y	^	~
1H-5	4 69	~		x	~	A	27X-4	193.70	x		x	x	
1H-5	4.83	х		x	х		27X-4	193.28	x		X	~	
1H-5	4.90	X					27X-4	197.48	X			х	
1H-5	4.97			х			27X-5	197.68	Х				
1H-5	5.02		Х				27X-5	197.78	Х	Х		Х	Х
316-000	06D-						28X-2	203.80	Х			Х	
1H-1	0.80	х			х	х	29X-6	219.03	Х			Х	
1H-1	0.94	~		х	~	~	30X-5	225.98	Х			Х	
1H-1	1.08	х		х	х		31X-2	232.31	X			X	
1H-1	1.15	Х					32X-6	246.41	X			X	v
1H-1	1.19		Х				34X-/	265.88	Χ.		v	X	X
1H-4	3.64	Х			Х	Х	34X-7	266.19	x		x	x	
1H-4	3.77			х			34X-7	266.26	x		Х	~	
1H-4	3.84	Х		Х	Х		34X-7	266.30	~	х			
1H-4	3.98	Х	v				35X-3	270.45	х			Х	
1H-4 1⊔ 0	4.03		X				36X-3	281.55	Х			Х	
1H-9 1H-0	8.50 8.64	x	^		x	x	37X-4	292.11	Х			Х	
1H-9	8 80	~		x	~	A	39X-6	311.58	Х			Х	Х
	0.00			~			39X-6	311.73			Х		
316-C00	06E-			N/		v	39X-6	311.88	Х		Х	Х	
1H-1	0.00			X	X	X	39X-6	311.95	Х				
1 III - 3	2.10	Y		~			398-6	312.00	v	X		v	
1H-3	2.20	x		x	x		40A-4 41X 5	320.38	Ŷ			Ŷ	
1H-3	2.40	~		x	~		418-3	330.40	×			×	
1H-3	2.73	х		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	х	х	43X-4	349.10	x			x	
2H-6	10.98	X			X	X	44X-7	360.52	x			x	х
2H-6	11.13			х			44X-7	360.67			х		
2H-6	11.33	Х		х	Х		44X-7	360.82	Х		х	Х	
2H-6	11.43	Х					44X-7	360.89	Х				
2H-6	11.47		Х				44X-7	360.94		Х			
3H-5	19.07	Х			Х	Х	45X-3	366.65	Х			Х	
3H-5	19.22	v		X	v		46X-4	377.59	X			X	
3H-3	19.37	X		Χ.	~		4/X-5	387.09	X			X	
3H-5	19.44	^	x				488-4	396.97	×			×	v
3H-5	19.93		~	х			497-2	403.33	~		x	~	~
5H-2	35.37	х		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~			49X-3	404.67	х		X	х	
5H-2	35.51	Х		х	х		21.6 600	0.45	~			~	
5H-2	35.59			Х			316-C00	100F-				v	
5H-2	35.74	Х			Х	Х	∠K-I כים כ	405.51 405.59	×			A V	v
7H-7	46.38	Х			Х	Х	2R-2 3R-2	403.38	x			^ X	^ X
7H-7	46.53			Х			3R-2	414 71	~		х	~	~
7H-7	46.69	X		Х	Х		4R-1	423.51			~	Х	
7H-7	46.77	Х	v				5R-1	434.32				X	
/H-/ 이니 스	40.81	v	X				6R-2	439.69				Х	
911-0 011 6	62.59	×		v	v		7R-1	447.84	Х				
9H-6	63.59	~		x	Λ		7R-1	447.89			Х		
9H-6	63.84	х		~	х	х	7R-1	447.95	Х			Х	Х
9H-6	63.96	~	х		~	~	7R-1	447.95		Х	Х	Х	
12H-5	76.06			Х			7R-1	448.53	.,	Х		••	
12H-5	76.21	х			Х	Х	8R-1	458.22	X	v		X	X
17X-2	99.84	Х			Х	Х	9K-1	40/.24	X	X		X	Х
17X-2	99.99			Х			10K-2	4/0.00 18752	^			A V	
17X-2	100.16	Х		Х	Х		12R-1	495 73			х	Λ	
17X-2	100.24	Х					12R-1	495.80		х	x	х	
17X-2	100.28		х				12R-1	495.80	х			X	х



Table T18 (continued).

Core.	Depth	Fro	zen	Anaerobic	Slurry	/ (–20°C)
section	CSF (m)	–80°C	–20°C	pack (4°C)	FISH	Acetone
12R-1	495.87	Х				
12R-2	496.64		Х			
13R-2	506.11				Х	
14R-2	516.80				Х	
15R-1	523.71	Х	Х		Х	
16R-1	534.21	Х			Х	Х
17R-1	542.78	Х			Х	Х
17R-2	544.30			х	Х	Х
18R-1	553.30				Х	
19R-3	565.47				Х	
20R-1	571.34				Х	
22R-1	590.45	Х			Х	Х
22R-1	590.50		Х	Х	Х	
22R-1	590.54			Х		
22R-1	590.59	Х				

Notes: Sample depths of Holes C0006C and C00006D indicate the length from the top of Core 1, not from the seafloor. CSF = core depth below seafloor. FISH = fluorescence in situ hybridization.



Table T19. Thermal conductivity measurements, Site C0006. (See table notes.) (Continued on next two pages.)

Tł			Thermal co	nductivity		Standard	Thermal
Core, section,	Depth	N 4 - 4	(W/[n	n·K])		deviation	conductivity
interval (cm)	CSF (m)	Method	Raw average	Calibrated	N	(w/[m⋅ĸ])	(vv/[m·K])*
316-C0006C-							
01H-1, 20	0.20	V10305	0.99	0.94	3	0.00	0.96
01H-3, 45	1.93	V10305	1.07	1.02	3	0.02	1.05
01H-5, 40	4.86	V10305	1.15	1.11	3	0.06	1.13
01H-7, 40	6.59	V10305	1.22	1.18	2	0.01	1.21
01H-9, 43	9.40	V10305	1.05	1.00	2	0.06	1.03
316-C0006D-							
01H-1, 40	0.40	V10305	1.10	1.05	3	0.00	1.08
01H-3, 60	2.03	V10305	1.35	1.31	3	0.01	1.35
0111-0,70	4.90	V10305	1.20	1.24	2	0.04	1.27
01H-10_60	9 97	V10305	1.23	1.15	3	0.01	1.21
21.6 6000.65					5	0.02	
01LL 1 50	0.50	V10205	1.04	1 00	2	0.00	1.02
01H-1, 30	2.03	V10303	1.04	1.00	2	0.00	1.02
01H-6 48	4 95	V10305	1.30	1.20	3	0.01	1.22
02H-2, 100	7.60	V10305	1.35	1.31	3	0.00	1.34
02H-4, 80	8.82	V10305	1.15	1.11	3	0.01	1.14
02H-6, 35	11.23	V10305	0.99	0.94	2	0.00	0.96
02H-8, 60	12.93	V10305	1.27	1.23	3	0.03	1.26
03H-2, 50	16.60	V10305	1.24	1.20	3	0.01	1.23
03H-4, 55	18.07	V10305	1.33	1.29	3	0.04	1.32
03H-6, 83	21.26	V10305	1.14	1.10	3	0.01	1.12
03H-8, 65	22.54	V10305	1.35	1.31	3	0.01	1.34
0411-1, 71	24.90	V10305	1.02	1.08	2	0.03	1.00
04H-6, 60	30.76	V10305	0.74	0.69	3	0.01	0.70
04H-6, 100	31.16	V10305	1.12	1.08	3	0.02	1.10
05H-1, 100	34.22	V10305	1.03	0.99	3	0.01	1.01
05H-1, 125	34.47	V10305	1.22	1.18	3	0.04	1.21
05H-4, 70	36.76	V10305	1.09	1.05	3	0.01	1.07
07H-1, 20	38.89	V10305	0.83	0.79	3	0.00	0.81
07H-5, 90	44.06	V10305	1.10	1.06	4	0.01	1.08
07H-7,20	40.18	V10305	0.92	0.87	3	0.01	0.89
08H-1 90	49.09	V10305	0.96	0.91	5	0.04	0.93
08H-3, 60	51.61	V10305	1.21	1.17	3	0.02	1.20
08H-5, 50	52.53	V10305	1.16	1.11	3	0.01	1.14
08H-8, 30	56.58	V10305	1.01	0.96	3	0.00	0.99
08H-9, 30	57.99	V10305	0.91	0.87	3	0.05	0.89
09H-1, 30	57.99	V10305	0.78	0.73	3	0.01	0.75
09H-2, 80	59.91	V10305	0.96	0.92	3	0.03	0.94
13H-1 60	00.01 78.42	V10305	1.51	1.27	2	0.04	1.50
15X-1.68	80.01	V10305	1.14	1.17	4	0.04	1.13
15X-3, 15	81.20	V10305	1.05	1.01	2	0.00	1.03
15X-5, 43	82.40	V10305	1.21	1.17	3	0.00	1.20
15X-7, 19	84.62	V10305	1.21	1.17	3	0.00	1.19
16X-1, 25	89.08	V10305	0.96	0.91	3	0.01	0.93
16X-3, 20	90.54	V10305	1.10	1.06	4	0.02	1.08
17X-1, 30	98.63	V10305	0.91	0.86	3	0.00	0.88
17X-4, 30	101.03	V10303	1.25	1.19	4	0.01	1.22
17X-3, 20 18X-1, 80	107.13	V10305	1.19	1.15	3	0.00	1.13
19X-1, 65	116.48	V10305	1.20	1.16	3	0.00	1.19
19X-3, 80	118.06	V10305	1.17	1.13	3	0.03	1.16
19X-3, 120	118.46	V10305	1.12	1.08	3	0.00	1.10
19X-4, 90	119.57	V10305	1.06	1.02	3	0.00	1.04
19X-6, 25	120.33	V10305	1.13	1.09	3	0.00	1.11
20X-1, 110	126.43	V10305	1.29	1.25	3	0.01	1.28
20X-3, 100	129.16	V10305	1.09	1.05	2	0.00	1.07
201-3, 13 211-1 80	131./0	V10305	1.23	1.19	3 2	0.02	1.22
217-1, 00 21X-2 80	137.08	V10303	1.23	1.21	כ ר	0.01	1.24
21X-4.80	138.50	V10305	1.12	1.08	3	0.00	1.10
22X-1, 105	145.38	V10305	1.27	1.23	3	0.01	1.25
22X-2, 80	146.54	V10305	1.24	1.20	3	0.00	1.22



Table T19 (continued). (Continued on next page.)

			Thermal co	nductivity		Standard	Thormal
Core section	Donth		(W/[n		deviation	conductivity	
interval (cm)	CSE (m)	Method*	Raw average	Calibrated [†]	N	(W/[m·K])	(W/[m·K]) [‡]
interval (em)	C31 (11)	method	nutr uveruge	cumprated			
22X-4, 80	147.98	V10305	1.24	1.20	3	0.02	1.22
22X-4, 120	148.38	V10305	1.40	1.36	3	0.01	1.39
22X-6, 60	150.60	V10305	1.34	1.31	3	0.00	1.33
23X-1.85	154.68	V10305	1.18	1.14	3	0.02	1.17
23X-3 50	157 15	V10305	1 1 3	1.09	3	0.01	1 11
23X-5 80	158.88	V10305	1.13	1 10	3	0.02	1 1 2
23X-7 65	161 55	V10305	1.14	1.10	3	0.02	1.12
237-7,03	162.92	V10305	1.22	1.10	2	0.01	1.20
247-1, 30	103.03	V10305	1.10	1.14	2	0.03	1.10
257-1,90	175.75	V10305	1.09	1.05	2	0.03	1.07
258-3, 75	170.39	V10305	1.14	1.10	3	0.02	1.12
258-5, 50	1/8.96	V10305	1.38	1.34	3	0.05	1.37
25X-5, 100	1/9.46	V10305	1.40	1.36	2	0.04	1.39
25X-6, 50	180.37	V10305	1.27	1.23	3	0.03	1.26
25X-8, 25	181.38	V10305	1.36	1.32	3	0.01	1.35
26X-1, 120	183.53	V10305	1.23	1.18	3	0.00	1.21
26X-3, 70	185.94	V10305	1.36	1.32	3	0.01	1.35
26X-5, 45	187.41	V10305	1.18	1.14	3	0.00	1.17
26X-7, 40	189.86	V10305	1.46	1.42	2	0.01	1.45
26X-8, 50	191.38	V10305	1.24	1.20	3	0.03	1.22
27X-1, 80	192.63	V10305	1.18	1.14	3	0.01	1.17
27X-2, 60	193.84	V10305	1.33	1.29	3	0.01	1.32
27X-3, 60	195.26	V10305	1.29	1.25	3	0.00	1.27
27X-4, 40	196.48	V10305	1.47	1.43	3	0.01	1.46
27X-6, 80	198.67	V10305	1.33	1.29	3	0.02	1.31
27X-8 90	201 22	V10305	1 46	1 4 3	3	0.01	1 46
28X-1 90	202.23	V10305	1 33	1 29	3	0.01	1 32
288-2 70	202.23	V10305	1.55	1.22	3	0.01	1.32
288-4 50	203.44	V10305	1.37	1.55	3	0.01	1.50
207-4, 50	204.07	V10305	1.23	1.19	2	0.01	1.21
297-1, 30	211.33	V10305	1.00	1.04	2	0.12	1.00
297-2, 30	212.70	V10303	0.76	0.72	2	0.04	1.23
297-3, 80	214.47	V10305	0.76	0.72	2	0.09	0.75
29X-4, 80	215.88	V10305	0.92	0.87	3	0.03	0.89
29X-5, 80	217.29	V10305	1.27	1.23	3	0.02	1.26
29X-6, 90	218.85	V10305	1.09	1.05	3	0.01	1.07
29X-8, 75	220.13	V10305	1.36	1.32	3	0.01	1.35
30X-1, 50	220.83	V10305	0.82	0.77	2	0.00	0.79
30X-1, 115	221.48	V10305	1.29	1.25	3	0.01	1.27
30X-2, 30	222.04	V10305	1.11	1.07	3	0.01	1.10
30X-4, 50	224.04	V10305	1.41	1.37	3	0.00	1.40
30X-6, 95	226.94	V10305	1.26	1.22	3	0.01	1.24
30X-8, 70	229.52	V10305	1.39	1.36	3	0.00	1.38
31X-1, 65	230.48	V10305	1.37	1.33	3	0.01	1.36
31X-2, 95	232.22	V10305	1.56	1.52	3	0.01	1.55
31X-4, 25	232.94	V10305	1.31	1.27	3	0.01	1.30
31X-5, 72	234.83	V10305	1.18	1.14	3	0.05	1.16
32X-1, 80	240.13	V10305	1.14	1.10	3	0.00	1.13
32X-2, 80	241.56	V10305	1.08	1.04	3	0.01	1.06
32X-3, 50	242.67	V10305	1.45	1.41	3	0.01	1.44
32X-5, 70	244.29	V10305	1.00	0.96	3	0.00	0.98
32X-6, 63	245.64	V10305	1.20	1.16	3	0.04	1.19
32X-8, 30	247.63	V10305	1.21	1.17	3	0.01	1.20
34X-1, 103	259.36	V10305	1.13	1.09	3	0.05	1.11
34X-2, 100	260.74	V10305	1.15	1.11	3	0.01	1.13
34X-3 105	262.20	V10305	1 27	1 23	3	0.00	1 25
342-4 75	263 32	V10305	1.27	1.23	3	0.02	1.20
348-6 50	264 50	V10305	1 30	1.17	3	0.02	1.20
348-7 20	265 21	V10305	1.52	1.55	2	0.05	1.50
358 1 25	202.01	V10303	1.07	1.05	ر د	0.01	1.07
258 2 65	200.00	V10303	1.40	1.37	כ ר	0.02	1.42
JJV-J, DJ	207./1	V10303	1.30	1.34	2	0.01	1.3/
33A-4, 3U	270.90	V10305	1.33	1.29	5	0.01	1.32
368-1, 95	2/8.28	V10305	1.22	1.18	2	0.06	1.20
36X-2, 50	2/9.24	V10305	1.13	1.09	3	0.01	1.11
36X-3, 111	281.26	V10305	1.29	1.25	3	0.01	1.28
36X-5, 50	282.42	V10305	1.32	1.28	1	—	1.30
36X-6, 20	283.16	V10305	1.25	1.21	1	—	1.24
36X-6, 40	283.36	V10305	1.35	1.31	1	—	1.34
36X-6, 65	283.61	V10305	1.45	1.41	1	_	1.44
36X-6, 84	283.80	V10305	1.34	1.30	1	—	1.32



Table T19 (continued).

Core section	Core. section. Depth			Thermal conductivity (W/[m·K])			Thermal	
interval (cm)	CSF (m)	Method*	Raw average	Calibrated [†]	Ν	(W/[m·K])	(W/[m·K]) [‡]	
36X-6, 113	284.09	V10305	1.08 1.04		1	_	1.06	
36X-7, 75	285.13	V10305	1.41	1.37	1	_	1.40	
36X-8, 50	286.28	V10305	1.46 1.42 1		_	1.45		
37X-1, 40	287.23	V10305	1.36 1.32 1 —		1.35			
37X-1, 88	287.71	V10305	1.27	1.23	1	_	1.26	
37X-2, 105	289.30	V10305	1.20	1.15	1	_	1.18	
37X-3, 40	290.06	V10305	1.17	1.13	1	_	1.15	
37X-3, 80	290.46	V10305	1.19	1.15	1	_	1.18	
37X-3, 120	290.86	V10305	1.29	1.25	1	_	1.28	
37X-4, 60	291.67	V10305	1.51	1.48	3	0.16	1.51	
37X-6, 50	292.99	V10305	1.27	1.23	2	0.00	1.26	
37X-7, 80	294.70	V10305	1.40	1.37	2	0.01	1.39	
37X-8, 15	295.46	V10305	0.41	0.35	1	_	0.36	
38X-3, 30	297.21	V10305	1.20	1.16	2	0.05	1.19	
39X-1, 26	306.09	V10305	1.03	0.98	1	_	1.00	
39X-1, 60	306.43	V10305	1.21	1.16	1	_	1.19	
39X-1, 110	306.93	V10305	1.20	1.16	1	_	1.18	
39X-2, 62	307.86	V10305	1.19	1.14	1	_	1.17	
39X-3, 15	308.80	V10305	1.01	0.96	1	_	0.98	
39X-3, 60	309.25	V10305	1.19	1.15	1	_	1.17	
39X-5, 46	310.53	V10305	1.13	1.08	2	0.03	1.11	
39X-5, 115	311.22	V10305	1.19	1.15	2	0.04	1.17	
39X-6, 30	311.78	V10305	1.05	1.01	2	0.01	1.03	
39X-6, 75	312.23	V10305	1.21	1.17	3	0.01	1.20	
39X-7, 85	313.74	V10305	1.25	1.21	2	0.01	1.24	
40X-1, 100	316.33	V10305	0.32	0.26	3	0.01	0.27	
40X-2, 75	317.49	H10304	1.26	1.15	3	0.03	1.18	
40X-3, 30	318.46	H10304	1.18	1.06	3	0.02	1.09	
40X-5, 20	320.79	H10304	1.07	0.96	3	0.21	0.98	
40X-8, 85	323.26	H10304	1.34	1.24	3	0.07	1.26	
43X-2, 125	346.49	H10304	1.44	1.35	9	0.03	1.38	
45X-8, 7	371.36	H10304	1.25	1.13	2	0.00	1.16	
46X-4, 30	376.87	H10304	1.51	1.44	15	0.01	1.47	
47X-4, 39	386.45	H10304	1.54	1.48	10	0.15	1.51	
49X-1, 57	401.40	H10304	1.68	1.64	9	0.05	1.68	
316-C0006F-								
06R-1, 55	438.55	H10304	1.52	1.49	8	0.11	1.51	
07R-1, 62	448.12	H10304	1.31	1.27	10	0.02	1.30	
10R-1, 47	476.47	H10304	1.28	1.24	5	0.00	1.26	
11R-1, 21	485.15	H10304	1.32	1.28	6	0.01	1.31	
12R-2, 60	497.04	H10304	1.46	1.42	8	0.09	1.45	
13R-1, 104	505.54	H10304	1.24	1.20	5	0.01	1.23	
14R-3, 54	517.56	H10304	1.33	1.29	5	0.00	1.32	
18R-1, 35	552.35	H10304	1.42	1.38	10	0.00	1.41	
19R-1, 97	562.47	H10304	1.48	1.45	9	0.01	1.47	

Notes: * = V10305 refers to full-space needle probe and H10304 refers to half-space line source, † = thermal conductivities were adjusted based on calibration formulas and constants given in the "Expedition 316 methods" chapter, ‡ = thermal conductivities were corrected for temperature and pressure as described in the "Expedition 316 methods" chapter. CSF = core depth below seafloor. — = not applicable.



Table T20. Temperature measurements, Hole C0006E. (See table notes.)

			Fit		Equilibrium				
Core	Tool	Depth CSF (m)	BWT (°C)	Time delay (s)	Start (min)	End (s)	temperature (°C)	Remark	
316-C00	06E-								
3H	APCT3	24.20	1.55	15.9	1.8	9.0	2.85		
5H	APCT3	38.50	1.66	15.0	1.0	12.7	3.00		
8H	APCT3	_	_	_	_	_	_	Bad data—tool movement.	
10H	APCT3	64.70	1.64	24.6	1.0	5.0	3.75		
12H	APCT3	_	_	_	_	_	_	Tool did not deploy.	
14H	APCT3	_	_	_	_	_	_	Tool did not penetrate.	
16H	DVTP	98.30	1.69	19.7	2.0	4.8	4.82	Tool movement truncated equilibrium temperature fit.	
23H	DVTP	_	_	_	_	_	_	Power failure—tool.	
26H	DVTP	_	_	_	_	_		Thermistor open closed circuit.	
28H	DVTP	_	_	_	_	_	_	Tool stuck in pipe; battery terminal sheared.	
29H	DVTP	220.30	1.69	37.9	1.5	4.8	7.87	Premature pullout.	
35H	DVTP	277.30	1.69	105.8	2.1	7.8	3.03	Tool movement after 7.8 min.	
42H	DVTP	_	—	—	—	—	_	Stiff formation/collet protection activated.	

Notes: CSF = core depth below seafloor. BWT = bottom water temperature. APCT3 = advanced piston corer temperature tool, DVTP = Davis-Villinger temperature probe. — = not measured.



 Table T21. Correlation and depth shifts among all holes, Site C0006. (See table notes.) (Continued on next page.)

Depth					Depth shift (m)				
LSF (m)		Depth C	SF-B (m)			Depth s	hift (m)		
Hole C0006B	Hole C0006C	Hole C0006D	Hole C0006E	Hole C0006F	Hole C0006C	Hole C0006D	Hole C0006E	Hole C0006F	
3.8	2.1	0.0	2.0		-1.7	-3.8	-1.8		
11.5	5.8	5.4	7.5		-5.7	-6.1	-4.0		
14.8	7.5	8.4	10.7		-7.3	-6.4	-4.1		
24.0			21.6				-2.4		
30.2			27.2				-3.0		
38.7			36.8				-1.9		
49.8			51.6				1.8		
56.6			59.4				2.8		
64.2			66.7				2.5		
71.1			72.0				0.9		
76.1			78.1				2.0		
80.8			80.8				0.0		
86.4			85.2				-1.2		
89.6			90.1				0.5		
99.3			99.7				0.4		
109.6			107.4				-2.2		
122.6			119./				-2.9		
132.5			128.3				-4.2		
141.0			139.3 1 <i>16</i> 0				-2.3		
150.0			140.0				-3.2		
163.1			163.3				-0.9		
178.2			176.8				_1 4		
185.5			183.3				_2.2		
199.0			192.0				-7.0		
206.9			201.2				-5.7		
210.5			204.9				-5.6		
224.9			218.8				-6.1		
236.0			229.8				-6.2		
245.2			239.0				-6.2		
248.9			243.8				-5.1		
270.0			265.0				-5.0		
283.5			278.6				-4.9		
289.4			286.0				-3.4		
298.0			295.2				-2.8		
313.6			311.4				-2.2		
326.7			322.0				-4.7		
334.7			329.9				-4.8		
347.8			343.7				-4.1		
358.5			356.8				-1./		
364./			303.8				-0.9		
3/3./ 201 0			372.2				-1.5		
301.0			379.0				-2.0 _4 7		
402.3			396.4	395 8			_5.9	-6 5	
406.8			400.7	400.3			-6.1	-6.5	
409.7			404.2	403.5			-5.5	-6.3	
412.4				406.6			0.0	-5.8	
420.3				415.2				-5.1	
428.4				424.6				-3.8	
438.2				434.6				-3.6	
443.0				438.6				-4.4	
455.2				449.0				-6.2	
462.7				457.5				-5.2	
473.1				467.6				-5.5	
483.0				477.1				-5.9	
493.0				487.1				-5.9	
501.0				496.5				-4.5	
513.1				506.0				-7.1	
520.2				514.4				-5.8	
524.7				518.3				-6.4	
530.5				525.8				-4.7	
538.3				534.9				-3.4	
558.6				555.5 565 A				-3.3	
572.4				202.4				-7.0	



Table T21 (continued).

Depth LSF (m)	_	Depth C	SF-B (m)		_	Depth s	hift (m)	
Hole C0006B	Hole C0006C	Hole C0006D	Hole C0006E	Hole C0006F	Hole C0006C	Hole C0006D	Hole C0006E	Hole C0006F
577.8 597.9				572.3 591.4				-5.5 -6.5

Notes: Hole C0006B logs are from LWD data acquired during IODP Expedition 314. Hole C0006C, C0006D, C0006E, and C0006F logs are from MSCL-W data from whole-round cores. LSF = LWD depth below seafloor, CSF-B = core depth below seafloor, IODP Method B (see the "Expedition 316 methods" chapter).

